

OPTIMIZATION OF MACHINING PARAMETERS USING GENETIC ALGORITHM

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(CAD/CAM & ROBOTICS)

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CERTIFICATE

This is to certify that the thesis entitled “**Optimization of Machining Parameters Using Genetic Algorithm**” being submitted by **Mr. Deepak Bhandari** in partial fulfillment of the requirements for the award of the degree of **MASTER OF ENGINEERING (CAD/CAM & ROBOTICS)** at **Thapar Institute of Engineering & Technology (Deemed University), Patiala**, is a bonafide work carried out by him under our supervision and guidance.

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ABSTRACT

The present competitive environment forces the organizations to stand on alert every minute and use its resources (man, material, and machine) to their best possible extent. The present work aims to explore genetic algorithm (GA) as a method for optimizing machining parameters selection. The algorithm searches for the best solution in terms of cutting speed and feed with the aim of optimizing an objective function. The objective functions considered here take into account optimizing anyone or a weighted sum of the two significant criteria- total production cost and total production time, in single pass turning operation. The GA technique used for optimization purpose provides an efficient and promising tool in view of high degree or non-linearity in the objective function. The technique, although applied here only on single pass turning, is applicable to much wider variety of machining situations.

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CHAPTER 1

INTRODUCTION

1.1 OPTIMIZATION

Optimization algorithms are becoming increasingly popular in engineering activities, primarily because of the availability and affordability of high-speed computers. They are extensively used in those engineering problems where the emphasis is on maximizing or minimizing of a certain goal.

For example, optimization algorithms are routinely used in aerospace design activities to minimize the overall weight, simply because every element or component adds to the overall weight of the aircraft. Chemical engineers on the other hand are interested in designing or operating a process plant for an optimum rate of production. Mechanical engineers design mechanical components for the purpose of achieving either a minimum manufacturing cost or maximum rate of production.

Production engineers are interested in designing optimum schedules of various machining operations to minimize the idle time of machines and the overall completion time. Civil engineers are involved in designing buildings, dams and other structures in order to achieve a minimum overall cost or maximum safety or both. Electronics engineers are interested in designing communication networks so as to achieve minimum time for communication from one node to another.

Thus, the ultimate aim of the optimization is to improve an existing process that meets the given requirements and satisfies all the restrictions/constraints placed on it. This is called the optimum process.

1.2 OPTIMIZATION IN MACHINING

Machining parameters such as speed, feed and depth of cut play vital role in machining the given work piece to the required shape. These have a major affect on the quantity of production, cost of production and production rate; hence their judicious selection assumes significance.

The selected machining parameters should yield desired quality on the machined surface while utilizing the machining resources such as machine tool and cutting tool to the fullest extent possible, consistent with the constraints on these resources. Traditionally the selection of machining parameters is carried out based on the experience of the machinist or the planner and referring the available catalogues and handbooks.

Manual selection of machining parameters reflects the problem of variability in experience and judgement among the planners. In addition to this, the induction of cost intensive NC-machines onto the shop floor, stresses more emphasis on the effective utilization of these resources using the optimal machining parameters. Present industries use both conventional and NC machines on their shop floor, hence it becomes necessary to go for automated methods to select the optimal machining parameters that suit the demands of the present industries.

Computer aided procedures have been found reliable for their fastness, accuracy and consistency in the automated selection of machining parameters compared to their manual counterparts. Various optimization techniques can be used to find the optimal machining parameters for a particular machining operation.

1.3 APPROACHES FOR MACHINING PARAMETER SELECTION

The advances in the manufacturing engineering and developments in the areas of computer aided design and computer aided manufacturing, give a high level of automation in the present competitive environment. In accordance with this, attempts have also been made to automate the selection of machining parameters. The traditional methods have been replaced by reliable computer aided procedures in the selection of machining parameters. Much of the research work has been done and ample literature is available in this direction.

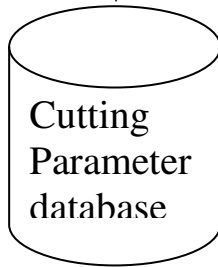
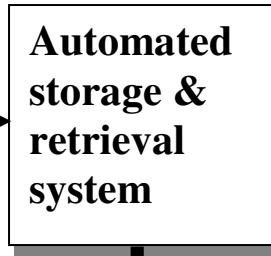
The published literature reveals that there are two most popular approaches for automated selection of machining parameters as give below:

- **DATA STORAGE AND RETRIEVAL APPROACH**
- **MATHEMATICAL MODEL APPROACH**

1.3.1 DATA STORAGE AND RETRIEVAL APPROACH

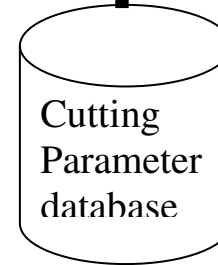
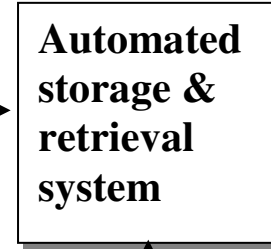
This approach consists of two steps as shown in the figure (1.1). In the first step, recommended parameters for various combinations of work material, tool material and machining operation are collected from the shop floor, cutting tool and machine tool manufacturer's catalogues and handbooks. Then, these parameters are stored in a database in a structured format as shown in the figure 1.1 (a). Based on the user inputs, the proper set of cutting conditions is retrieved from the database as shown in figure 1.1 (b) and presented to the user.

	BHN	V	feed
M.S.	200	175	0.5



(a)

Work material
 Work hardness
 Tool material
 Machining operation



(b)

Speed
 Feed
 Depth of cut

Figure 1.1 Data storage and retrieval approach

(a) Storage and (b) Retrieval

This is in-effect a computerized look-up table approach. Though this approach aids in the fast and consistent selection of parameters, the parameters are general in nature and a lot of computer storage space is required. Also they are often characterized by lack of adequate maintenance and difficulties in updating the current machining recommendations.

1.3.2 MATHEMATICAL MODEL APPROACH

In this approach, the problem is converted into mathematical models based on certain criteria. The criteria differ for different problems. In case of automated machining parameters selection, mathematical model are formulated to determine the machining parameters for a particular objective such as minimization of unit cost or maximization of production rate. In this approach, empirical equations formulated based on experimental data for tool life (usually extended tool life equations) and other practical restrictions on machining variables are used in the model development. The resultant function from this mathematical modeling is called objective function, which is subjected to practical constraints. The developed model is then solved using an optimization technique to yield optimal parameters that reflects the shop floor capabilities. This procedure is illustrated in Figure 1.2. The success of this approach depends on the reliability of the empirical equations used in the model formulation.

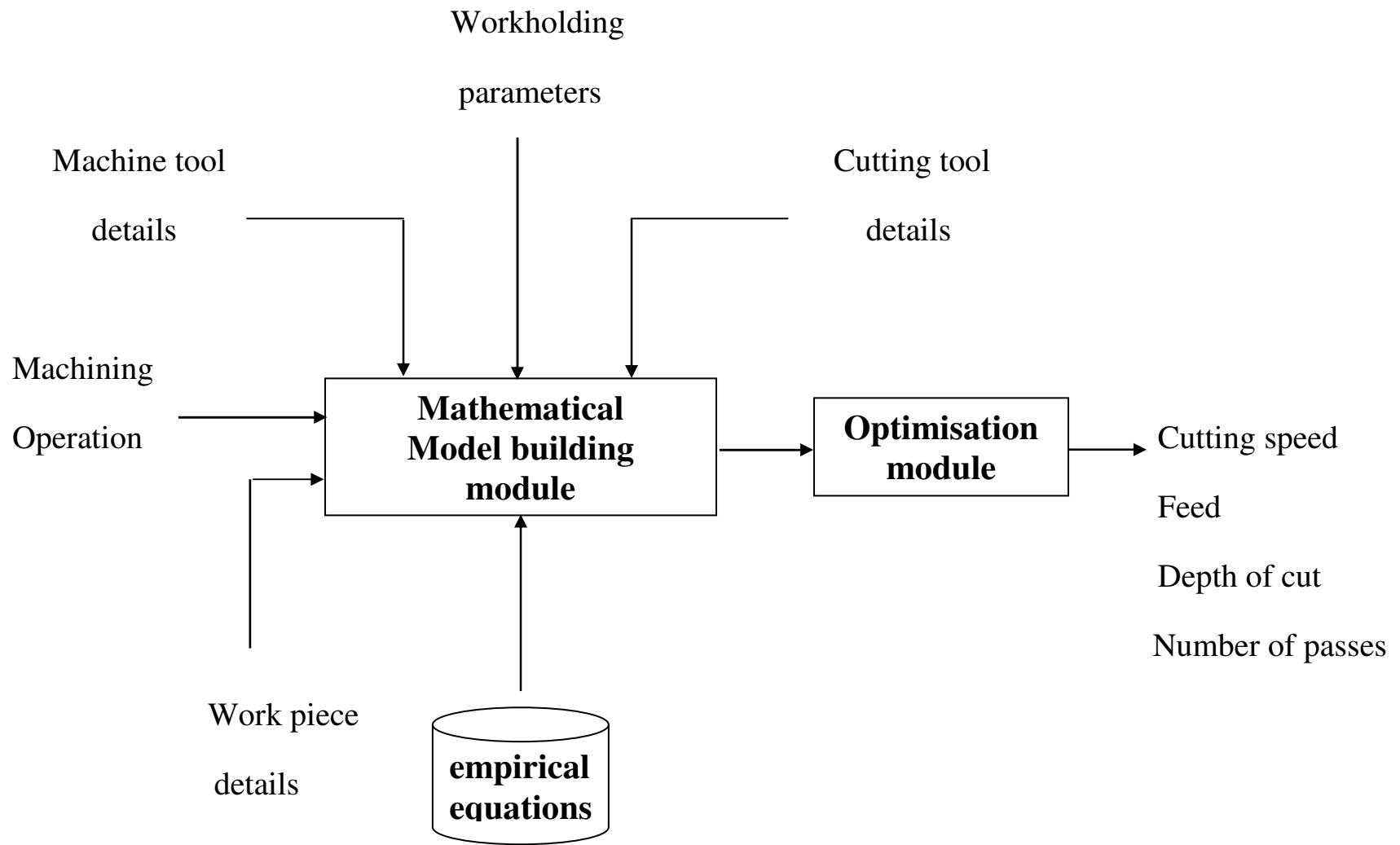


Figure 1.2 Mathematical model approach

CHAPTER 2

LITERATURE-SURVEY

Armarego and Brown [1] expressed the production cost and production rate in terms of speed and feed rate and partially differentiated these terms with respect to speed and feed which are equated to zero to get optimum cutting conditions.

Yen and Wright [2] developed a unified method of adaptive control of constraints in which a suitable cutting region is determined satisfying all the physical constraints. The objective of the optimization is to maximize the production rate under constraints of plastic deformation, crater wear and fracture. Taylor's tool life equation is not used and the tool life equations for different model of failures are established on the basis of properties of tool and work material.

R. Meenakshi Sunderam and Tajen Cheng [5] proposed a process planning system with the aid of a microcomputer. They have developed a computer program in BASIC. In their software development, the geometric programming technique is used for the selection of optimal machining parameters.

J. S. Agapiou [6] developed a Nelder-Mead Simplex Method to determine the optimum machining conditions. An objective function incorporating a combination of the minimum production cost and minimum production time requirements is considered for the optimization. The two criteria of production time and production cost are prioritized

through their weight coefficients. A constant multiplier is used to normalize the objective function. Physical constraints regarding the cutting parameters are also considered. The superiority of the combined objective function over the single criterion objective functions, using the production cost, or production time, or maximum profit rate is also illustrated.

J. S. Agapiou [7] outlined the use of two techniques (Dynamic Programming and Nelder-Mead Simplex Method) to determine the optimum cutting conditions for the multi-pass operations. The optimum number of machining passes is obtained through the dynamic programming technique and the optimum machining conditions for each pass are then determined based on the combined objective function of total production cost and the total production time. This approach can be very effectively applied to the multi-stage machining since the optimum arrangement of the different operations can be determined by the dynamic programming method while the optimum cutting conditions for the operation in each machining stage are obtained using the method for single pass (Nelder-Mead Simplex Method) while incorporating the objective function.

A. Ihsan Sonmez and Adil Baykasoglu [14] have outlined the development of an optimization strategy to determine the optimum cutting parameters for multi-pass milling operations like plain milling. The developed strategy is based on the maximum production rate and incorporates eight technological constraints. The optimum number of passes is determined via dynamic programming and the optimum values of cutting conditions are found based on the objective function by using the geometric programming technique. This paper also underlies the importance of using optimization strategies rather than handbook recommendations.

Dereli, T. and Filiz, H. I. [16] explained the application of GA for determination of optimal sequence of machining operations based on either minimum tool change or minimum tool traveling distance or safety. Combination of these criteria also might be used. They have also explained how the optimum position of tools on the automatic tool changer or turret magazine of a CNC machine tool is obtained by using GA.

T. S. Sidhu [17] outlined the use of goal programming technique in setting optimum machining parameters in single pass turning operation. The optimum values for speed and feed are determined by setting different goals under a given set of conditions. The calculated values are set on the lathe and surface finish of the turned work pieces are measured for different values of depth of cut.

Q. Meng [21] have used machining theory for calculating optimum cutting conditions in turning. The method uses a variable flow stress machining theory to predict cutting forces, stress etc. which are then used to check process constraints such as machine power, tool plastic deformation and built-up edge formation. Their results indicate that the method is capable of selecting the appropriate cutting conditions.

M. S. Shunmugam and S. V. Bhaskara Reddy [22] outlined the use of genetic algorithm for the selection of optimal conditions in multi-pass face-milling operation. In this work, the total production cost is used as an objective function. The number of passes, speed and feed are obtained using the machining theory and then the depth of cut for the each pass is determined by using the genetic algorithm. The technological constraints considered here is allowable speed and feed, dimensional accuracy, surface finish, tool wear and machine tool capabilities.

Y. V. Hui [23] developed a time dynamic economic model for single pass turning. The model incorporates considerations on the stochastic nature of the tool life and tool maintenance activities such as tool replacement and tool regrinding. Furthermore, they have developed a model of quality cost of tool cutting in terms of deviation from target roughness and deviation from target dimension. Finally, they have provided a quality machining economic model for turning to investigate the trade-off between quality cost and other cost factors.

Nafis Ahmad and Dr. A. F. M. Anwarul Haque [24] outlined the use of genetic algorithm to find out the optimum machining parameters. In this work, machining parameters for the turning rotational components are optimized by a genetic algorithm optimization toolbox developed in Matlab environment. Here machining time is considered as the objective function and constraints are machining capacity, limits of feed rate, depth of cut and cutting speed. Machining time is minimized through a series of generations while some genetic operators are applied at each generation. The result of the work shows how a complex optimization problem is handled by a genetic algorithm and converges very quickly.

In the present work, optimization of machining parameters (feed and speed) has been done with GA (genetic algorithm) by using the data from J. S. Agapiou [6]. Hence, in the 3rd chapter, basics of GA are explained and in the 4th chapter, mathematical formulation of the single pass machining optimization problem has been done.

CHAPTER 3

GENETIC ALGORITHM

Machining optimization problem requires a robust search method (Robustness means numerical stability and ability to find a solution for a wide range of algorithmic parameters), which runs well in complex situations. The genetic algorithm (GA) approach has been selected firstly because their behavior is robust and so far efficient and secondly more and more attention is being drawn to GA in a variety of disciplines. Evolution program started in the sixties when a group of biologists used digital computers to simulate genetic systems.

But it was John Holland who, in 1975, published ‘**Adaptation in natural and artificial systems**’, laying down the two main principles for current GAs: the ability of simple representation (bit strings) to encode complicated structures. In his schemata theory he explains, how with proper control, there is rapid improvement in the bit strings as also occurs in animal population. Thereafter a number of his students and other researchers have contributed to developing this field. An extensive list of GA-related papers is referenced in **Goldberg [13]**.

3.1 BASIC GA OPERATIONS

Let us consider the following minimization problem:

Minimize $f(x)$

$$x_i^{(L)} \leq x_i \leq x_i^{(U)}, \quad i=1,2,\dots,N.$$

3.1.1 CODING

In order to use GAs to solve the above problem, variables x_i are first coded in some string structure. It is important to mention here that the coding of variables is not absolutely necessary. There exist some studies where GAs is directly used on the variables (**Real-Coded GAs**). The type of coding used is a critical decision, which is made on the basis of the nature of the problem.

As an example, if four bits are used to code each variables in a two-variable function optimization problem, the strings **(0000 0000)** and **(1111 1111)** would represent the points

$$(x_1^{(L)}, x_2^{(L)}) \quad (x_1^{(U)}, x_2^{(U)})$$

respectively, because the sub-strings (0000) and (1111) have the minimum and the maximum decoded values. Any other eight-bit string can be found to represent a point in the search space according to a fixed mapping rule. Usually, the following linear mapping rule is used:

$$x_i = x_i^{(L)} + [x_i^{(U)} - x_i^{(L)} / (2^{I_i} - 1)] * \text{Decoded values of } (S_i) \quad (1)$$

In the above equation, the variable x_i is coded in a sub-string S_i of length I_i . The decoded value of binary sub-string S_i is calculated as $\sum 2^j b_j$ where b_j can be 0 or 1 as obtained from the string. Here, j varies from 1 to I_i with four bits to code each variable; there is only 2^4 or 16 distinct sub-strings possible, because each bit-position can take a value either 0 or 1. The accuracy that can be obtained with a four bit coding only approximately $1/16^{\text{th}}$ of the

search space. But as the string length increased by one, the obtainable accuracy increased $1/32^{\text{nd}}$ of the search space.

The length of a sub-string representation depends upon the desired accuracy in that variable.

Generalizing this concept, we may say that I_i -bit coding for a variable, the obtainable accuracy in that variable is approximately

$$x_i = (x_i^{(U)} - x_i^{(L)}) / (2^{I_i} - 1).$$

Once the coding of the variable has been done, the corresponding point $x = (x_1, x_2, x_3, \dots, x_N)$ can be found using equation (1). Thereafter, the function value at the point x can also be calculated by substituting x in the given objective function $f(x)$.

3.1.2 FITNESS FUNCTION

GAs mimics the 'survival-of-the-fittest' principle of nature to make a search process. Therefore, GAs are naturally suitable for solving maximization problems. Minimization problems are usually transformed into maximization problems by some suitable transformation. In general, a fitness function $F(x)$ is first derived from the objective function $f(x)$ and used in successive genetic operations. Certain genetic operators require that the fitness function to be non-negative, although certain operators do not have this requirement.

For maximization problems the fitness function can be considered to be the same as the objective function or $F(x) = f(x)$. For minimization problem, the fitness function is an equivalent maximization problem chosen such that optimum point remains unchanged. A number of such transformations are possible. The following function is often used for that purpose:

$$F(x) = 1 / (1 + f(x))$$

This transformation does not alter the location of the maximum, but converts a minimization problem to an equivalent maximization problem. The fitness function value of a string is known as the string's **fitness**.

3.1.3 GENERATION

The operation of GAs begins with a population of random strings representing machining or decision variables. Thereafter, each string is evaluated to find the fitness value. The population is then operated by three main operators- **reproduction**, **crossover**, and **mutation** – to create a new population of points. The new population is further evaluated and tested for termination. If the termination criterion like the maximum generation or predefined fitness value is not met, the population is iteratively operated by the above operators and evaluated. This procedure is continued until the termination criterion is met. One cycle of these operations and the subsequent evaluation procedure is known as a **generation in GA's terminology**.

3.1.4 GA OPERATORS

Reproduction is usually the first operator applied on a population. Reproduction selects good strings in a population and forms a mating pool. That is why the reproduction operator is sometimes known as the **selection operator**. There exists a number of reproduction operators in GA literature, but the essential idea in all of them is that the above-average strings are picked from the current population and their multiple copies are inserted in the mating pool in a probabilistic manner. The commonly used reproduction operator is the **proportionate reproduction operator** where a string is selected for the

mating pool with a probability proportional to the fitness (F_i). Thus the i -th string in the population is selected with a probability proportional to F_i . Since the population size is usually kept fixed in a simple GA, the sum of the probability of the strings being selected for the mating pool must be one therefore, the probability for selecting the i -th string is

$$p_i = F_i / \sum F_j$$

Where i varies from 1 to n , n being the population size and j also varies from 1 to n in the summation. One way to implement this selection scheme is to imagine a roulette-wheel with its circumference marked for each string proportionate to the string's fitness. The roulette-wheel is spun n times, each time selecting an instance of the string chosen by the roulette-wheel pointer.

Fig.3.1 shows a roulette-wheel for five individual having different fitness value. Since the third individual has the higher fitness value than any other, it is expected that the roulette-wheel selection will choose the third individual more than any other individual. This roulette-wheel selection scheme can be simulated easily. Using the fitness value F_i ,

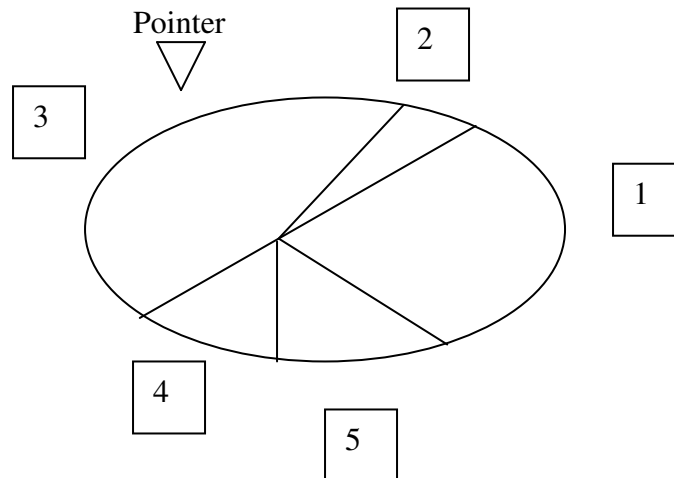


Figure.3.1 A Roulette-wheel

TABLE 3.1

Point	Fitness
1	25.0
2	5.0
3	42.0
4	10.0
5	18.0

of all strings, the probability of selecting a string \mathbf{p}_i can be calculated. Thereafter the cumulative probability (\mathbf{P}_i) of each string being copied can be calculated by adding the individual probability from the top of the list. Thus, the bottom most string should have cumulative probability (\mathbf{P}_n) equal to one.

The roulette-wheel concept can be simulated by realizing that the i -th string in the population represents the cumulative probability values from P_{i-1} to P_i . The first string represents the cumulative values from 0 to P_1 . Thus, the cumulative probability of any string lies between 0 to 1. In order to choose n strings, n random numbers between 0 and 1 are created at random. Thus a string that represents the chosen random number in the cumulative range (calculated from the fitness values) for the string is copied to the mating pool. This way, the string with a higher fitness value will represent a larger range in the cumulative probability values and therefore has a higher probability values and therefore has a higher probability of being copied into the mating pool. On the other hand, a string with a smaller fitness value represents a smaller range in cumulative probability values and has a smaller probability of being copied into the mating pool.

In **reproduction**, good strings in a population are probabilistically assigned a larger number of copies and a mating pool is formed. It is important to note that no new strings are formed in the reproduction phase.

In the **crossover operator**, new strings are created by exchanging information among strings of the mating pool. Many crossover operators exist in the GA literature. In most of the crossover operators, two strings are picked from the mating pool at random and some portions of the strings are exchanged between the strings. A single point crossover operator is performed by randomly choosing site along the string and by exchanging all bits on the right side of the crossing site as shown:

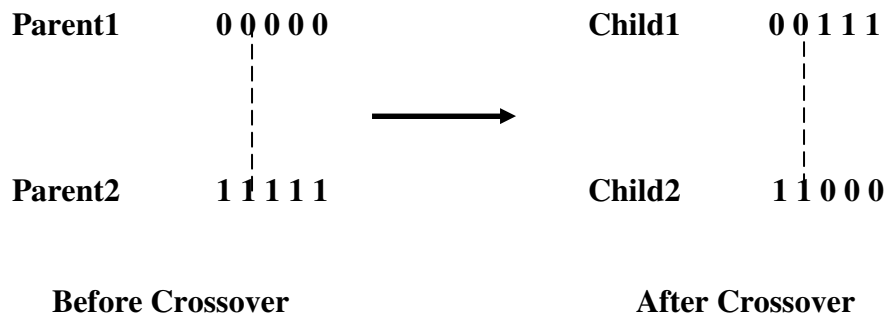


Figure 3.2

The two strings participating on the crossover operation are known as ‘parent strings’ and the resulting strings are known as ‘children strings’. Here, the dotted line represents the crossover site. It is intuitive that good sub strings from parent strings can be combined to form a better child string, if an appropriate site is chosen. Since the knowledge of appropriate site is usually not known before hand, a random site is often chosen. With a random site the children string produce may or may not have a combination of good sub string from parent string, depending on whether or not the crossing falls in the appropriate place. But we do not worry about this too much, because if good strings are created by crossover there will be more copy of them in the next mating pool generated by reproduction operator. But if good strings are not created by crossover, they will not survive to long, because reproduction is selected against those strings in subsequent generations.

It is clear from the above discussion that the effect of crossover may be beneficial. Thus, in order to preserve some of the good strings that are already present in the mating pool, not all strings in the mating pool are used in the crossover. When a crossover probability of p_c is used, only $100p_c$ percent strings in the population are used in the crossover population and $100(1-p_c)$ percent of the population remains as they are in the current population.

A crossover operator is mainly responsible for the search of the new string taking into account the character string in the mating pool.

The **mutation operator** changes 1 to 0 and vice-versa with a small mutation probability, p_m . The bit-wise mutation is performed bit by bit by flipping a coin with a probability p_m is simulated as follows:

A number between 0 and 1 is chosen at random. If the random number is smaller than p_m , the outcome of coin flipping is true; otherwise the outcome is false.

If at any bit the outcome is true then the bit is altered; otherwise the bit is kept unchanged. The need for mutation is to create a point in the neighborhood of the current point, thereby achieving a local search around the current solution. The mutation is also used to maintain diversity in the population. For example, consider the following population having four eight-bit strings:

0110 1011
0011 1101
0001 0110
0111 1100

It is to be noticed in the above population that all four strings have a 0 in the left most bit position.

If the true optimum solution requires 1 in that position, then neither reproduction nor crossover operator described above will be able to create 1 in that position. Then mutation operator is the only rescue.

3.2 DIFFERENCE BETWEEN GAS AND TRADITIONAL METHODS

As seen from the above description of the working principles of GAS, they are radically different from most of the traditional optimization methods. However, the fundamental differences are described as:

(i) DISCRETIZATION OF SEARCH SPACE

GAS work with a string coding of variables instead of the variables. The advantage of working with a coding of variables is that the coding discretizes the search space; even though the function may be continuous function can be handled with no extra cost. This allows GAS to be applied to a wide variety of problems.

(ii) NO GRADIENT INFORMATION REQUIRED

In GA operators or in their working principles no information about the gradient of a function is required. Infact, GAS do not require any auxiliary information except the function values.

(iii) PROBABILISTIC IN NATURE

One other difference is the operation of GAS is the use of probabilities in their operators. None of the genetic operators work deterministically. In the reproduction operator,

simulation of the roulette- wheel selection scheme is used to assign the true number of copies. In the crossover operator, even though good strings (obtained from the mating pool) are crossed, strings to be crossed are created at random and so is the case with the crossing sites. In the mutation operator, a random bit is suddenly altered. The action of these operators may appear to be native, but careful studies may provide some interesting insights about this type of search.

(iv) ROBUSTNESS

The basic problem with most of the traditional methods is that they use fixed transition rules to move one point to another. For instance, in the steepest descent method, the search direction is always calculated as the negative of the gradient at any point, because in that direction the reduction in the function value is maximum. In trying to solve a multi-modal problem with many local optimum points (interestingly, many real world engineering optimization problems including those of machining optimization are likely to be multimodal), search procedures may easily get trapped in one of the local optimum points. Consider the bimodal function shown in figure 3.4. The objective function has one local minimum and one global minimum. If the initial point is chosen to be a point in the local basin (point $x^{(t)}$ in the figure) the steepest descent algorithm will eventually find the local optimum point.

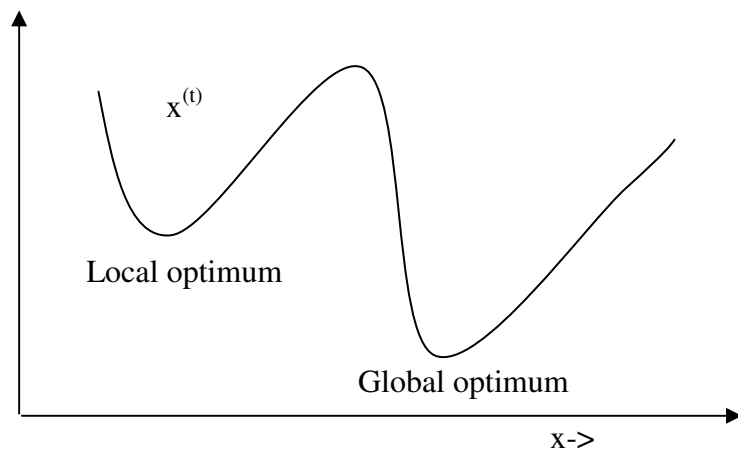


Figure 3.4

Since the transition rules are rigid, there is no escape from these local optima. The only way to solve the above problem to global optimality is to have a starting point in the global basin. Since this information is usually not known in any problem, the steepest –descent method (and for that matter most traditional methods) fails to locate the global optimum. However, these traditional methods can be best applied to a special class of problems suitable for those methods. For example, the gradient search methods will outperform, almost any algorithm in solving continuous, unimodal problems, but they are not suitable for multi-modal problem.

Thus in general, traditional methods are not robust. A robust algorithm can be designed in such a way that it uses the steepest descent direction most of the time, but also uses the steepest descent direction (or any other direction) with some probability. Such a mixed strategy may require more number of function evaluations to solve continuous, unimodal problems, because of the extra computations involved in trying with non-descent direction. But this strategy may be able to solve complex multimode problem to global optimality. In the multi-modal problem, shown in the above figure, the mixed strategy may take the point $x^{(t)}$ into the global basin (when tried with non-descent directions) and finally find the global optimum point.

GA use similar search strategies by using probability in all their operators. Since an initial random population is used, to start with, the search can proceed in any direction and no major decisions are made in beginning. Later on, when the population begins to converge in some bit positions, the search directions narrow and a near optimal solution is achieved. This nature of narrowing the search space as the search progress is adaptive and is a unique characteristic of genetic algorithms.

3.3 BASIC ALGORITHM

Step 1 Choose a coding to represent problem parameters, a selection operator, a crossover operator, and a mutation operator. Choose population size, n , crossover probability, p_m . Initialize a random population of strings of size n . Choose a maximum allowable generation number t_{max} . Set $t = 0$.

Step 2 Evaluate each string in the population.

Step 3 If $t > t_{max}$ or other termination criteria is satisfied, Terminate.

Step 4 Perform **reproduction** on the population.

Step 5 Perform **crossover** on the random pairs of strings.

Step 6 Perform **mutation** on every string.

Step 7 Evaluate strings in the new population. Set $t = t+1$ and go to **step 3**.

The algorithm is straightforward with repeated application of three operators (**Step 4 to 7**) to a population of points (strings).

3.4 GAS FOR CONSTRAINED OPTIMIZATION

Genetic algorithms have also been used to solve constrained optimization problems. Although different methods to handle constraints have been suggested, penalty function methods have been mostly used. In the penalty function method, a penalty term corresponding to the constraint violation is added to the objective function. In most cases,

Two random sites are chosen along the string length and bits inside the cross-sites are swapped between the parents.

3.6 REAL CODDED GAs

GAs has also been developed to work with continuous variables (instead of discrete variables). In that GAs, binary strings are not used. Instead, the variables are directly used. Once a population of random sets of points is created, a reproduction operator (roulette-wheel or other selection operators) can be used to select good strings in the population. In order to create new strings, the crossover the mutation operators described earlier cannot be used efficiently. Even though simple single-point crossover can be used on those points by forcing the cross-sites to fall only on the variable boundaries, the search is nor adequate. This type of GA has been used in earlier studies by Wright. Recently, new and efficient crossover operators have been designed so that search along variables is also possible.

Let us consider $x_i^{(j)}$ and $x_i^{(k)}$ values of design variables x in two parent strings j & k . The crossover between these two values may produce the following new value:

$$x_i^{(new)} = (1 - \lambda) x_i^{(j)} + \lambda x_i^{(k)} \quad 0 < \lambda < 1 \quad (II)$$

The parameter λ is a random between zero & one. The above equation calculates a new value bracketing $x_i^{(j)}$ and $x_i^{(k)}$. This calculation is performed for each variable in the string. This crossover has a uniform probability of creating a point inside the region bounded by two parents. An extension to this crossover is also suggested to create points outside the range bounded by the parents. Eshelman and Schaffer have suggested to blend crossover operator (BLX- α), in which a new point is created uniformly at random from a

larger range extending an amount $\alpha |x_i^{(j)} - x_i^{(k)}|$ on either side of the region bounded by two parents. The crossover operation depicted in Equation (II) can also be used to achieve BLX- α by varying λ in the range $(-\alpha, 1+\alpha)$. In a number of test problems, Eshleman and Schaffer have observed that $\alpha=0.5$ provides good results.

One interesting feature of this type of crossover operator is that the created point depends on the location of both parents. If both parents are close to each other, the new point will also be close to the parents. On the other hand, if parents are far from each other, the search is more like a random search.

The random search feature of these crossover operators can be relaxed by using a distribution other than random distribution between parents. A recent study using a polynomial probability distribution with a bias towards near-parent points has been found to perform better than BLX-0.5 in a number of test problems. More studies in this direction are necessary to investigate the efficacy of real-coded GAs.

CHAPTER 4

PROPOSED METHODOLOGY

4.1 FORMULATION OF THE OPTIMIZATION PROBLEM

The formulation of the optimization problem requires the knowledge of some mathematical equations, which represent the economical and physical parameters for the machining process and the whole machine-tool system. The mathematical formulation used here is:

4.1.1 FORMULATION OF THE OBJECTIVE FUNCTION

Both the production cost and total production time are considered in the formulation of the objective function. The production cost per component for a machining operation is comprised of the sum of the costs for tooling, machining, tool changing time, handling time and quick return time:

$$\text{Time of machining, } T_m = \frac{L}{fN}$$

$$V = \frac{\pi DN}{1000}$$

$$\therefore T_m = \frac{\pi DL}{1000fV}$$

$$\text{Cost of cutting action} = C_o T_m$$

$$\text{Cost of tool changing} = C_o \frac{T_m}{T} T_{cs}$$

$$\text{Cost of tooling} = C_t \frac{T_m}{T}$$

$$\text{Handling cost} = C_o T_h$$

$$\text{Quick return time} = T_r$$

$$\text{Total cost of Production} = C_o T_m + C_o \frac{T_m T_{cs}}{T} + C_t \frac{T_m}{T} + C_o T_h + C_o T_r$$

Where V and f are, respectively, the cutting speed and feed, while D and L are the outside diameter and length of the part, respectively. C_o is the operating cost in \$/min, C_t is the tool cost per cutting edge in \$/edge, T_{cs} is the tool change time in min/edge, T_h is the loading and unloading time in min/piece, T is tool life in min/edge.

Taylor's expanded tool life equation is

$$V * f^a * d^b * T^c = K$$

Where a, b, c and K are empirical constants and d is the depth of cut.

Thus, the total cost of production as an objective function can be written as:

$$C_u = C_o * V^{-1} * f^{-1} + A * V^{(1/c-1)} * f^{(a/c-1)} * d^{(b/c)} * K^{(-1/c)} * (C_o * T_{cs} + C_t) + C_o * (T_h + T_r) \dots \dots \dots (1)$$

Where $A = \pi * D * L / 1000$.

The total time required to produce a part is the sum of the times necessary for machining, work piece handling, tool changing and tool quick return and thus can be written as :

$$\text{Total time} = T_u = T_m + T_h + \frac{T_m T_s}{T} + T_r \quad \dots\dots\dots(2)$$

For the multi-objective problem, the objective function consists of the sum of the production cost and the production time along with different weight coefficients for each criterion:

$$\mu(V, f, d) = w_1 * C_u + w_2 * \lambda * T_u$$

Where w_1 and w_2 are the weight coefficients representing the relative importance of the production cost and the total production time criteria, respectively.

These weight coefficients satisfy the following condition:

$$w_1 + w_2 = 1, \quad 0 \leq w_1 \leq 1 \text{ and } 0 \leq w_2 \leq 1$$

The objective function would provide the optimum of the individual production cost or time criteria by setting the corresponding weight coefficient equal to zero. The optimum multi-objective function is normalized through the use of a constant multiplier, λ :

$$\lambda = C_{u\min} / T_{u\min}$$

where, $C_{u\min}$ and $T_{u\min}$ are the minimum production cost and the minimum production time, respectively, under the defined process constraints. The values are determined by putting the optimum values of the cutting speed V_{opc} and V_{opt} respectively, in equations (1) and (2), for the highest possible feed f_h . For V_{opc} and V_{opt} , we have:

$$V_{opc} = K / f_h^a * d^b [(1/c-1) * (t_{cs} + c_t / c_o)]^c$$

$$V_{opt} = K / f_h^a * d^b [(1/c-1) * (t_{cs})]^c$$

4.1.2 CONSTRAINTS

Practical limitations of the actual cutting conditions always exist for the optimization of the objective function.

1. FEED

The maximum allowable feed has a pronounced effect on both maximum spindle speed and production rate. Feed changes have a more significant impact on tool life than depth of cut changes. The system energy requirement reduces with feed since the optimum speed becomes lower. Therefore, the largest possible feed consistent with the available machine power and surface finish is desirable in order for the machine to be fully utilized. It is often possible to obtain much higher metal removal rates without reducing tool life by increasing the feed and decreasing the cutting speed. This technique is particularly useful for roughing cuts where the maximum feed is dependent on the maximum tool force the machine tool is able to withstand.

In general, the maximum feed in a roughing operation is limited by the maximum force that the cutting tool, machine tool, workpiece, and the fixture are able to withstand. The maximum feed in a finish operation is limited by the surface finish requirement and can be often predicted to a certain degree based on the surface finish and tool nose radius.

2. SPEED

Cutting speed has a greater effect on the tool life than either depth of cut or feed. When compared, the cutting speed has only a secondary effect on the chip-breaking. There are certain combinations of speed and feed, which are preferred for the easy chip-removal and are mainly dependent on the type of the tool and the workpiece material.

The following physical constraints are considered in the formulation of the objective model :

- ❖ **Feed and Speed Limitations** : Maximum and minimum permissible feed rate and cutting speed::

$$f_{\min} \leq f \leq f_{\max} ,$$

$$V_{\min} \leq V \leq V_{\max} ,$$

- ❖ **Power Limitation** : The power consumption allowed on the steel material is given as a function of feed, speed and depth of cut::

$$0.0373 * V^{0.9} * f^{0.78} * d^{0.75} \leq HP_{\max} ,$$

- ❖ **Surface Roughness Limitation** : The surface roughness allowed for the steel material is given as a function of feed, speed and depth of cut::

$$14785 * V^{-0.52} * f^{1.004} * d^{0.25} \leq SR_{\max} ,$$

- ❖ **Temperature Constraint** : The temperature constraint given by inequality is ::

$$74.96 * V^{0.4} * f^{0.2} * d^{0.1025} - 17.8 \leq T_{\max} ,$$

- ❖ **Cutting Force Constraint** : Constraint for the maximum cutting force allowed is::

$$844 * V^{-0.103} * f^{0.725} * d^{0.75} \leq F_{\max}$$

4.2 GA IMPLEMENTATION

In the section, GA has been developed to obtain the optimal solution from the objective functions and various constraints that we have discussed in the problem formulation:

4.2.1 CHROMOSOME REPRESENTATION

The genes or process variables of the solution are coded first. The values for the string size, population size and the maximum number of generations to be used are found through the experimentation. The values giving best results are found to be 30 for the length of each string, 60 for the population size and 240 for the maximum no. of generation.

4.2.2 INITIALIZATION

Initialization involves the formation of an initial population of chromosomes wherein each gene of a chromosome is obtained randomly by using the random number generator.

4.2.3 EVALUATION OF CHROMOSOMES

Each chromosome of the population is then evaluated to get its fitness function and the various constraints values. A penalty operator for each constraint is included in the fitness function so as to account the situation when constraint crosses its extreme limit. Thus for the objective function $F(x)$, we have the fitness function [13]:

$$P(x) = F(x) + u_1 \langle t(x) \rangle^2 + u_2 \langle f(x) \rangle^2 + u_3 \langle p(x) \rangle^2 + u_4 \langle r(x) \rangle^2$$

where u_j is penalty coefficient, whose value is calculated through experimentation. Here, $t(x)$, $f(x)$, $p(x)$ and $r(x)$ are the temperature, force, power and the surface roughness constraints. Whenever any constraint crosses its extreme limit, the square of its value

multiplied with penalty coefficient gets added to objective function so as to reduce the value of the fitness function to zero. The values of penalty coefficients calculated through experiments are $u_1 = 100$, $u_2 = 100$, $u_3 = 1000$ and $u_4 = 1000$.

Then the statistics for the each chromosome, which involves the sum of fitness values, average, probability of selection is done.

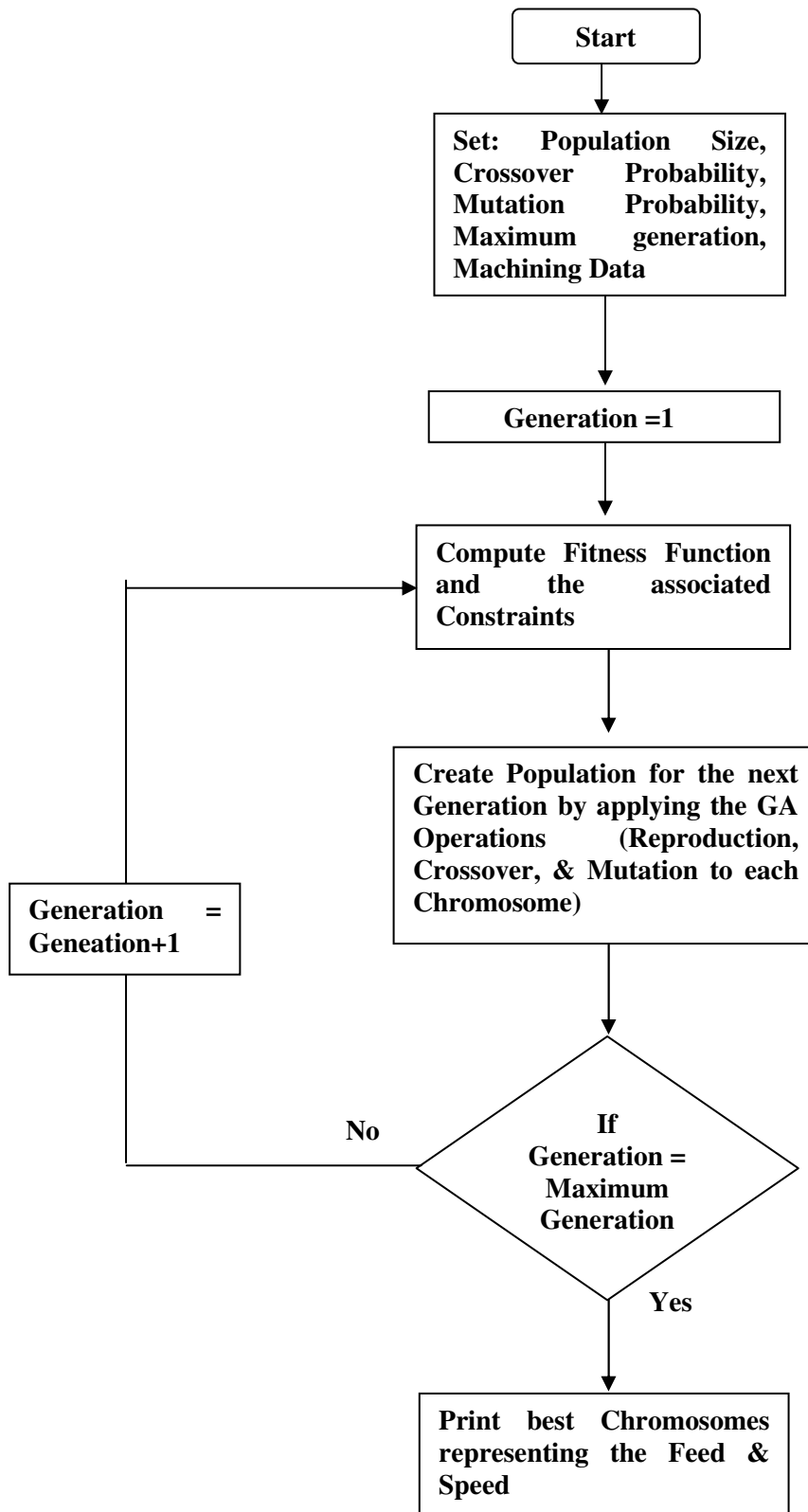
4.2.4 CROSSOVER AND MUTATION

A new population of offsprings is generated using crossover and mutation operators. The parents for crossover are selected from the previous population of chromosomes on the basis of the statistics and the selection operator in which the probability of selection of each parent is directly proportional to its fitness values. The crossover operator is applied on the mating sites of the parents. Then the mutation operator is applied so as to avoid the entrapment in the local optima. Then a complete new population is obtained.

4.2.5 TERMINATION

Unless the generation reaches its maximum value, the above procedure is repeated over and again to produce subsequent generations. The procedure gets terminated when (generation = maximum generation). Then we can pick the best solution from the latest solution.

4.3 FLOW CHART OF GA FOR MACHINING OPTIMIZATION PROBLEM



CHAPTER 5

RESULTS AND CONCLUSION

In this chapter, the various results related to the optimization of machining parameters have been discussed. The results are taken for two depth of cuts i.e. $doc = 2.54$ mm and $doc = 5.08$ mm, applied to the various objective functions. Here three objective functions i.e. the total production time, total production cost and combined of these two, has been taken.

Machining parameters used for the example are::

Parameter	Value	Parameter	Value
L	203 mm	a	0.29
D	152 mm	b	0.35
V_{min}	30 m/min.	c	0.25
V_{max}	200 m/min.	K	193.3
f_{min}	0.2540 mm/rev.	T_{cs}	0.50 min/edge.
f_{max}	0.7620 mm/rev.	T_r	0.13 min/pass.
SR_{max}	A	T_h	1.50 min/piece.
HP_{max}	B	C_o	0.10 \$/min.
F_{max}	C	C_t	0.50 \$/edge.
T_{max}	D		

Here the constraints surface roughness, power, force and temperature have given values A, B, C and D respectively. In the next sections, the various results will be discussed by taking the different values of these constraints.

In the section 5.1, the total production time is taken as an objective function with depth of cut, $doc = 2.54$ mm and the constraints force, surface roughness, temperature and power.

Machining parameters used for the example are::

Parameter	Value
SR_{max}	8 μm
P_{max}	4 KW
F_{max}	600 N
T_{max}	400 deg C

The table 5.1(a), shows the values of randomly selected machining parameters, the associated fitness values and the various constraints at the starting generation. After applying the various GA operations, we get the table 5.1(b), that shows the values of above stated variables at the end generation.

It is clear from these tables that the value of fitness function becomes zero, when the constraints cross their extreme limits. These both tables are also graphically plotted in fig. 5.1(a) to fig. 5.1(d).

Fig. 5.1(e) and fig. 5.1(f), shows the variation of best fitness function and the objective function values with generation, respectively. These figures clearly show how the values of both these functions get improved with generation, after applying the GA operations. From fig. 5.1(f), the best value of the objective function i.e. the total production time is approximated to be 4.41001081 min. It is clear from table 5.1(b) that the constraints surface roughness = 7.18585 μm , force = 554.72638 N and temperature = 399.17020 deg C have their extreme limits for the calculated best objective function value.

From fig. 5.1(g), that we have from J. S. Agapiou [6], the value of objective function lies at point A (less than 5 min) that justifies our objective function value.

5.1 TOTAL PRODUCTION TIME AS AN OBJECTIVE FUNCTION with doc = 2.54mm

TABLE 5.1(a)

Accumulated Statistics for Generation ---> 0

```

*****Calculated Constraints*****
FEED      SPEED      FITNESS      POWER      ROUGNESS      TEMP      FORCE
*****
1)  0.265398  175.937546  0.000000    2.79767    1.90405    483.68732  384.44864
2)  0.368651  164.810791  0.000000    3.40864    2.92479    503.94052  491.11554
3)  0.707231  154.328079  0.000000    5.34063    6.21660    561.13177  792.88513
4)  0.277501  113.571846  0.000000    1.95355    3.87308    406.91574  415.08380
5)  0.353852  96.545815  0.000000    2.04021    6.32779    400.02536  503.28018
6)  0.472962  33.475842  0.000000    0.98618    42.36076    272.06448  691.45142
7)  0.711192  138.368027  0.000000    4.86201    7.37989    537.01575  804.95435
8)  0.651704  190.695023  0.000000    6.06176    4.15165    602.04474  731.40137
9)  0.387555  119.104492  0.000000    2.64588    5.03855    444.98053  526.28137
10) 0.492019  110.423180  0.000000    2.97738    7.18337    453.13144  630.51129
11) 0.665699  154.542709  0.000000    5.10076    5.83777    554.48468  758.74115
12) 0.484704  160.232910  0.000000    4.11417    4.01815    527.12061  600.61646
13) 0.494961  91.315140  0.000000    2.52109    9.64615    419.18689  645.54816
14) 0.493255  179.400391  0.000000    4.61712    3.44399    554.31158  601.35675
15) 0.491475  156.755234  0.000000    4.07760    4.21269    523.85925  608.03699
16) 0.516609  155.135895  0.000000    4.19992    4.49947    527.02167  631.08917
17) 0.601101  84.331436  0.000000    2.73089    13.23088    422.27063  749.20697
18) 0.409431  152.891190  0.000000    3.45764    3.64249    499.24252  533.97498
19) 0.451691  184.893066  0.000000    4.42934    3.01142    551.14954  562.45667
20) 0.405126  78.410904  0.000010    1.88015    9.94484    377.20782  566.98322
21) 0.587060  76.430313  0.000000    2.45384    15.00455    403.29477  743.85382
22) 0.563392  67.814285  0.000000    2.13381    17.26774    380.33258  730.79004
23) 0.597078  131.112030  0.000000    4.04126    6.71968    506.52472  712.97296
24) 0.480172  69.253204  0.000000    1.91964    14.24570    371.05927  649.44745
25) 0.720388  85.014328  0.000000    3.16795    15.67467    439.96994  853.58325
26) 0.522766  174.428543  0.000000    4.71053    3.81023    554.52881  629.02026
27) 0.418351  135.793015  0.000000    3.16028    4.45741    477.41769  548.93884
28) 0.634586  69.288139  0.000000    2.38709    18.83339    393.44321  794.90350
29) 0.344363  167.934296  0.000000    3.28725    2.65450    500.75650  466.54953
30) 0.712110  138.465622  0.000000    4.87000    7.38155    537.31549  805.65033
31) 0.729286  32.286057  0.000000    1.33816    69.13161    293.74640  949.96069
32) 0.569894  82.386620  0.000000    2.56522    12.99407    413.55881  722.50745
33) 0.641435  87.315018  0.000000    2.96410    13.39540    434.26746  782.56622
34) 0.595076  150.749207  0.000000    4.57015    5.41693    536.25598  701.25433
35) 0.274393  75.849586  0.392977    1.34655    7.07339    342.77292  428.89325
36) 0.587354  76.946098  0.000000    2.46970    14.85941    404.47147  743.61719
37) 0.707795  56.659851  0.000000    2.16875    28.53373    370.01880  878.10016
38) 0.633645  166.084961  0.000000    5.23687    4.97945    565.42816  726.75287
39) 0.417891  185.984482  0.000000    4.19076    2.76041    543.68805  531.30115
40) 0.451644  113.705063  0.000000    2.85942    6.30464    450.59079  590.80573
41) 0.546790  144.663055  0.000000    4.12245    5.29734    518.05121  662.28235
42) 0.522768  98.583450  0.000000    2.81863    9.07047    437.73364  666.45245
43) 0.281335  119.956047  0.000000    2.07419    3.61358    417.50220  416.91788
44) 0.509273  136.066681  0.000000    3.69090    5.41384    497.69907  632.93280
45) 0.580263  120.321571  0.000000    3.65823    7.44024    485.93192  704.46088
46) 0.452371  83.005196  0.000000    2.15682    10.18841    395.32184  610.65503
47) 0.709183  73.238640  0.000000    2.73648    19.35467    412.11722  856.77966
48) 0.445151  166.812454  0.000000    3.99186    3.47012    526.61487  562.37225
49) 0.396755  114.283096  0.000000    2.59636    5.49305    439.53491  537.55481
50) 0.395401  190.531403  0.000000    4.10198    2.51714    542.90100  509.16626
51) 0.516358  125.885933  0.000000    3.47869    6.17828    483.29285  644.36145
52) 0.287945  31.923386  0.000001    0.64164    27.66502    239.73877  484.84283
53) 0.529086  59.035137  0.000000    1.79343    20.01530    354.15176  708.12640
54) 0.720278  95.229164  0.000000    3.50814    13.18954    461.21063  843.73486
55) 0.260188  33.414845  0.000002    0.61774    23.31256    239.22202  448.41052
56) 0.685605  197.917953  0.000000    6.52091    4.12848    617.74451  755.94000
57) 0.459890  189.774918  0.000000    4.59853    2.94721    559.18365  568.33783
58) 0.524591  37.749146  0.000000    1.19127    39.15896    292.70181  736.37189
59) 0.461275  154.051361  0.000000    3.82051    4.05876    513.32312  581.73853
60) 0.402880  158.939590  0.000000    3.53574    3.37873    505.63794  525.69720

```

max=0.392977 min=0.000000 avg=0.006550 sum=0.392992 no_mutation=0 no_cross=0

```

FEED      0.274393
SPEED     75.849586
FITNESS   0.392977

```

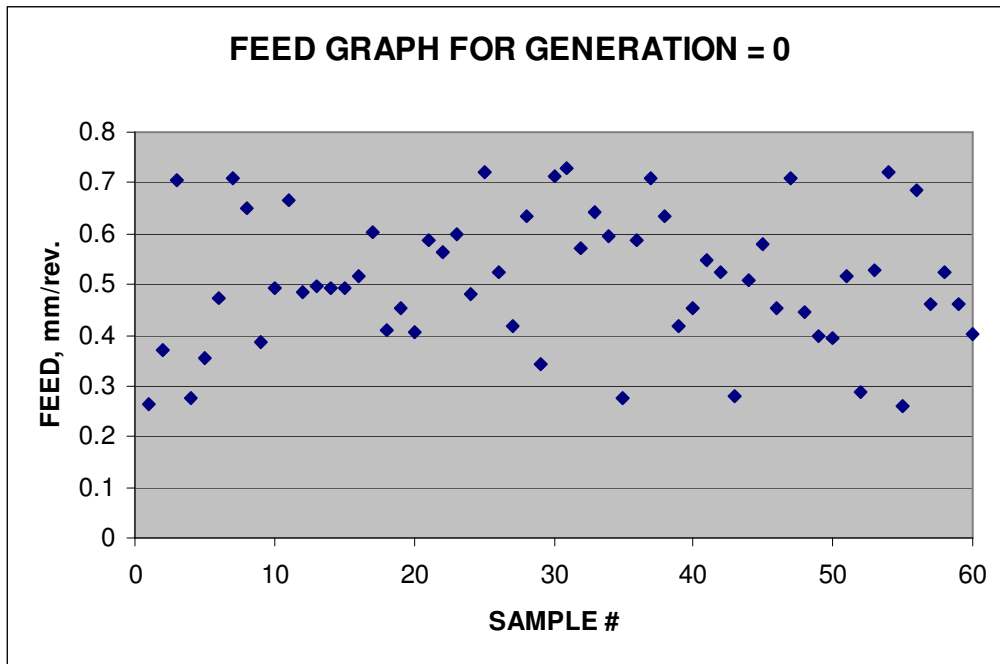


FIG. 5.1 (a)

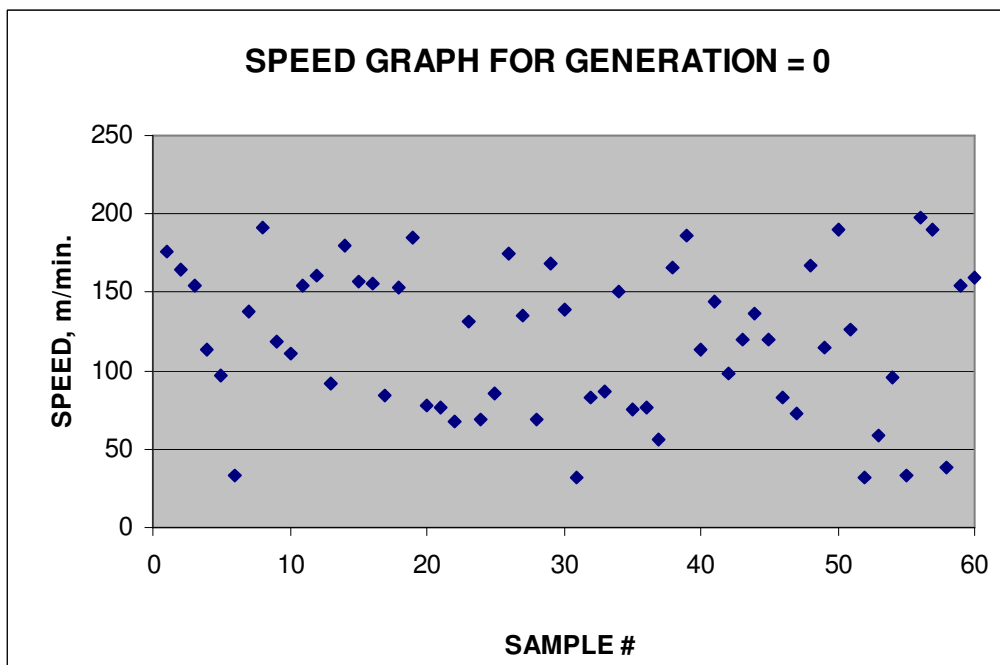


FIG. 5.1 (b)

Fig. 5.1 Speed and feed graphs for starting generation with doc = 2.54mm

TABLE 5.1(b)

Accumulated Statistics for Generation ---> 240

```

*****Calculated Constraints*****
FEED      SPEED      FITNESS    POWER      ROUGHNESS  TEMP      FORCE
*****
1)  0.375904  91.115112  0.474351  1.87830   6.90060   386.29996  498.64789
2)  0.367274  89.691856  0.468479  1.72542   6.42043   376.67111  466.84549
3)  0.345866  89.830795  0.459197  1.87392   6.99879   385.62106  500.56079
4)  0.347882  91.115112  0.462216  1.91110   6.79283   389.07382  500.03418
5)  0.375160  89.465988  0.471436  1.99395   7.53395   392.25635  529.14117
6)  0.334824  89.039345  0.452653  2.08532   7.46118   398.76367  538.78033
7)  0.375663  90.048653  0.472576  2.00774   7.47003   393.43286  529.30798
8)  0.344063  90.631027  0.459676  1.88565   6.77258   387.31244  496.31622
9)  0.347387  89.258080  0.458948  1.87392   6.99878   385.62128  500.56073
10) 0.367275  84.601303  0.000016  1.86495   8.02911   381.48785  524.01385
11) 0.335940  90.616554  0.455826  1.85057   6.61364   385.35538  487.80048
12) 0.375160  89.465988  0.471436  1.99395   7.53395   392.25635  529.14117
13) 0.375774  90.710060  0.473665  2.02147   7.38958   394.66266  529.02850
14) 0.347387  46.763103  0.000003  1.04733  18.69620   293.70218  534.43652
15) 0.333830  89.472473  0.452904  1.82056   6.70010   382.80646  486.20270
16) 0.376656  90.658424  0.473947  2.02413   7.41340   394.76205  529.95874
17) 0.336436  89.604828  0.454383  1.83407   6.73746   383.66730  488.87833
18) 0.335603  81.067444  0.438477  1.67279   7.82551   367.71472  492.97583
19) 0.268090  79.288788  0.396434  1.37621   6.45984   347.52383  419.83749
20) 0.392069  91.692383  0.481686  2.49519   7.18585   399.17020  554.72638
21) 0.375904  89.656906  0.472051  2.00087   7.52453   392.76880  529.78735
22) 0.333830  68.222473  0.000010  1.42632  10.11764   341.62900  499.74280
23) 0.279904  89.288353  0.423411  1.58386   5.63143   368.61752  427.98999
24) 0.347386  83.945450  0.449641  1.77323   7.68298   375.83936  503.68146
25) 0.344163  92.311913  0.462420  1.91753   6.58793   390.32486  495.49716
26) 0.448093  91.747498  0.000000  2.34281   8.66683   411.38889  600.34229
27) 0.327621  90.045982  0.450828  1.80444   6.51145   382.32651  479.31985
28) 0.439274  91.691132  0.000000  2.30549   8.50352   409.58093  591.78937
29) 0.379136  83.945450  0.000014  1.89842   8.38812   382.78534  536.65283
30) 0.347820  83.945450  0.449845  1.77496   7.69262   375.93768  504.13766
31) 0.343417  91.747498  0.461179  1.90375   6.63517   389.14835  495.02618
32) 0.321093  89.025848  0.445811  1.75821   6.49266   378.90695  472.92178
33) 0.343419  89.025200  0.456717  1.85285   6.94605   384.27518  496.54092
34) 0.312226  90.051247  0.442975  1.73804   6.20371   378.50241  462.87909
35) 0.347389  91.649178  0.462846  1.91905   6.72316   389.91031  499.22403
36) 0.376620  89.465828  0.472041  2.00000   7.56341   392.57480  530.63373
37) 0.347387  91.115112  0.461990  1.90897   6.78311   388.95786  499.51767
38) 0.343402  172.426010  0.000000  3.35894  2.54296   505.96777  464.36221
39) 0.279904  78.715363  0.402719  1.41402   6.82050   349.61990  433.48917
40) 0.375636  89.049835  0.470963  1.98757   7.59721   391.59631  529.87872
41) 0.347847  42.509823  0.000002  0.96218  21.64111   282.12344  540.14203
42) 0.371199  83.903946  0.000015  1.86651   8.21799   381.01489  528.51007
43) 0.367275  80.033424  0.000013  1.77407   8.73592   372.72061  526.96906
44) 0.312660  91.628418  0.445860  1.76733   6.05057   381.37521  462.53131
45) 0.375665  90.712715  0.473625  2.02107   7.38711   394.64368  528.91620
46) 0.375664  90.048653  0.472576  2.00774   7.47003   393.43286  529.30804
47) 0.375160  89.548996  0.471570  1.99562   7.52334   392.40848  529.09143
48) 0.343404  87.426003  0.453981  1.82280   7.13977   381.36682  497.43732
49) 0.343417  90.624458  0.459365  1.88277   6.76055   387.14847  495.64413
50) 0.375665  89.913788  0.472363  2.00504   7.48711   393.18680  529.39038
51) 0.329031  91.747498  0.454334  1.84125   6.35612   385.68008  479.90286
52) 0.375266  89.465988  0.471481  1.99439   7.53609   392.27954  529.24957
53) 0.347843  112.932098  0.000000  2.31819  4.90112   425.54379  489.23764
54) 0.343417  110.952232  0.000000  2.25891  4.97037   421.29248  485.58658
55) 0.347389  91.649178  0.462846  1.91905   6.72316   389.91031  499.22403
56) 0.375160  89.465988  0.471436  1.99395   7.53395   392.25635  529.14117
57) 0.376620  89.465828  0.472041  2.00000   7.56341   392.57480  530.63373
58) 0.375160  89.465988  0.471436  1.99395   7.53395   392.25635  529.14117
59) 0.347387  89.257919  0.458948  1.87392   6.99879   385.62097  500.56082
60) 0.335603  81.067444  0.438477  1.67279   7.82550   367.71466  492.97552

```

max=0.481686 min=0.000 avg=0.366902 sum=22.014145 no_mutation=17185 no_cross=4308

```

FEED      0.392069
SPEED    91.692383
FITNESS  0.481686

```

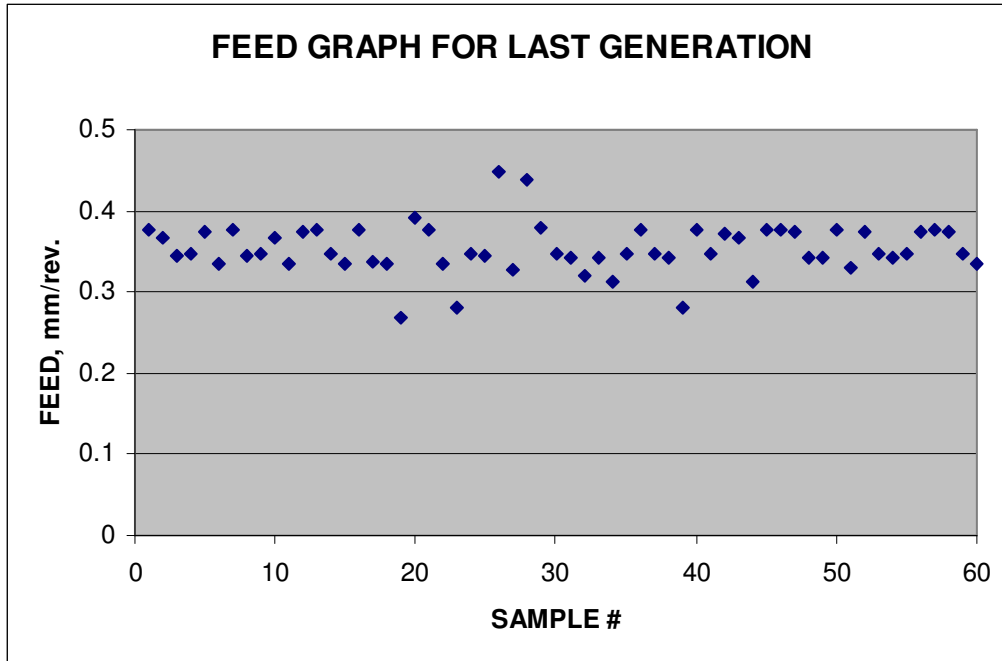


FIG. 5.1 (c)

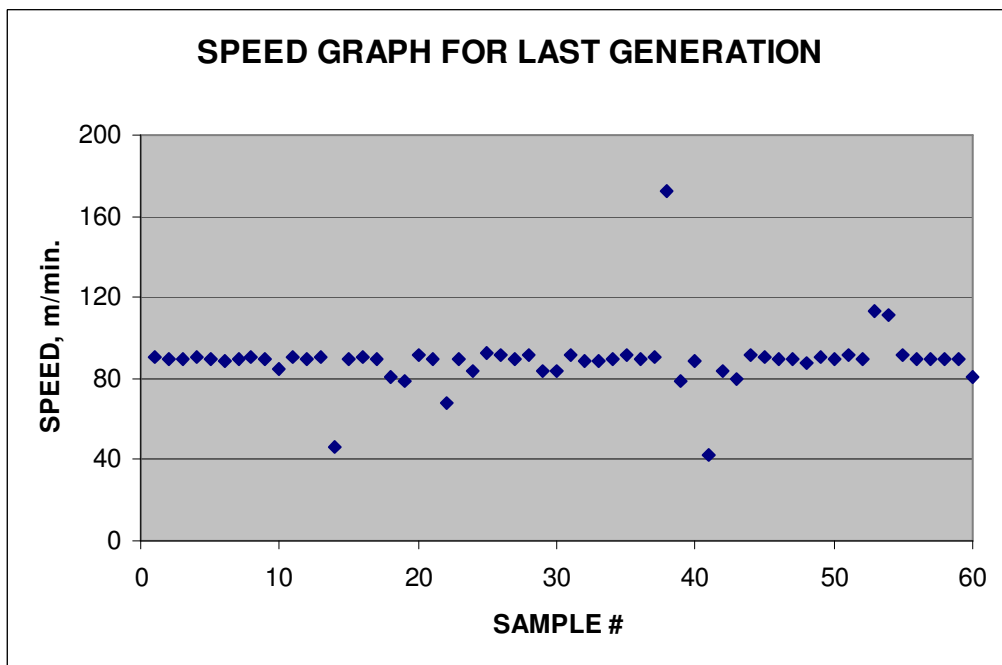


FIG. 5.1 (d)

Fig. 5.1 Speed and feed graphs for last generation with doc = 2.54mm

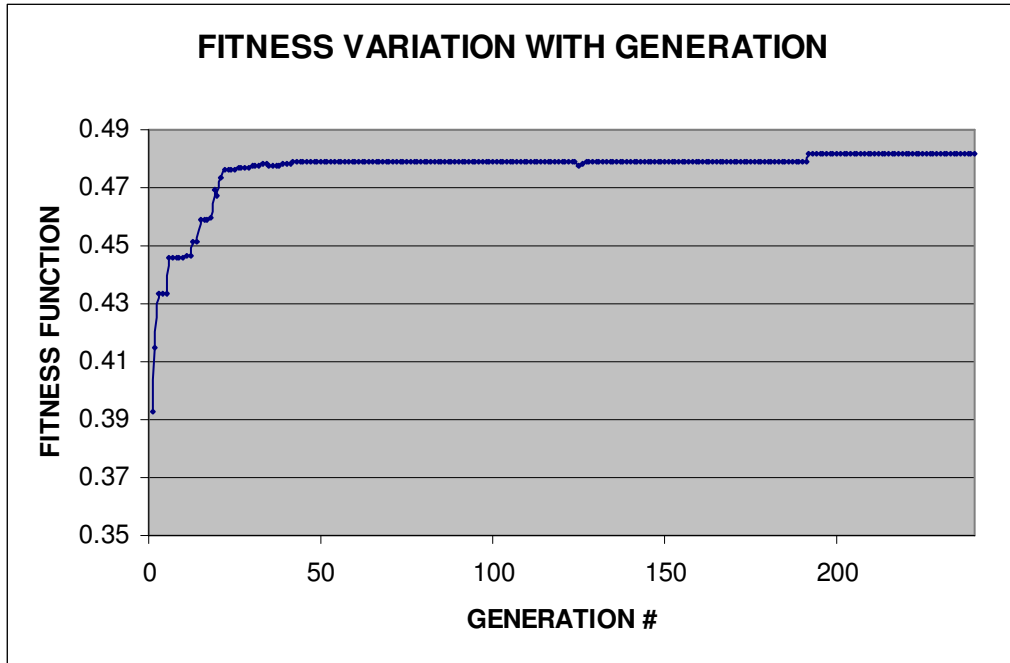


FIG. 5.1 (e)

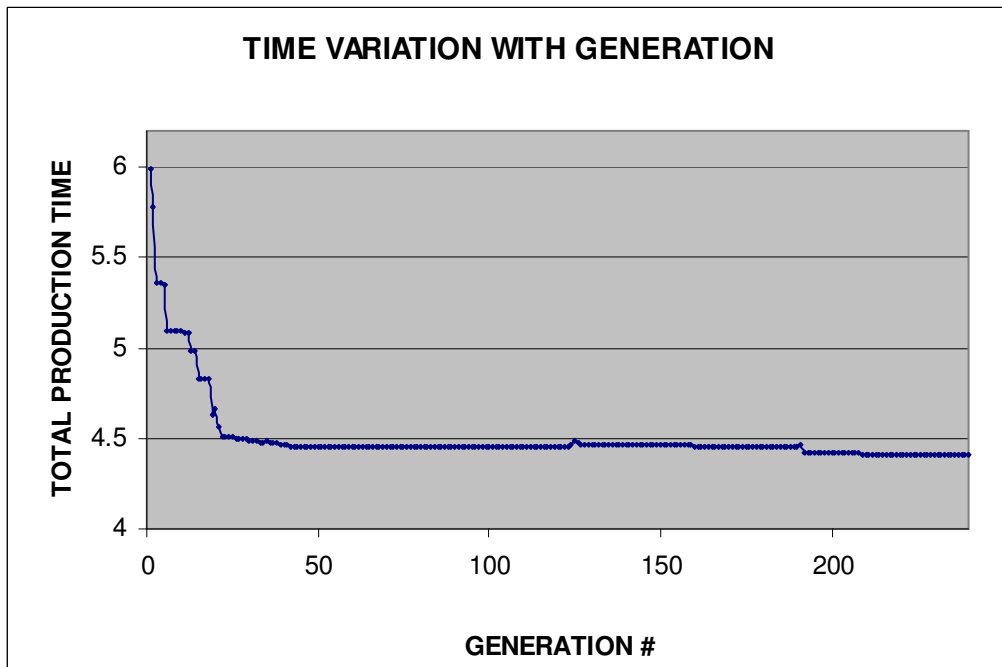


FIG. 5.1 (f)

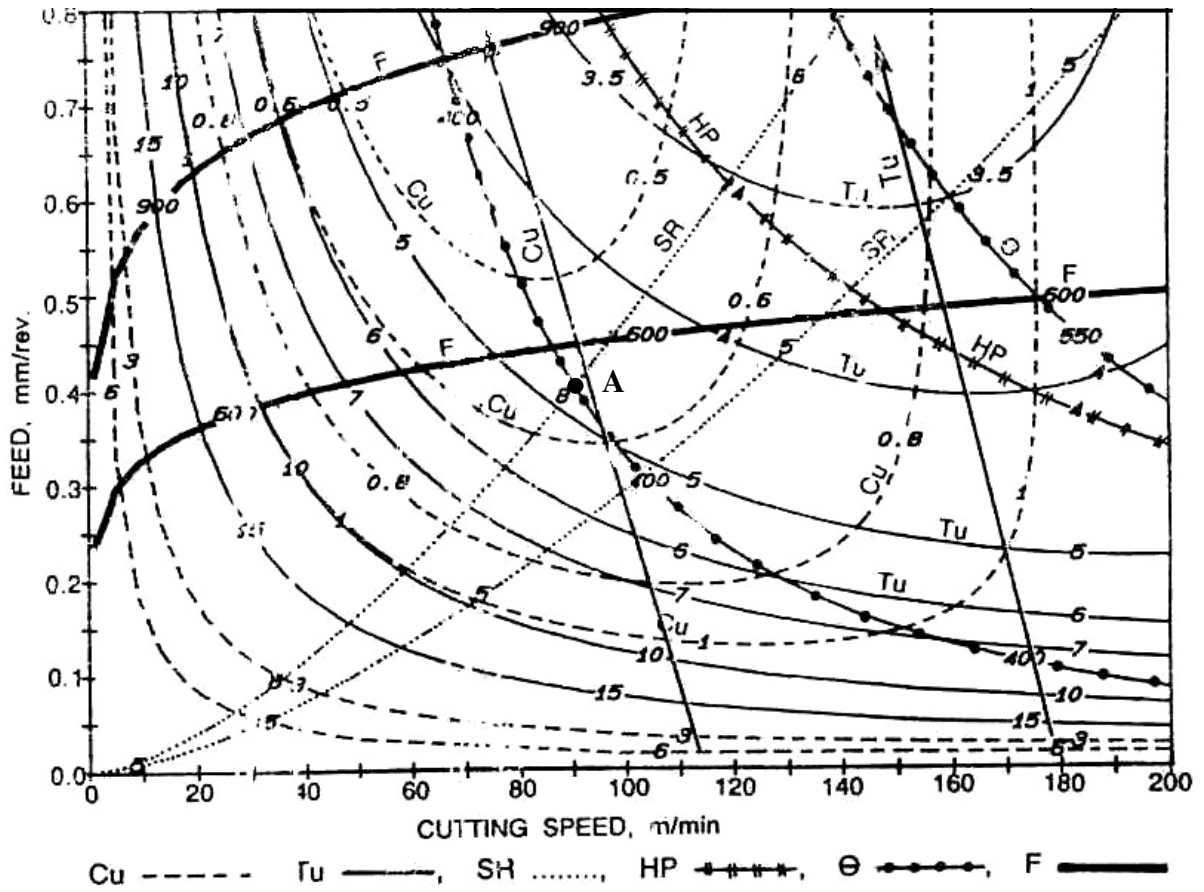


FIG. 5.1(g) Location of best result found by GA on the contours given by Agapiou [6], for $d_{oc} = 2.54$ mm and the constraints of power, force, surface roughness, and temperature.

In the section 5.2, the total production time is taken as an objective function with depth of cut, $doc = 5.08$ mm and the constraints force, surface roughness, temperature and power.

Machining parameters used for the example are::

Parameter	Value
SR_{max}	$8\mu m$
HP_{max}	5KW
F_{max}	1200N
T_{max}	400 deg C

It is clear from tables 5.2(a) and 5.2(b) that the value of fitness function becomes zero, when the constraints cross their extreme limits. These both tables are also graphically plotted in fig. 5.2(a) to fig. 5.2(d).

Fig. 5.2(e) and fig. 5.2(f), shows the variation of best fitness function and the objective function values with generation, respectively. These figures clearly show how the values of both these functions get improved with generation, after applying the GA operations. From fig. 5.2(f), the best value of the objective function i.e. the total production time is approximated to be 5.44656 min. It is clear from table 5.2(b) that the constraints surface roughness = $7.97880 \mu m$ and temperature = 394.33133 deg C have their extreme limits for the calculated best objective function value.

From fig. 5.2(g), that we have from J. S. Agapiou [6], the value of objective function lies at point B (less than 6 min) that justifies our objective function value.

5.2 TOTAL PRODUCTION TIME AS AN OBJECTIVE FUNCTION with doc = 5.08mm

TABLE 5.2(a)

Accumulated Statistics for Generation ---> 0
 *****Calculated Constraints*****

	FEED	SPEED	FITNESS	POWER	ROUGHNESS	TEMP	FORCE
1)	0.601896	149.667526	0.000000	7.70457	6.58769	577.72589	1190.01672
2)	0.527198	113.823242	0.000000	5.43068	8.74335	501.99533	1111.41150
3)	0.270287	154.535706	0.000000	4.24675	2.80877	496.15115	663.84216
4)	0.290274	141.421555	0.000000	4.14535	3.45274	485.36823	705.38983
5)	0.314289	108.783211	0.000000	3.48280	5.57226	442.49451	767.36133
6)	0.709576	108.464958	0.000000	6.55611	12.67798	523.27917	1385.28638
7)	0.671191	46.700748	0.000000	2.94061	43.15869	364.18295	1449.10876
8)	0.519633	195.971603	0.000000	8.75636	3.77323	626.31262	1040.92847
9)	0.665176	155.502121	0.000000	8.62104	6.87189	599.11743	1274.51843
10)	0.430016	159.317413	0.000000	6.26991	4.27431	553.08350	926.67468
11)	0.704758	93.228828	0.000000	5.69080	15.84905	490.79654	1399.76123
12)	0.395009	59.706654	0.000003	2.42594	17.44722	361.23190	962.43018
13)	0.504574	74.656189	0.000000	3.59044	15.88415	417.46786	1123.61975
14)	0.266873	147.868607	0.000000	4.04122	2.96542	485.88220	660.69763
15)	0.284507	154.480118	0.000000	4.41859	2.95876	501.37384	689.00836
16)	0.541538	39.574612	0.000000	2.14295	44.74839	324.68198	1261.25513
17)	0.265586	159.109161	0.000000	4.30044	2.64006	500.36075	653.51825
18)	0.415806	62.776356	0.000003	2.64154	17.02171	372.89856	993.84589
19)	0.336536	59.330444	0.000004	2.12883	14.99841	348.35306	857.44293
20)	0.696105	182.985504	0.000000	10.34113	5.61642	646.62653	1295.67725
21)	0.476496	31.923330	0.000000	1.59842	54.55246	288.53766	1174.80847
22)	0.581488	171.727509	0.000000	8.48798	5.16333	607.06958	1144.57190
23)	0.717919	107.619682	0.000000	6.56974	12.98110	522.85101	1398.18384
24)	0.260627	135.821854	0.000000	3.67514	3.29501	466.74823	655.06512
25)	0.541009	193.130066	0.000000	8.91807	4.01728	627.74432	1073.38794
26)	0.416957	144.553726	0.000000	5.60796	4.80413	527.92688	915.15741
27)	0.685347	194.900528	0.000000	10.81306	5.02372	661.48584	1272.96716
28)	0.757890	77.180283	0.000000	5.08107	22.71966	460.68573	1504.00781
29)	0.695064	182.565384	0.000000	10.30772	5.62761	645.81714	1294.57288
30)	0.663895	177.339615	0.000000	9.68878	5.61681	632.16113	1255.90881
31)	0.728978	67.585785	0.000000	4.37415	26.73451	432.42569	1481.98474
32)	0.711330	120.021751	0.000000	7.19542	10.89661	545.92004	1373.60791
33)	0.273794	130.023682	0.000000	3.67212	3.69953	463.08255	681.90204
34)	0.477893	45.728088	0.000001	2.21386	31.68526	336.10333	1135.21619
35)	0.517391	171.940155	0.000000	7.75756	4.58340	592.94513	1051.51477
36)	0.633017	166.295761	0.000000	8.81056	5.90431	609.65240	1221.21204
37)	0.505782	177.379608	0.000000	7.83810	4.27300	597.80103	1031.09680
38)	0.486744	199.588150	0.000000	8.45907	3.43663	622.61182	990.89966
39)	0.506519	152.534561	0.000000	6.85050	5.38247	561.91119	1048.08557
40)	0.583818	105.598839	0.000000	5.49662	10.85595	497.03064	1205.85364
41)	0.726151	181.110077	0.000000	10.58902	5.95231	649.51013	1337.38110
42)	0.369985	103.618721	0.000000	3.78603	7.06769	448.59866	867.97968
43)	0.642848	47.710159	0.000000	2.89855	40.00734	364.15424	1401.44360
44)	0.389450	57.867855	0.000003	2.33266	18.03830	355.45917	955.61401
45)	0.277080	186.072372	0.000000	5.11744	2.17143	538.53845	663.30029
46)	0.587628	78.165901	0.000000	4.21427	17.26155	439.25943	1249.04138
47)	0.688636	185.771057	0.000000	10.39486	5.42978	649.21320	1283.61633
48)	0.435565	143.546280	0.000000	5.76581	5.07304	531.17499	945.25739
49)	0.398500	105.077202	0.000000	4.06255	7.45460	458.23004	914.68604
50)	0.561466	86.991112	0.000000	4.47823	14.01541	454.91550	1195.44812
51)	0.650304	74.220558	0.000000	4.35321	20.67566	439.05487	1351.34302
52)	0.430250	125.804352	0.000000	5.07148	6.12358	501.67865	949.48627
53)	0.628764	176.212204	0.000000	9.23335	5.37024	623.49402	1208.14832
54)	0.316410	131.499115	0.000000	4.15272	4.20510	479.43826	756.44104
55)	0.547799	195.628342	0.000000	9.11002	3.98920	632.69232	1081.72864
56)	0.354577	107.605789	0.000000	3.78907	6.39450	451.68488	838.40784
57)	0.692318	189.607254	0.000000	10.63199	5.29194	655.40668	1285.92371
58)	0.758101	185.827393	0.000000	11.20708	5.97705	662.24023	1376.20044
59)	0.291352	143.251266	0.000000	4.20573	3.39855	488.33719	706.36719
60)	0.431961	192.545975	0.000000	7.46165	3.21945	598.57928	912.04132

max=0.000004 min=0.000000 avg=0.000000 sum=0.000017 no_mutation=0 no_cross=0

FEED 0.336536
 SPEED 59.330444
 FITNESS 0.000004

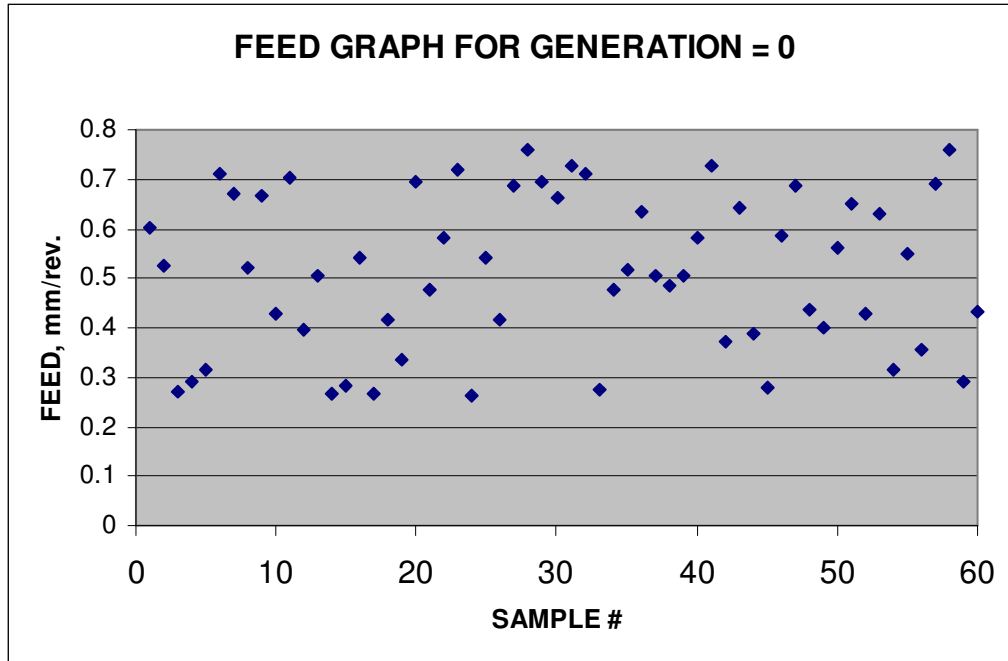


FIG. 5.2 (a)

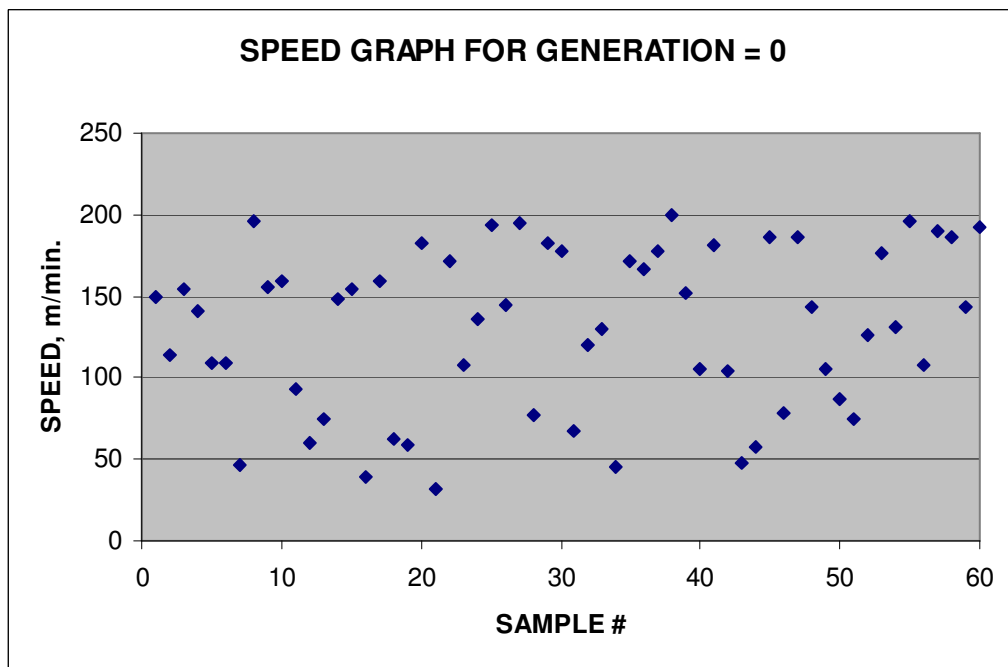


FIG. 5.2 (b)

Fig. 5.2 Speed and feed graphs for starting generation with doc = 5.08mm

TABLE 5.2(b)

Accumulated Statistics for Generation ---> 240

```

*****Calculated Constraints*****
FEED      SPEED      FITNESS      POWER      ROUGHNESS      TEMP      FORCE
*****
 1)  0.292876  85.999023  0.420278  2.66787  7.42008  395.32318  746.65900
 2)  0.309557  86.024597  0.429376  2.69950  7.97880  394.33133  777.92627
 3)  0.293800  86.486893  0.000001  4.33965 13.84488  450.28546 1172.55408
 4)  0.295504  91.311440  0.000000  2.68808  7.37983  396.51981  747.93616
 5)  0.294052  86.178932  0.421234  2.68125  7.42634  395.99991  748.67114
 6)  0.293748  85.914803  0.420626  2.67170  7.45333  395.40674  748.34314
 7)  0.309549  87.352722  0.000000  2.82504  7.66018  402.54095  776.01056
 8)  0.293125  85.997719  0.420415  2.66960  7.42657  395.39084  747.11987
 9)  0.298703  86.082436  0.423650  2.71154  7.55715  397.11490  757.32471
10)  0.294196  85.823067  0.420724  2.67231  7.47687  395.35602  749.25092
11)  0.293748  85.846901  0.420513  2.66980  7.46229  395.27606  748.40302
12)  0.292656  85.822792  0.419860  2.66138  7.43761  394.92209  746.40588
13)  0.292877  85.998367  0.420277  2.66786  7.42018  395.32214  746.66089
14)  0.277801  86.355331  0.412133  2.56968  6.99255  391.65628  718.29138
15)  0.294048  85.914803  0.420794  2.67383  7.46097  395.49106  748.89679
16)  0.294172  85.914803  0.420863  2.67471  7.46413  395.52591  749.12579
17)  0.357548  85.916420  0.000000  3.11441  9.07901  411.97635  862.94940
18)  0.292532  85.914803  0.419943  2.66307  7.42235  395.06400  746.90552
19)  0.301611  86.452652  0.425839  2.74269  7.58141  398.63394  762.33203
20)  0.308407  86.024597  0.428771  2.77833  7.81162  399.66403  775.13544
21)  0.293748  86.085632  0.420910  2.67648  7.43086  395.73517  748.19250
22)  0.294228  86.257217  0.421462  2.68470  7.42055  396.19977  748.92706
23)  0.294048  85.914803  0.420794  2.67383  7.46097  395.49106  748.89679
24)  0.298792  86.085640  0.423704  2.71226  7.55897  397.14572  757.48499
25)  0.300807  86.354683  0.425244  2.73419  7.57415  398.22293  760.94525
26)  0.285738  86.420502  0.416910  2.62855  7.18492  394.09412  733.05707
27)  0.298705  43.331703  0.000002  1.46191 21.45293  297.49435  811.86371
28)  0.294047  85.998779  0.420933  2.67617  7.44987  395.65234  748.82092
29)  0.297841  86.409111  0.423712  2.71467  7.49198  397.50375  755.44891
30)  0.356032  86.238075  0.000000  3.11456  8.98916  412.25363  859.96967
31)  0.309487  85.914803  0.429161  2.78271  7.85432  399.74271  777.20337
32)  0.277646  86.023300  0.411479  2.55967  7.02968  390.98019  718.28101
33)  0.298791  85.998741  0.423560  2.70980  7.57057  396.97800  757.56158
34)  0.295504  75.462135  0.000012  2.38837  9.13239  374.98016  761.52576
35)  0.293125  87.325844  0.422589  2.70668  7.25557  397.93158  745.96088
36)  0.309487  85.914803  0.429161  2.78271  7.85432  399.74271  777.20337
37)  0.300807  86.414345  0.425341  2.73589  7.56621  398.33786  760.89203
38)  0.292876  85.999016  0.420278  2.66787  7.42008  395.32318  746.65900
39)  0.294172  86.910896  0.422501  2.70260  7.33449  397.43613  748.25153
40)  0.298792  85.906082  0.423407  2.70717  7.58300  396.79932  757.64520
41)  0.298672  86.486839  0.424295  2.72279  7.50272  397.88489  756.90851
42)  0.348866  85.916946  0.000000  3.05528  8.85761  409.86975  847.70654
43)  0.292861  86.021881  0.420307  2.66840  7.41668  395.36267  746.60980
44)  0.309557  85.917107  0.429201  2.78327  7.85578  399.76599  777.32819
45)  0.295094  88.079681  0.424885  2.74198  7.20969  399.92227  748.93756
46)  0.298212  86.001862  0.423247  2.70578  7.55541  396.82297  756.49323
47)  0.294048  85.914803  0.420794  2.67383  7.46097  395.49106  748.89679
48)  0.298705  85.993828  0.423505  2.70905  7.56905  396.94467  757.40820
49)  0.334367  86.019745  0.000000  2.95896  8.47264  406.45721  821.91620
50)  0.294047  85.831795  0.420655  2.67150  7.47192  395.33102  748.96838
51)  0.293125  87.325844  0.422589  2.70668  7.25557  397.93158  745.96088
52)  0.298705  85.993828  0.423505  2.70905  7.56905  396.94467  757.40820
53)  0.307504  172.352722  0.000000  5.18092  2.70853  533.11261  720.91333
54)  0.485670  85.914803  0.000000  3.95470 12.34783  439.12057 1077.49805
55)  0.292876  85.999016  0.420278  2.66787  7.42008  395.32318  746.65900
56)  0.300807  86.414345  0.425341  2.73589  7.56621  398.33786  760.89203
57)  0.298672  86.486839  0.424295  2.72279  7.50272  397.88489  756.90851
58)  0.292470  86.024597  0.420091  2.66569  7.40638  395.25745  745.88434
59)  0.298703  85.916412  0.423376  2.70684  7.57935  396.79462  757.47284
60)  0.294228  86.736153  0.422247  2.69811  7.35836  397.11771  748.50708

```

max=0.429376 min=0.000000 avg=0.351944 sum=21.116669 no_mutation=17234 no_cross=4300

```

FEED      0.309557
SPEED    86.024597
FITNESS  0.429376

```

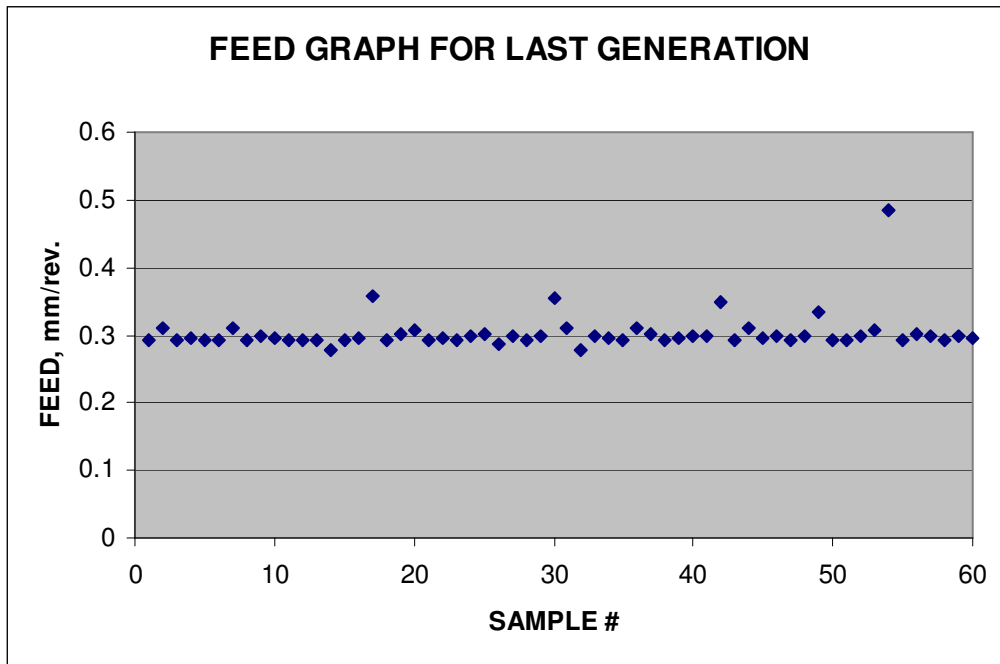


FIG. 5.2 (c)

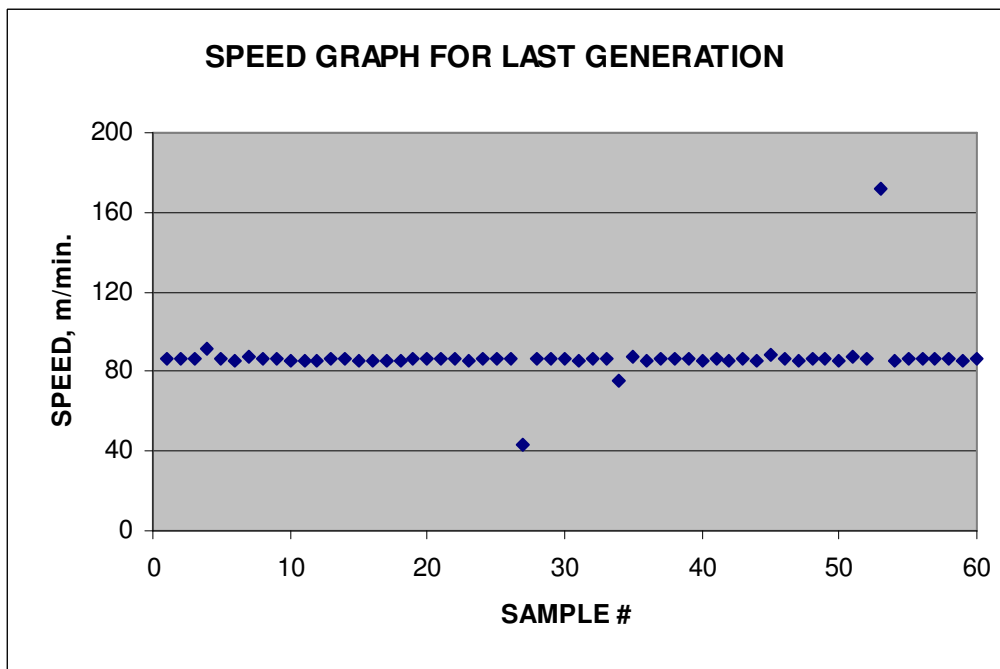


FIG. 5.2 (d)

Fig. 5.2 Speed and feed graphs for last generation with doc = 5.08mm

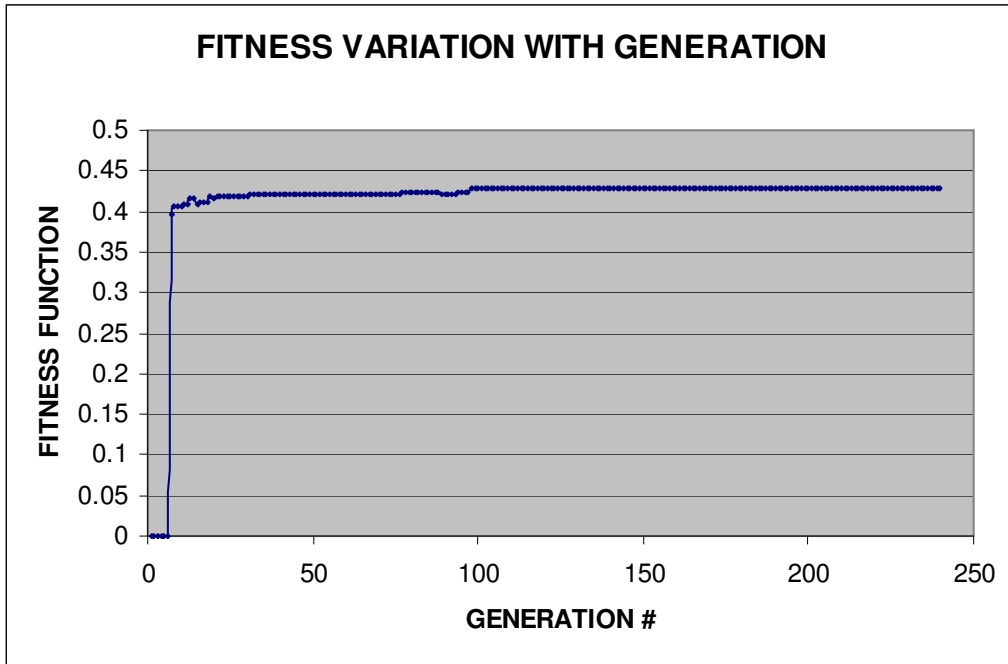


FIG. 5.2 (e)

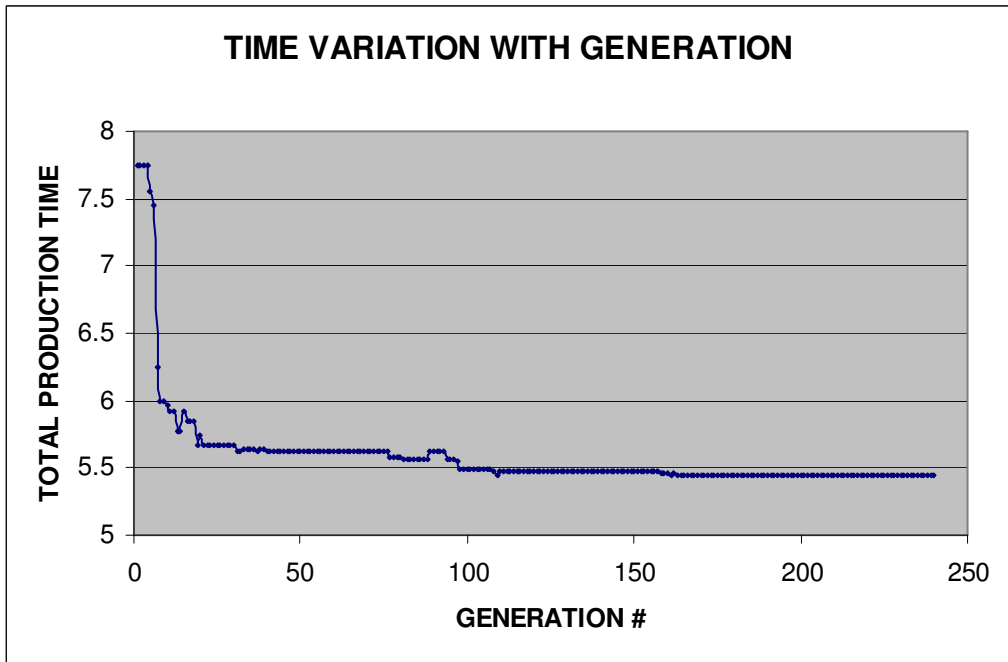


FIG. 5.2 (f)

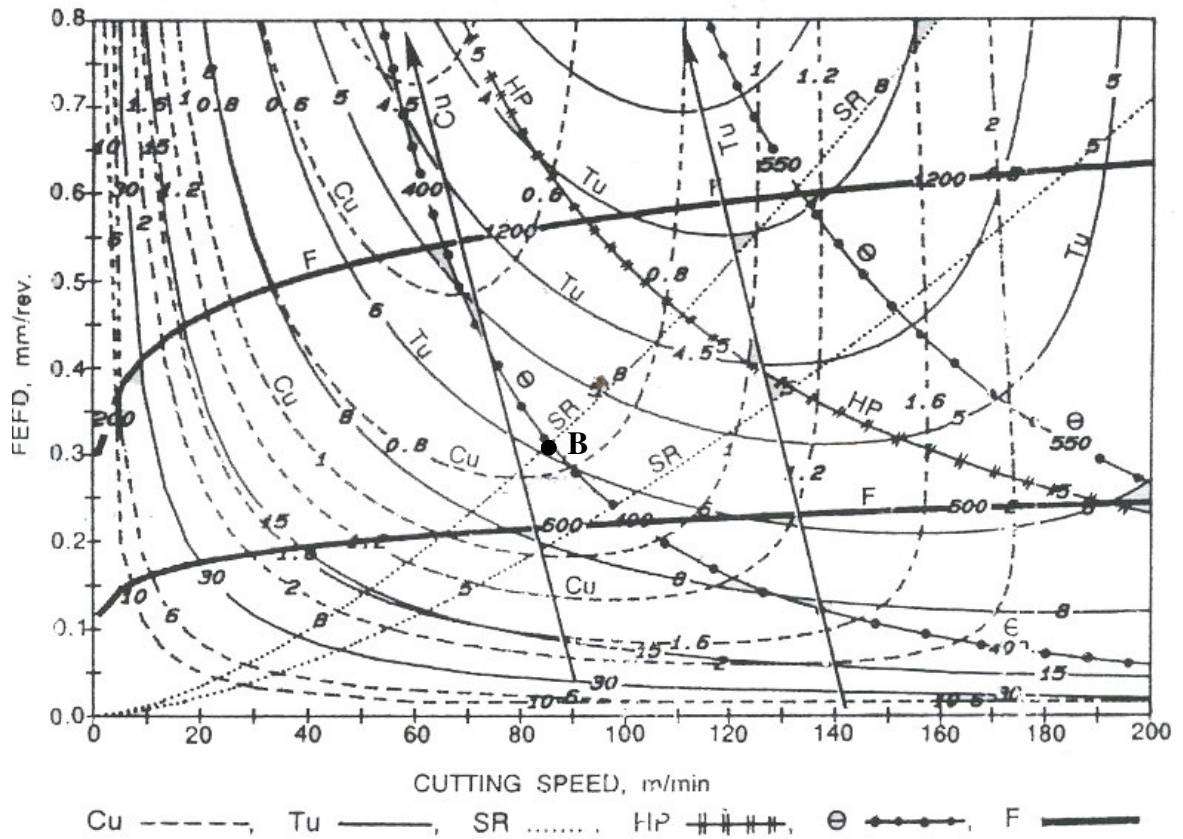


FIG. 5.2(g) Location of best result found by GA on the contours given by Agapiou [6], for $d_o = 5.08$ mm and the constraints of power, force, surface roughness, and temperature.

In the section 5.3, the total production cost is taken as an objective function with depth of cut, $doc = 2.54$ mm and the constraints force, surface roughness, temperature and power.

Machining parameters used for the example are::

Parameter	Value
SR_{max}	8 μm
HP_{max}	4 KW
F_{max}	600 N
T_{max}	400 deg C

The table 5.3(a), shows the values of randomly selected machining parameters, the associated fitness values and the various constraints at the starting generation. After applying the various GA operations, we get the table 5.3(b), that shows the values of above stated variables at the end generation. It is clear from these tables that the value of fitness function becomes zero, when the constraints cross their extreme limits. These both tables are also graphically plotted in fig. 5.3(a) to fig. 5.3(d).

Fig. 5.3(e) and fig. 5.3(f), shows the variation of best fitness function and the objective function values with generation, respectively. These figures clearly show how the values of both these functions get improved with generation, after applying the GA operations. From fig. 5.3(f), the best value of the objective function i.e. the total production cost is approximated to be 0.51912403 \$. It is clear from table 5.3(b) that the constraints surface roughness = 7.97486 μm , force = 556.27032 N and temperature = 399.54901 deg C have their extreme limits for the calculated best objective function value.

From fig. 5.3(g), that we have from J. S. Agapiou [6], the value of objective function lies at point C (less than 0.6 \$) that justifies our objective function value.

5.3 TOTAL PRODUCTION COST AS AN OBJECTIVE FUNCTION with doc =2.54mm

TABLE 5.3 (a)

Accumulated Statistics for Generation ---> 0
 *****Calculated Constraints*****

	FEED	SPEED	FITNESS	POWER	ROUGHNESS	TEMP	FORCE
1)	0.292335	132.968033	0.000000	2.34474	3.21129	439.30115	424.22491
2)	0.555556	91.106155	0.000000	2.75305	10.86986	428.98825	702.09052
3)	0.449115	117.851395	0.000000	2.94018	5.93701	456.81610	586.27393
4)	0.627980	100.989311	0.000000	3.32338	10.51159	459.32965	759.35553
5)	0.400390	193.546219	0.000000	4.20124	2.48892	547.84985	512.99951
6)	0.541260	167.803116	0.000000	4.67424	4.18479	549.66406	647.61218
7)	0.305438	38.739738	0.000002	0.79968	21.87232	263.76880	496.20035
8)	0.582464	198.214157	0.000000	5.74996	3.49716	597.72369	671.56482
9)	0.297424	88.476028	0.620547	1.64706	6.06909	371.91083	447.66342
10)	0.689890	52.994846	0.000000	2.00167	30.78431	357.85269	867.79700
11)	0.551487	130.097961	0.000000	3.77203	6.27827	496.66095	673.60504
12)	0.397367	45.946182	0.000002	1.14480	21.97858	299.94250	590.19592
13)	0.256019	172.642548	0.000000	2.67435	1.89003	476.34061	375.26791
14)	0.755221	119.513138	0.000000	4.46587	9.79364	511.76367	853.35394
15)	0.597399	140.026352	0.000000	4.28952	6.08359	520.56134	708.51361
16)	0.447940	99.459442	0.000000	2.51864	7.66359	425.44046	595.30597
17)	0.522132	151.958099	0.000000	4.15675	4.69311	523.68036	637.30859
18)	0.600518	125.005272	0.000000	3.88884	7.26672	497.20755	719.41583
19)	0.361475	145.726425	0.000000	3.00483	3.45750	476.92996	490.23969
20)	0.435209	72.425919	0.000000	1.85107	12.05711	370.38098	602.02740
21)	0.500640	35.975334	0.000000	1.09994	40.20001	283.94785	715.32031
22)	0.476404	53.474293	0.000000	1.51177	20.93806	332.29843	662.88568
23)	0.397115	56.130802	0.000004	1.37016	16.20153	326.39215	578.08032
24)	0.575647	77.674034	0.000000	2.45191	14.35514	404.36157	732.14325
25)	0.671931	35.087349	0.000000	1.35295	56.10932	299.05627	887.67596
26)	0.395937	30.829102	0.000000	0.79716	40.16294	252.87405	612.93542
27)	0.508467	165.055237	0.000000	4.38617	4.03014	538.92578	619.95776
28)	0.350291	142.078934	0.000000	2.86593	3.48170	468.87012	480.42664
29)	0.641004	96.909134	0.000000	3.25397	11.42467	453.45416	773.96838
30)	0.708093	138.297150	0.000000	4.84324	7.35333	536.41779	802.45142
31)	0.522005	88.734421	0.000000	2.56096	10.62859	418.82538	672.88434
32)	0.565257	163.732956	0.000000	4.72943	4.53731	549.01428	669.96820
33)	0.536809	197.995209	0.000000	5.38993	3.22741	587.48926	633.04706
34)	0.417081	147.055374	0.000000	3.38718	3.93695	493.14420	543.32709
35)	0.411751	114.914871	0.000000	2.68589	5.65394	443.95822	551.90210
36)	0.643016	174.114868	0.000000	5.52713	4.70342	578.29547	731.02441
37)	0.590551	52.786884	0.000000	1.76680	26.49308	345.77914	775.59912
38)	0.464380	61.641014	0.000000	1.68414	16.44254	350.88864	641.41229
39)	0.529146	167.894470	0.000000	4.59468	4.08737	547.22375	637.03540
40)	0.299137	104.653839	0.622860	1.92438	4.72906	399.46606	441.94870
41)	0.475444	62.308090	0.000000	1.73206	16.56267	354.22733	651.74493
42)	0.683941	161.017441	0.000000	5.40548	5.63562	567.11127	770.54846
43)	0.677419	70.521309	0.000000	2.55206	19.57778	401.80118	831.96362
44)	0.448983	96.658516	0.000000	2.45917	8.02238	420.60861	598.03876
45)	0.391266	103.945671	0.000000	2.35824	6.25641	421.29047	537.28802
46)	0.596014	151.364059	0.000000	4.59256	5.39203	537.33356	701.76575
47)	0.291578	91.624153	0.619365	1.67360	5.64142	375.83350	439.70691
48)	0.703280	88.674088	0.000000	3.22932	14.35145	445.52051	835.26465
49)	0.695903	173.502808	0.000000	5.86001	5.11921	586.94110	774.41528
50)	0.416767	185.150482	0.000000	4.16508	2.77182	542.37750	530.50543
51)	0.275311	78.578583	0.600090	1.39370	6.72590	348.15155	428.39642
52)	0.541328	185.495361	0.000000	5.11603	3.59383	572.89392	641.12781
53)	0.504070	30.825405	0.000000	0.96227	51.19051	266.25266	730.20923
54)	0.552917	84.893860	0.000000	2.57393	12.04393	416.12988	704.69434
55)	0.374497	73.831947	0.000010	1.67511	10.07026	361.79858	538.84619
56)	0.526812	96.564583	0.000000	2.78331	9.43297	434.67578	671.59253
57)	0.672678	43.300648	0.000000	1.63632	40.80158	326.94373	869.66357
58)	0.311996	83.715027	0.624028	1.62665	6.92619	367.04718	466.06430
59)	0.556007	158.816315	0.000000	4.54258	4.67444	540.29895	664.04913
60)	0.593069	148.181244	0.000000	4.48818	5.54143	532.08954	700.75732

max=0.624028 min=0.000000 avg=0.051448 sum=3.086909 no_mutation=0 no_cross=0

FEED 0.311996
 SPEED 83.715027
 FITNESS 0.624028

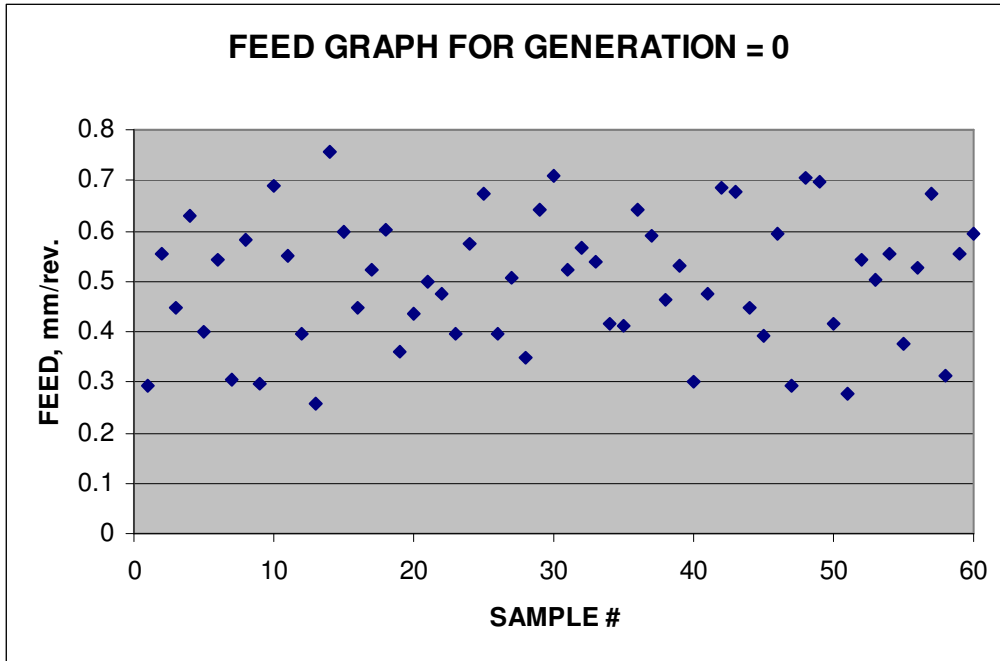


FIG. 5.3 (a)

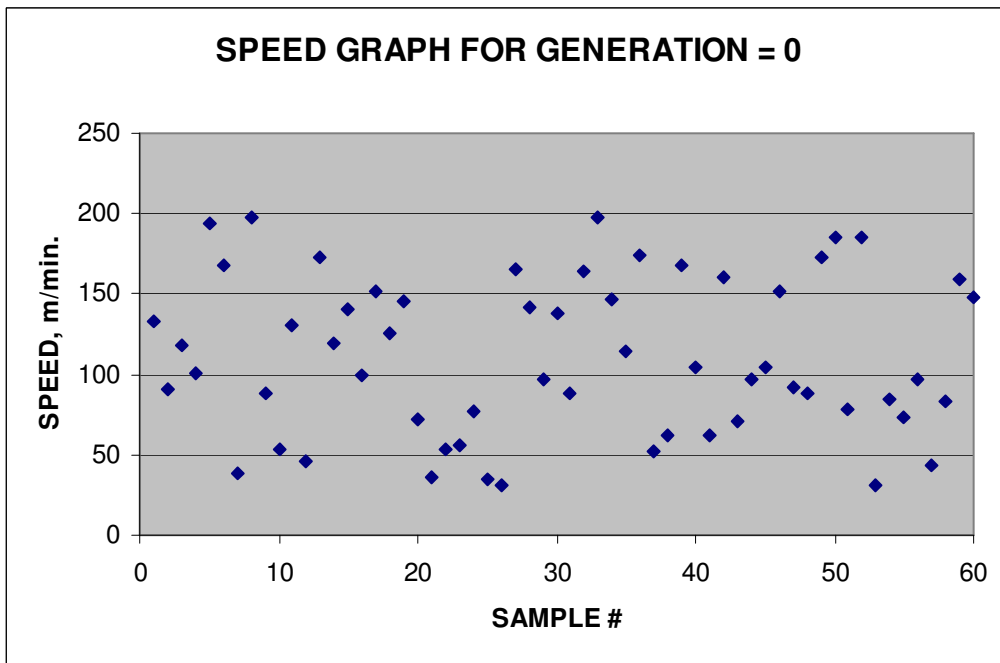


FIG. 5.3 (b)

Fig. 5.3 Speed and feed graphs for starting generation with doc = 2.54mm

TABLE 5.3(b)

Accumulated Statistics for Generation ---> 240

*****Calculated Constraints*****							
	FEED	SPEED	FITNESS	POWER	ROUGNESS	TEMP	FORCE

1)	0.266643	91.917366	0.607243	1.56537	5.13215	369.35254	411.97861
2)	0.278927	175.066818	0.000000	1.47929	6.95564	354.80020	446.01025
3)	0.275449	90.388443	0.610978	1.58149	5.43925	369.27078	422.51578
4)	0.321516	88.904922	0.631136	1.75787	6.51470	378.79578	473.43884
5)	0.260336	92.937363	0.604394	1.55175	4.92693	369.20813	404.43839
6)	0.260091	91.386017	0.603416	1.52730	5.04984	366.53860	404.85187
7)	0.256181	90.270775	0.600517	1.49277	5.06733	363.49872	400.92871
8)	0.260088	80.761177	0.593813	1.36650	6.09344	347.99875	409.94943
9)	0.276007	85.215034	0.607598	1.50216	5.96114	360.40536	425.67062
10)	0.402449	90.271416	0.658240	2.12326	7.97486	399.54901	556.27032
11)	0.276007	85.215034	0.607598	1.50216	5.96114	360.40536	425.67062
12)	0.260088	91.386093	0.603415	1.52729	5.04979	366.53799	404.84903
13)	0.263212	80.766205	0.595715	1.37936	6.16634	348.88242	413.51080
14)	0.260088	92.557159	0.604065	1.54489	4.95299	368.50043	404.32684
15)	0.256119	90.270775	0.600482	1.49249	5.06610	363.48022	400.85831
16)	0.263212	92.557167	0.605750	1.55934	5.01272	369.42398	407.84195
17)	0.285460	85.092392	0.612432	1.54014	6.17964	362.74182	436.25449
18)	0.402573	90.271416	0.000004	2.38031	9.23858	411.95892	618.60852
19)	0.349105	84.929054	0.639941	1.79883	7.58564	378.06839	504.89075
20)	0.280241	90.401688	0.613392	1.60313	5.53304	370.63129	427.82678
21)	0.274230	90.276581	0.610292	1.57428	5.42530	368.73624	421.21283
22)	0.260091	92.937363	0.604262	1.55061	4.92227	369.13519	404.16211
23)	0.281606	90.266258	0.613993	1.60704	5.57277	370.77563	429.40091
24)	0.402573	84.923195	0.000013	2.01019	8.75334	389.50204	559.84753
25)	0.383120	90.405663	0.652769	2.04603	7.57322	395.70645	536.68903
26)	0.392347	90.265556	0.655434	2.08145	7.77466	397.42166	546.11530
27)	0.395319	90.399048	0.656275	2.09653	7.81621	398.29474	549.02930
28)	0.281392	90.558594	0.614042	1.61077	5.54122	371.21948	429.02423
29)	0.311292	90.516861	0.627564	1.74205	6.13679	379.08295	461.63382
30)	0.289750	85.580887	0.614973	1.56622	6.21854	364.75378	440.74240
31)	0.275978	85.215034	0.607582	1.50204	5.96051	360.39740	425.63812
32)	0.280736	84.922844	0.609851	1.51750	6.09541	361.17139	431.09518
33)	0.283392	47.898838	0.000005	0.91304	14.69375	284.15662	459.97214
34)	0.403441	84.958916	0.000013	2.01433	8.76669	389.74612	560.69873
35)	0.276007	90.361519	0.611247	1.58357	5.45279	369.38150	423.14951
36)	0.395319	85.257751	0.000014	1.98890	8.54378	388.66226	552.29559
37)	0.260134	173.728638	0.000000	2.72315	1.90232	479.16406	379.39029
38)	0.268274	90.404884	0.607259	1.54952	5.29554	367.26099	414.50015
39)	0.283854	84.538010	0.611142	1.52438	6.20608	361.32010	434.76120
40)	0.274230	90.281113	0.610295	1.57435	5.42488	368.74399	421.21066
41)	0.330019	85.209297	0.632722	1.72676	7.13350	374.15814	484.56277
42)	0.279542	85.587204	0.609783	1.52311	5.99792	362.03064	429.42630
43)	0.383118	88.942657	0.652624	2.01620	7.76334	393.01633	537.57501
44)	0.260987	90.371941	0.603287	1.51610	5.15399	365.09021	406.32162
45)	0.311292	85.580887	0.625045	1.65632	6.68278	370.28009	464.26349
46)	0.402573	90.271416	0.658274	2.12377	7.97733	399.57474	556.39459
47)	0.311292	85.583481	0.625047	1.65636	6.68247	370.28473	464.26181
48)	0.438292	85.580887	0.000011	2.16296	9.42209	397.76648	594.97180
49)	0.383660	89.242790	0.652825	2.02455	7.73464	393.68646	537.94208
50)	0.401443	90.270767	0.657966	2.11911	7.95493	399.33893	555.26202
51)	0.256119	90.401024	0.600569	1.49443	5.05500	363.70013	400.79956
52)	0.275448	88.987694	0.610138	1.55942	5.56992	366.86011	423.18457
53)	0.260091	93.038567	0.604312	1.55213	4.91415	369.30389	404.11835
54)	0.349229	89.853111	0.641826	1.89295	6.96534	387.12296	502.14569
55)	0.275443	90.398880	0.610981	1.58163	5.43817	369.28696	422.50403
56)	0.347429	92.896431	0.641652	1.94271	6.58719	392.13013	498.58234
57)	0.392343	90.400444	0.655437	2.08424	7.75695	397.66891	546.02875
58)	0.277076	90.281113	0.611744	1.58708	5.48141	369.54306	424.37558
59)	0.599135	90.517174	0.000000	2.90310	11.84224	434.61240	742.08984
60)	0.260087	91.386093	0.603414	1.52728	5.04977	366.53766	404.84775

max=0.658274 min=0.0000 avg=0.537718 sum=32.263084 no_mutation=17407 no_cross=4285

FEED 0.402573
 SPEED 90.271416
 FITNESS 0.658240

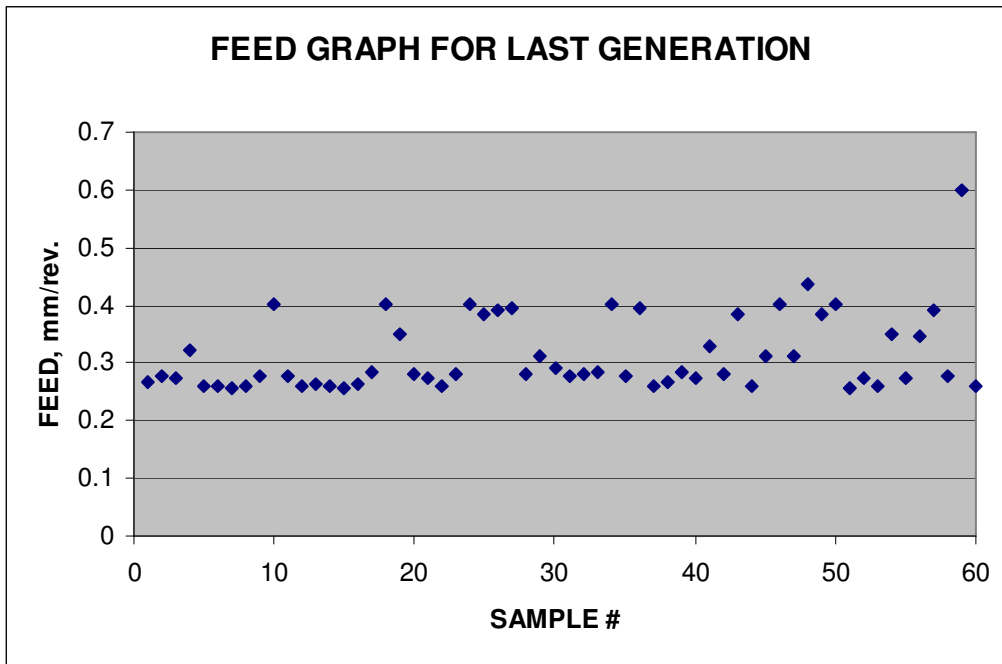


FIG. 5.3 (c)

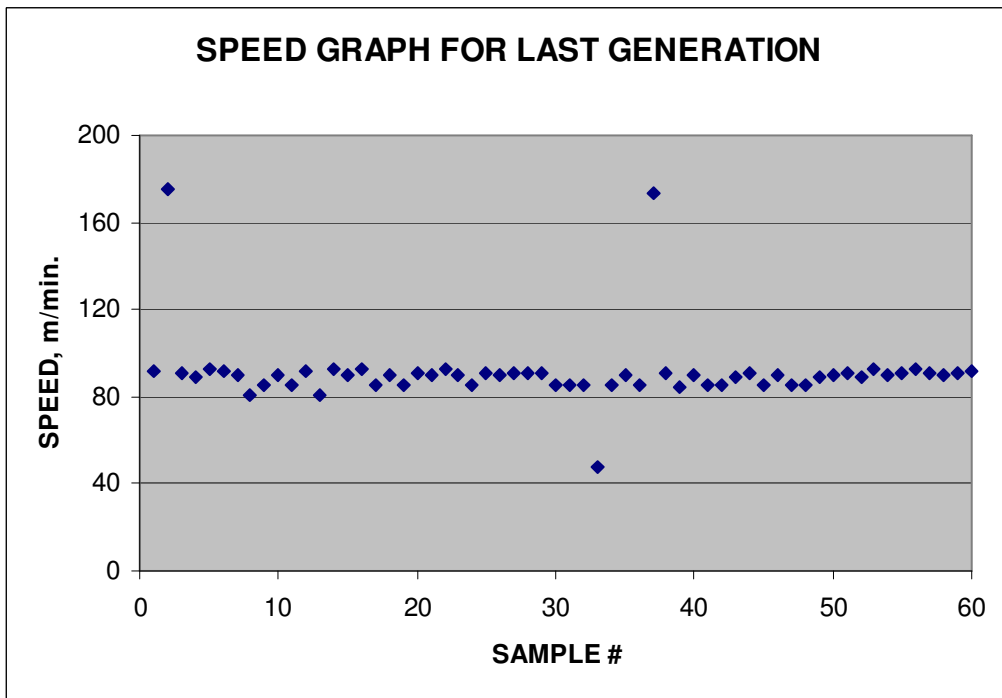


FIG. 5.3 (d)

Fig. 5.3 Speed and feed graphs for last generation with doc = 2.54mm

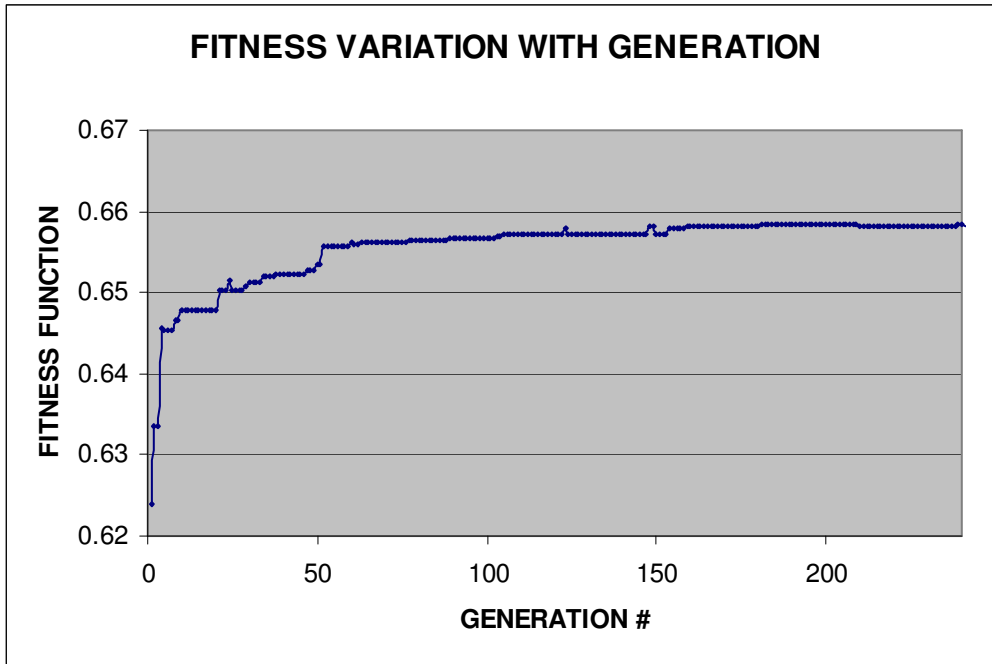


FIG. 5.3 (e)

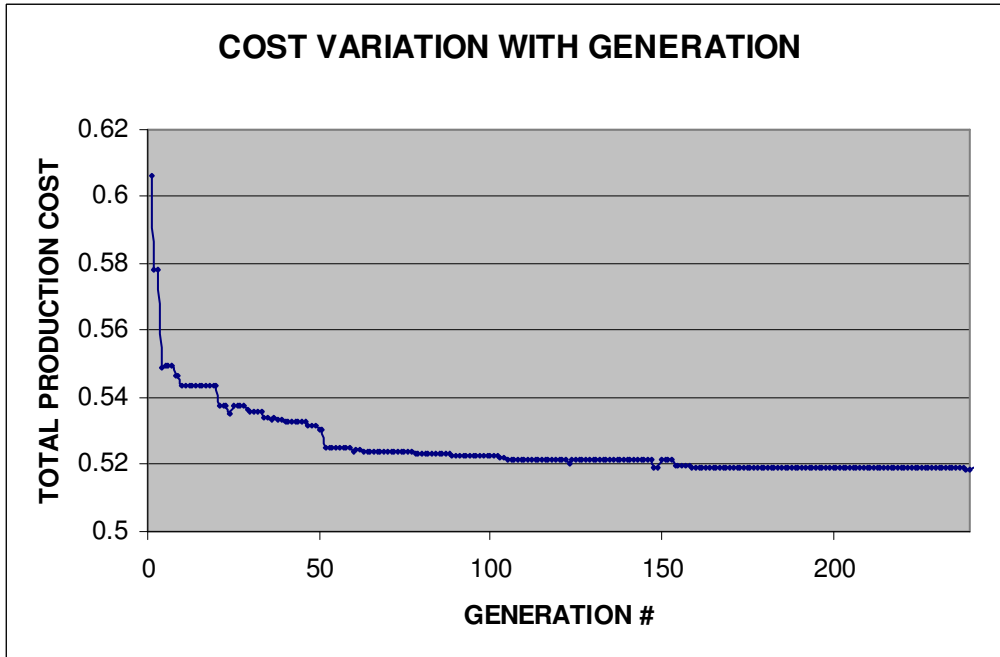


FIG. 5.3 (f)

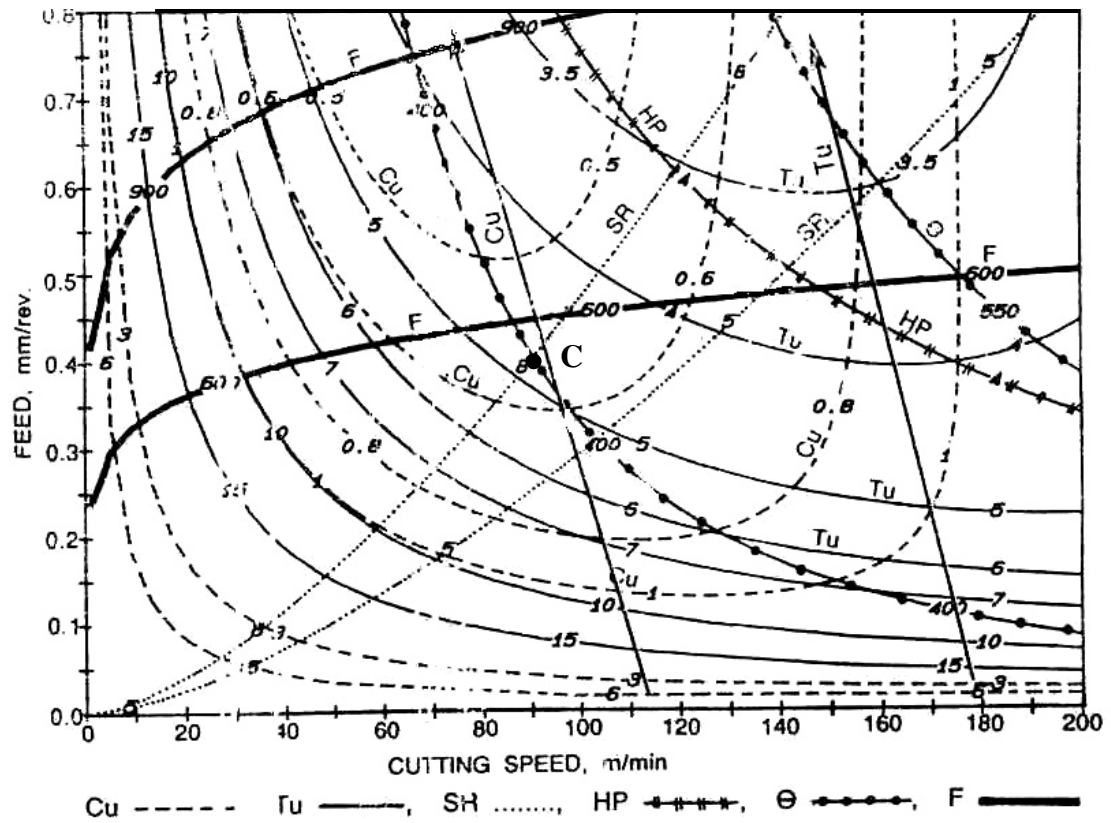


FIG. 5.3(g) Location of best result found by GA on the contours given by Agapiou [6], for $d_{oc} = 2.54$ mm and the constraints of power, force, surface roughness, and temperature.

In the section 5.4, the total production cost is taken as an objective function with depth of cut, $doc = 5.08$ mm and the constraints force, surface roughness, temperature, and power. Machining parameters used for the example are::

Parameter	Value
SR_{max}	8 μm
HP_{max}	5 KW
F_{max}	1200 N
T_{max}	400 deg C

The table 5.4(a), shows the values of randomly selected machining parameters, the associated fitness values and the various constraints at the starting generation. After applying the various GA operations, we get the table 5.4(b), that shows the values of above stated variables at the end generation.

Fig. 5.4(e) and fig. 5.4(f), shows the variation of best fitness function and the objective function values with generation, respectively. These figures clearly show how the values of both these functions get improved with generation, after applying the GA operations. From fig. 5.4(f), the best value of the objective functions i.e. the total production cost is approximated to be 0.71820772 \$. It is clear from table 5.4(b) that the constraints surface roughness = 7.99032 μm and temperature = 399.88733 deg C have their extreme limits for the calculated best objective function value.

From fig. 5.4(g), that we have from J. S. Agapiou [6], the value of objective function lies at point D (less than 0.8 \$) that justifies our objective function value.

5.4 TOTAL PRODUCTION COST AS AN OBJECTIVE FUNCTION with doc = 5.08mm

TABLE 5.4(a)

Accumulated Statistics for Generation ---> 0
 *****Calculated Constraints*****

	FEED	SPEED	FITNESS	POWER	ROUGHNESS	TEMP	FORCE
1)	0.408028	128.861130	0.000000	4.97227	5.59803	501.15790	911.45538
2)	0.431649	135.988861	0.000000	5.45332	5.45799	518.45667	944.24762
3)	0.417278	146.122513	0.000000	5.66609	4.72960	530.37244	914.66638
4)	0.595206	187.120193	0.000000	9.33804	4.63906	631.92120	1154.00684
5)	0.278887	71.214409	0.000011	2.16696	9.41010	361.56570	734.53174
6)	0.649358	61.237061	0.000000	3.65727	27.65409	405.10986	1376.46960
7)	0.347416	39.013523	0.000001	1.49645	29.28555	293.80276	915.51666
8)	0.612997	138.745483	0.000000	7.29997	7.52875	562.06177	1215.18018
9)	0.720976	35.888702	0.000000	2.45328	69.19968	330.94867	1567.52942
10)	0.493170	58.797855	0.000002	2.84492	22.31654	376.01230	1132.20947
11)	0.318152	70.350945	0.000008	2.37522	10.94163	369.79678	809.13660
12)	0.285897	190.316025	0.000000	5.35153	2.16531	547.10760	676.98914
13)	0.757483	54.809780	0.000000	3.73241	38.20441	399.41806	1556.46509
14)	0.428904	183.063324	0.000000	7.09069	3.45162	585.39508	912.01007
15)	0.646126	81.214676	0.000000	9.67227	5.28923	634.25781	1228.75525
16)	0.472415	193.947983	0.000000	8.05371	3.48359	611.53827	972.48419
17)	0.513896	194.835175	0.000000	8.63555	3.76454	623.39087	1033.19360
18)	0.433894	166.907455	0.000000	6.58407	4.01844	564.85620	928.33972
19)	0.670720	184.164490	0.000000	10.10402	5.35823	643.40460	1260.42566
20)	0.616414	121.236298	0.000000	6.49346	9.29388	532.21277	1236.87427
21)	0.470739	193.842026	0.000000	8.02746	3.47406	610.95361	970.03497
22)	0.532331	87.484390	0.000000	4.31784	13.17163	450.96365	1149.48877
23)	0.389342	117.283676	0.000000	4.40432	6.16224	477.31546	889.43939
24)	0.268315	32.659256	0.000001	1.04245	29.60445	257.79843	772.92761
25)	0.299420	42.516071	0.000002	1.43980	22.13460	295.25638	814.83728
26)	0.728896	189.040680	0.000000	11.03787	5.59808	661.56079	1335.23486
27)	0.717508	77.282845	0.000000	4.87446	21.46106	455.72604	1445.27966
28)	0.758391	111.284836	0.000000	7.06669	13.03519	536.18542	1449.96973
29)	0.653219	89.224884	0.000000	5.15573	15.69883	474.41107	1330.67969
30)	0.675701	138.657486	0.000000	7.87162	8.31011	573.31702	1304.16724
31)	0.301350	151.937500	0.000000	4.55282	3.21473	503.90561	719.55536
32)	0.262905	159.025757	0.000000	4.26452	2.61538	499.20163	648.76184
33)	0.537256	75.069305	0.000000	3.78934	16.77592	423.93973	1175.26904
34)	0.478104	93.774849	0.000000	4.22680	10.64037	453.92004	1055.89746
35)	0.742246	95.963181	0.000000	6.08174	15.97785	502.07230	1449.10608
36)	0.263009	50.883278	0.000005	1.52968	14.78915	309.97009	728.35394
37)	0.583679	153.893936	0.000000	7.71298	6.12279	580.70630	1160.51575
38)	0.411408	33.794559	0.000001	1.50038	43.16876	286.52557	1050.06335
39)	0.720651	176.316025	0.000000	10.27531	6.15290	641.38452	1333.64893
40)	0.362764	174.197006	0.000000	5.95046	3.14607	554.05573	811.80292
41)	0.425611	145.779343	0.000000	5.74200	4.84171	532.02728	928.09497
42)	0.296374	125.682091	0.000000	3.78868	4.21812	464.17279	724.71539
43)	0.383948	83.143631	0.000000	3.19658	10.25078	412.46042	911.71533
44)	0.621441	109.097389	0.000000	5.94280	10.99975	510.34235	1257.54785
45)	0.458077	113.079910	0.000000	4.83822	7.66873	486.26569	1004.41370
46)	0.661922	168.979767	0.000000	9.25522	6.02654	619.34821	1259.34668
47)	0.330835	111.854355	0.000000	3.71699	5.62374	452.44998	794.20056
48)	0.483582	193.047501	0.000000	8.16754	3.59158	613.31000	989.56335
49)	0.454688	145.674576	0.000000	6.04183	5.17950	539.18231	973.71405
50)	0.426715	114.465324	0.000000	4.62830	7.01071	481.59308	952.89905
51)	0.598122	165.502396	0.000000	8.39318	5.61826	601.39142	1172.59448
52)	0.737637	120.437439	0.000000	7.42522	11.24201	550.81519	1409.76013
53)	0.553303	146.055450	0.000000	7.05803	6.28283	562.08911	1122.33545
54)	0.737833	83.728340	0.000000	5.35425	19.54118	473.88373	1462.92712
55)	0.582040	179.800034	0.000000	8.85280	4.81970	618.77820	1140.04224
56)	0.646133	59.594906	0.000000	3.55505	28.67692	400.12012	1375.29187
57)	0.329858	48.588875	0.000003	1.75100	19.91369	318.88629	862.34546
58)	0.260648	124.174423	0.000000	3.39045	3.77639	449.68634	661.07977
59)	0.258701	127.025024	0.000000	3.44024	3.62097	453.24295	655.98602
60)	0.716501	193.317734	0.000000	11.11272	5.31854	665.32050	1315.74939

max=0.000011 min=0.000000 avg=0.000001 sum=0.000035 no_mutation=0 no_cross=0

FEED 0.278887
 SPEED 71.214409
 FITNESS 0.000011

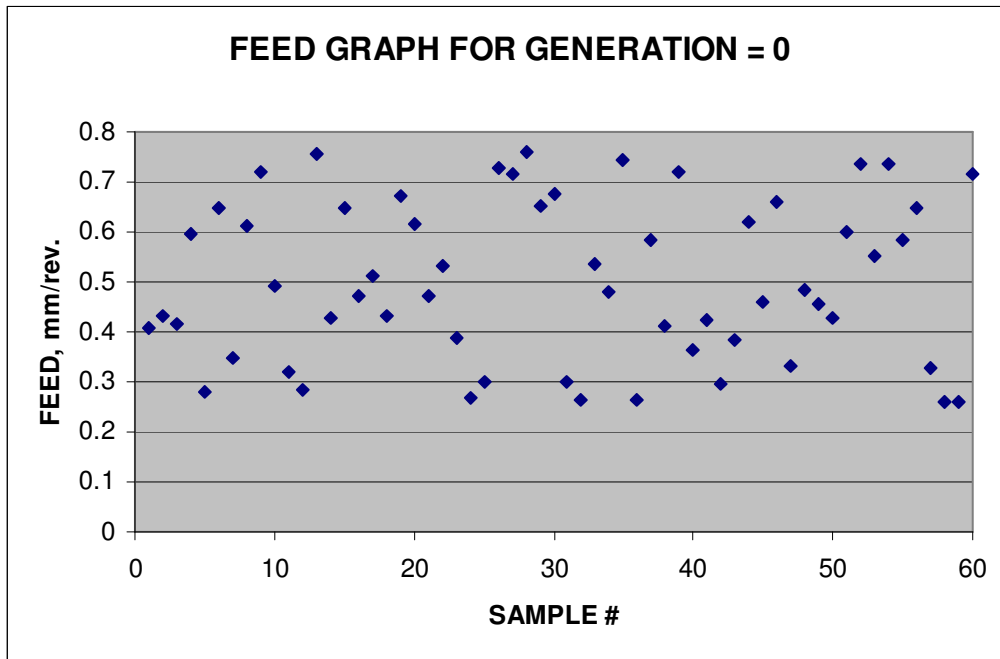


FIG. 5.4 (a)

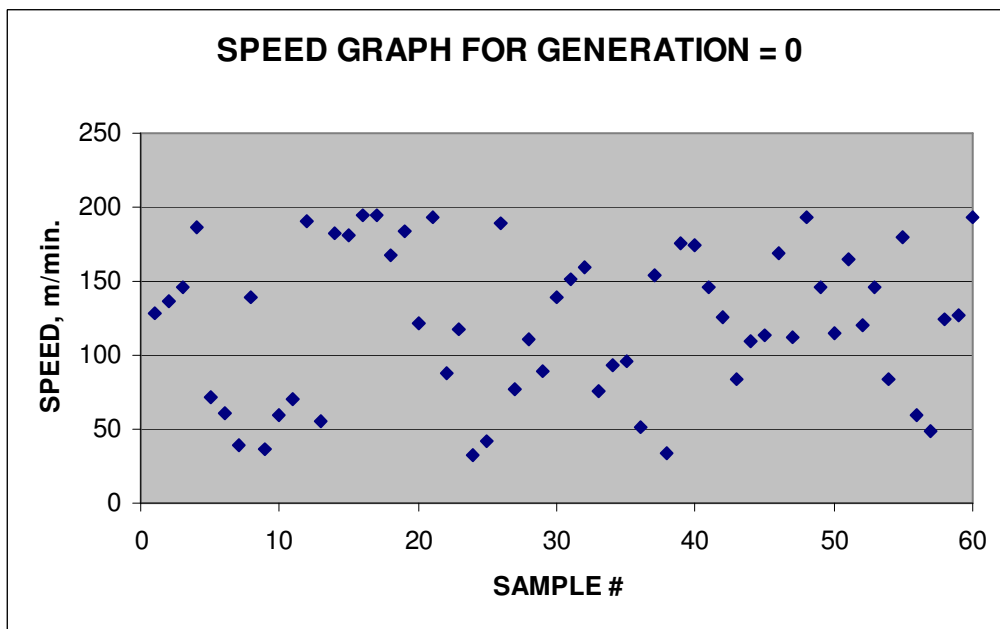


FIG. 5.4 (b)

Fig. 5.4 Speed and feed graphs for starting generation with doc = 5.08mm

TABLE 5.4(b)

Accumulated Statistics for Generation ---> 240

```

*****Calculated Constraints*****
FEED      SPEED      FITNESS      POWER      ROUGHNESS      TEMP      FORCE
*****
 1)  0.307866  85.610725  0.580168  2.72842  7.89848  396.82614  771.41779
 2)  0.295968  84.885216  0.576158  2.52139  6.99811  389.02112  711.99518
 3)  0.274949  84.880081  0.567242  2.50986  7.10415  388.00562  714.18414
 4)  0.307803  85.590622  0.580162  2.76149  7.85644  398.65726  774.43280
 5)  0.308684  85.591270  0.580485  2.36557  6.55369  382.00388  674.89355
 6)  0.256444  90.904022  0.554613  2.14442  7.08149  363.88120  692.93243
 7)  0.412747  85.539909  0.000002  5.09557  2.75585  529.43146  719.55255
 8)  0.303031  169.924545  0.000000  5.05704  2.72716  528.39166  714.32050
 9)  0.288209  85.451767  0.572622  2.61955  7.37255  392.94775  738.49042
10)  0.376247  74.914909  0.000007  2.86475  11.76842  393.22394  907.95459
11)  0.290952  85.611664  0.573634  2.64342  7.42188  394.03445  743.43842
12)  0.274075  84.883972  0.566844  2.50373  7.08097  387.75467  712.53369
13)  0.291454  85.249161  0.574090  2.63689  7.48283  393.47775  744.68781
14)  0.312743  85.591789  0.581956  2.79603  7.98286  399.98761  783.42175
15)  0.304966  84.879860  0.579662  2.72111  7.88302  396.50232  769.90021
16)  0.313774  106.789581  0.000000  3.42093  5.72172  438.95169  767.88702
17)  0.274069  87.707535  0.565034  2.57852  6.73725  393.09616  710.16498
18)  0.336641  84.929802  0.000000  2.94070  8.69744  404.87128  827.03253
19)  0.295972  84.875473  0.576166  2.65819  7.65023  394.02087  753.37555
20)  0.274335  84.880043  0.566964  2.50548  7.08822  387.82413  713.02734
21)  0.400160  85.539909  0.000000  3.38689  10.23373  420.99292  936.76642
22)  0.312747  84.874825  0.000015  2.77497  8.08568  398.58527  784.09668
23)  0.273141  84.929802  0.566396  2.49829  7.05096  387.56543  710.73389
24)  0.303031  84.924545  0.578891  2.52143  6.99794  389.02359  711.99408
25)  0.305836  84.888168  0.579985  2.72741  7.90443  396.75479  771.48517
26)  0.274069  85.549332  0.566476  2.52135  6.99729  389.02164  711.96008
27)  0.296033  84.929840  0.576153  2.66015  7.64436  394.14331  753.43915
28)  0.308747  106.841270  0.000000  3.37957  5.62554  437.56677  758.91052
29)  0.295972  84.874825  0.576167  2.65817  7.65031  394.01959  753.37616
30)  0.307866  85.610725  0.580168  2.76251  7.85524  398.71323  774.52789
31)  0.306833  87.536331  0.000000  2.81099  7.56851  402.15323  770.90381
32)  0.528038  85.591568  0.000000  4.20701  13.50666  446.12814  1145.29480
33)  0.295972  84.929802  0.576129  2.65972  7.64279  394.12628  753.32672
34)  0.274069  84.880081  0.566843  2.50359  7.08132  387.74551  712.52600
35)  0.296031  85.559639  0.575701  2.67788  7.55895  395.36197  752.87177
36)  0.549972  84.874825  0.000000  4.30996  14.25100  448.34924  1180.59778
37)  0.306085  74.304802  0.000011  2.42091  9.68562  375.31580  782.42371
38)  0.264222  74.258118  0.000014  2.15731  8.36399  363.82489  703.33398
39)  0.306085  84.883118  0.580083  2.72900  7.91161  396.81241  771.94507
40)  0.312747  85.539909  0.582002  2.79453  7.99032  399.88733  783.47693
41)  0.307866  85.610725  0.580168  2.76251  7.85524  398.71323  774.52789
42)  0.305666  84.553482  0.580169  2.71655  7.94760  396.05420  771.48273
43)  0.308684  85.591270  0.580485  2.76767  7.87891  398.89639  776.03693
44)  0.288035  85.040840  0.572821  2.60698  7.42226  392.10690  738.52710
45)  0.293988  84.550484  0.575583  2.63517  7.64317  392.83652  750.00153
46)  0.305837  84.905952  0.579972  2.72793  7.90194  396.78979  771.47046
47)  0.295972  42.374825  0.000002  1.42259  21.98969  294.11670  808.29718
48)  0.272215  84.592499  0.566139  2.48277  7.06959  386.64578  709.27136
49)  0.272215  41.101032  0.000002  1.29660  21.17787  285.21817  763.07605
50)  0.295972  87.580826  0.574005  2.73432  7.29392  399.22195  750.98383
51)  0.312685  84.875847  0.000015  2.77457  8.08393  398.57077  783.98297
52)  0.270405  169.885590  0.000000  4.62614  2.43328  516.03961  657.71228
53)  0.305836  85.562622  0.579456  2.74690  7.80991  398.06909  770.86652
54)  0.312653  84.211540  0.000015  2.75480  8.18023  397.25583  784.55035
55)  0.273142  84.929802  0.566396  2.49830  7.05099  387.56573  710.73572
56)  0.273141  84.928513  0.566396  2.49825  7.05113  387.56299  710.73499
57)  0.295972  84.929802  0.576129  2.65972  7.64279  394.12628  753.32672
58)  0.295972  84.874825  0.576167  2.65817  7.65031  394.01959  753.37616
59)  0.274087  85.546364  0.566486  2.52139  6.99811  389.02112  711.99518
60)  0.312743  85.581085  0.581965  2.79571  7.98438  399.96671  783.43170

```

max=0.582002 min=0.000000 avg=0.411754 sum=24.705212 no_mutation=17561 no_cross=4344

```

FEED      0.312747
SPEED    85.539909
FITNESS  0.582002

```

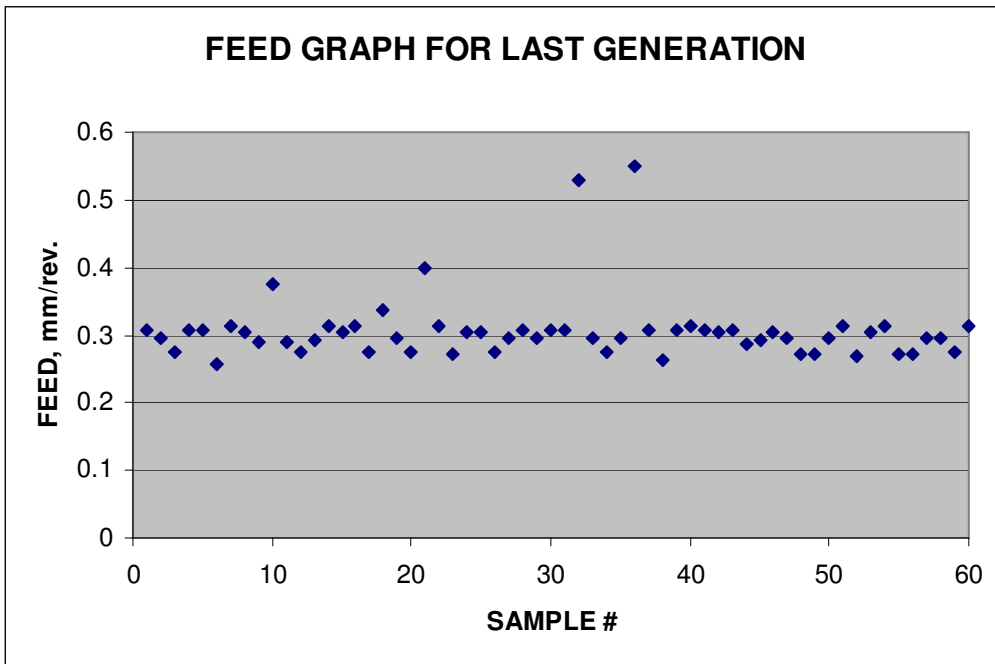


FIG. 5.4 (c)

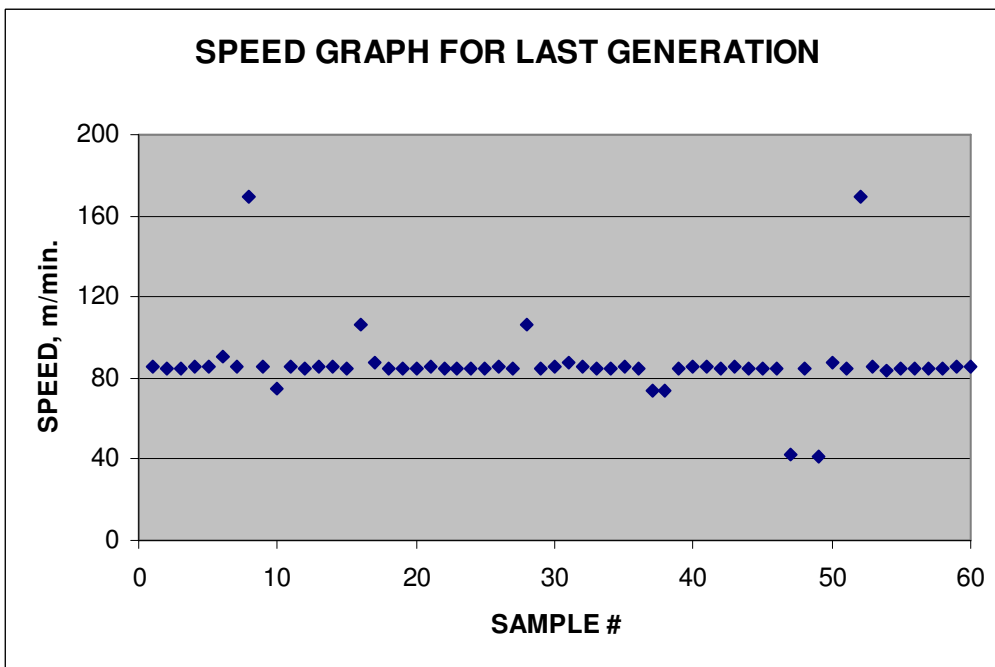


FIG. 5.4 (d)

Fig. 5.4 Speed and feed graphs for last generation with doc = 5.08mm

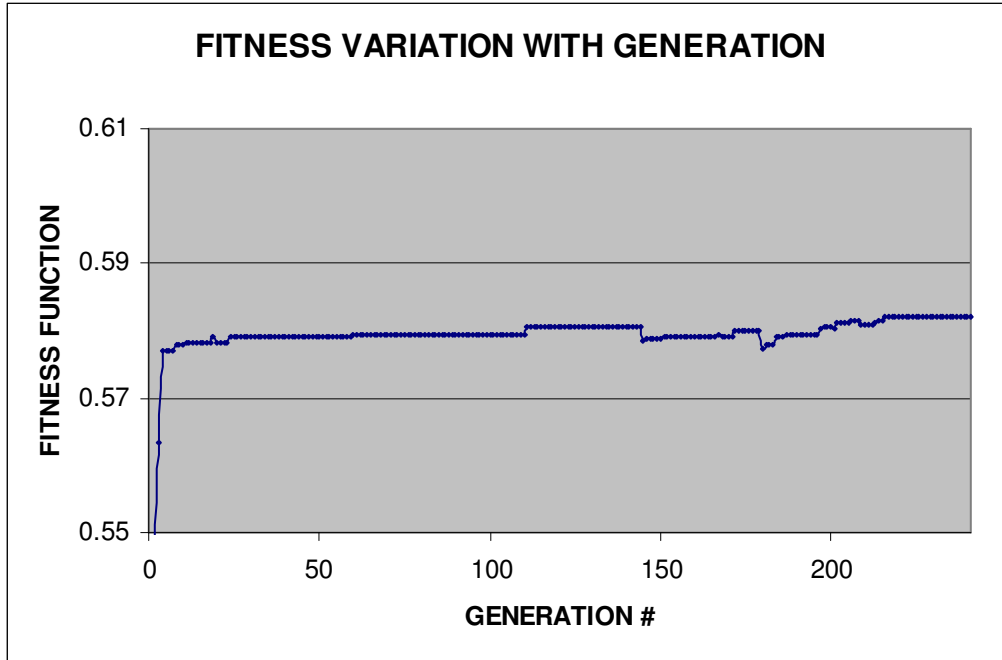


FIG. 5.4 (e)

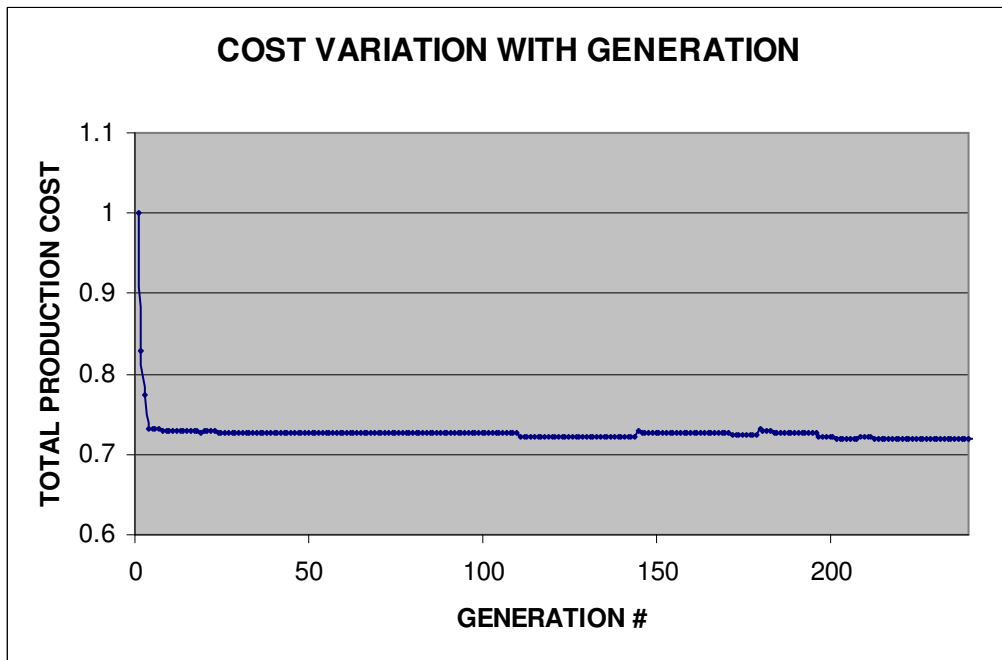


FIG. 5.4 (f)

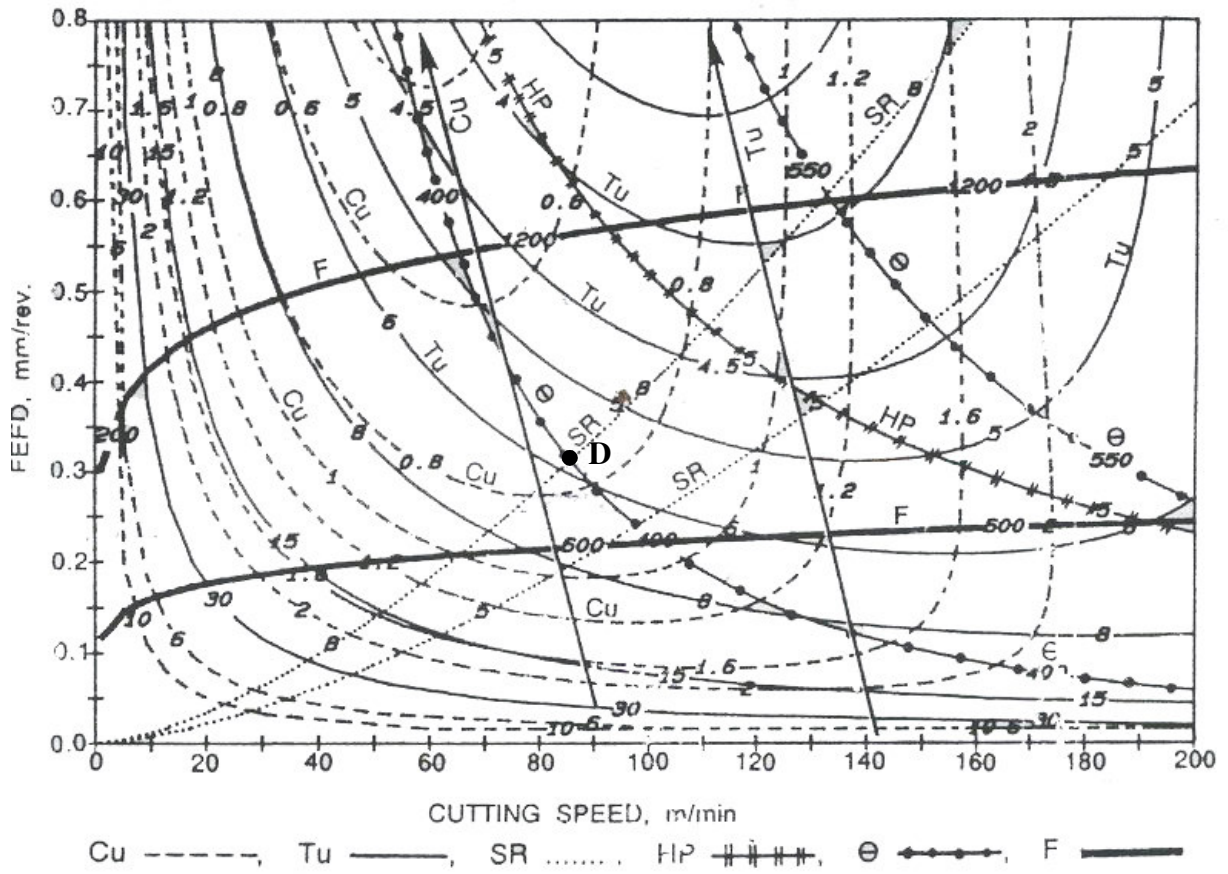


FIG. 5.4(g) Location of best result found by GA on the contours given by Agapiou [6], for $doc = 5.08$ mm and the constraints of power, force, surface roughness, and temperature.

In the section 5.5, the combined objective function is taken that includes both the total production cost and the total production time with weight coefficients 0.6 and 0.4 respectively, and depth of cut, $doc = 2.54$ mm having the constraints force, surface roughness, temperature and power.

Machining parameters used for the example are::

Parameter	Value
SR_{max}	2 μ m
HP_{max}	5 KW
F_{max}	600 N
T_{max}	500 deg C
λ	0.212

Fig. 5.5(e) and fig. 5.5(f), shows the variation of best fitness function and the objective function values with generation, respectively. These figures clearly show how the values of both these functions get improved with generation, after applying the GA operations. From fig. 5.5(f), the best value of the objective function is approximated to be 0.91696537. It is clear from table 5.5(b) that the constraints surface roughness = 1.99998 μ m and temperature = 467.68423 deg C have their extreme limits for the calculated best objective function value. Here we get the results at early generation because other constraints are no more acting due to their high values.

From fig. 5.5(g), that we have from J. S. Agapiou [6], the value of objective function lies at point E (less than 1) that justifies our objective function value.

5.5 COMBINED OBJECTIVE FUNCTION with doc = 2.54mm

TABLE 5.5(a)

Accumulated Statistics for Generation ---> 0
 *****Calculated Constraints*****

	FEED	SPEED	FITNESS	POWER	ROUGHNESS	TEMP	FORCE
1)	0.509809	143.570511	0.000000	3.87678	4.99491	508.99881	629.98132
2)	0.684130	180.702728	0.000000	5.99806	4.73067	594.76294	761.75049
3)	0.680531	116.590492	0.000012	4.02673	9.15969	495.73724	793.28534
4)	0.448951	116.046623	0.000027	2.89880	6.07570	453.86099	587.03625
5)	0.564842	90.154854	0.000008	2.76266	11.23004	428.59384	711.33557
6)	0.563974	33.474651	0.000000	1.13126	50.55053	282.44473	785.55566
7)	0.343484	166.771347	0.000140	3.26025	2.67581	499.05298	466.01419
8)	0.746385	126.624870	0.000000	4.66136	8.86453	522.87634	841.16431
9)	0.641327	138.249557	0.000000	4.48181	6.66084	525.47351	746.88055
10)	0.410470	191.418243	0.000000	4.24110	2.59507	548.16132	522.91589
11)	0.342245	165.294357	0.000137	3.22515	2.70242	496.84512	465.21420
12)	0.747566	123.108353	0.000000	4.55029	9.26695	516.98846	844.53473
13)	0.520237	195.282150	0.000000	5.19478	3.19366	580.39441	619.68274
14)	0.602754	106.890472	0.000012	3.38757	9.25344	466.30637	732.88861
15)	0.421478	191.924759	0.000000	4.33987	2.65427	551.76666	532.90344
16)	0.703031	33.467255	0.000000	1.34317	63.09134	295.94736	921.68030
17)	0.328929	70.889549	0.000011	1.45948	9.40406	346.10699	492.49600
18)	0.368603	132.485016	0.000060	2.80027	4.07531	460.29648	502.05032
19)	0.439069	30.772434	0.000001	0.86269	44.68136	258.32669	660.77411
20)	0.738818	154.090332	0.000000	5.51812	6.51063	565.85309	818.53223
21)	0.308129	179.644821	0.000000	3.20272	2.14292	503.21408	427.49051
22)	0.445688	153.749023	0.000000	3.71287	3.93280	509.26993	567.53284
23)	0.288519	186.980835	0.000000	3.15419	1.88762	504.70557	405.93958
24)	0.421008	69.434967	0.000006	1.73660	12.43421	361.36340	590.23657
25)	0.476449	187.077835	0.000000	4.66667	3.12093	559.96246	583.94733
26)	0.750772	160.908707	0.000000	5.80968	6.19497	577.95892	824.48865
27)	0.603141	197.564240	0.000000	5.89113	3.63994	601.21942	688.99530
28)	0.727499	40.298916	0.000000	1.63052	49.23381	322.46783	927.21381
29)	0.749536	177.998032	0.000000	6.35398	5.30506	602.29999	815.12720
30)	0.458599	30.759521	0.000000	0.89214	46.70675	260.69382	681.98431
31)	0.440820	48.830963	0.000002	1.31124	22.23571	314.60492	632.40045
32)	0.757005	74.974197	0.000000	2.94071	19.94248	421.86475	896.16071
33)	0.661191	154.092651	0.000000	5.06049	5.82384	553.04108	755.23535
34)	0.562687	147.456573	0.000000	4.28884	5.29576	525.27051	674.87878
35)	0.398529	118.924271	0.000037	2.70045	5.19375	447.29044	537.12659
36)	0.698850	85.290886	0.000000	3.10289	15.12932	437.79086	834.72968
37)	0.569022	156.931808	0.000000	4.57588	4.87191	540.21692	676.10010
38)	0.419369	110.029816	0.000026	2.62010	6.15206	437.67075	561.75238
39)	0.619395	103.571518	0.000010	3.36345	9.97700	462.84756	749.89478
40)	0.254020	145.111496	0.000168	2.27333	2.44191	442.44751	379.76648
41)	0.686146	46.946667	0.000000	1.78724	36.80891	339.68875	875.05695
42)	0.702958	156.939896	0.000000	5.39633	6.02326	564.32501	788.06769
43)	0.411141	148.619888	0.000069	3.38155	3.81874	493.84186	537.13037
44)	0.671093	176.531952	0.000000	5.78583	4.80782	586.73712	752.97729
45)	0.525717	119.736664	0.000022	3.37229	6.78827	475.12216	656.12781
46)	0.323726	151.894196	0.000118	2.86194	2.90607	474.22729	450.66794
47)	0.663476	84.374069	0.000000	2.95084	14.59837	431.13733	804.75903
48)	0.382964	51.526951	0.000003	1.23319	17.79214	312.40414	567.97369
49)	0.459375	197.565643	0.000000	4.76392	2.76926	568.41254	565.56610
50)	0.690213	177.411804	0.000000	5.94053	4.90813	591.35358	768.08405
51)	0.333952	145.988678	0.000099	2.82940	3.18451	469.50580	462.79968
52)	0.302949	177.848083	0.000218	3.13218	2.13919	499.36685	422.69839
53)	0.689907	130.841187	0.000000	4.51503	7.79334	521.45355	791.88965
54)	0.638884	134.475082	0.000000	4.35854	6.92051	519.08136	746.90863
55)	0.650006	122.476387	0.000000	4.06122	8.11631	501.16907	763.50677
56)	0.340853	191.176865	0.000000	3.66461	2.15747	527.23523	457.05573
57)	0.620774	95.129494	0.000008	3.12109	11.37879	446.98267	757.60236
58)	0.637174	197.961075	0.000000	6.15995	3.83445	608.55511	716.82190
59)	0.580563	98.608284	0.000010	3.05956	10.07364	447.43503	719.07678
60)	0.284390	60.076977	0.000009	1.12260	10.45017	313.02869	450.68423

max=0.000218 min=0.000000 avg=0.000020 sum=0.001214 no_mutation=0 no_cross=0

FEED 0.302949
 SPEED 177.848083
 FITNESS 0.000218

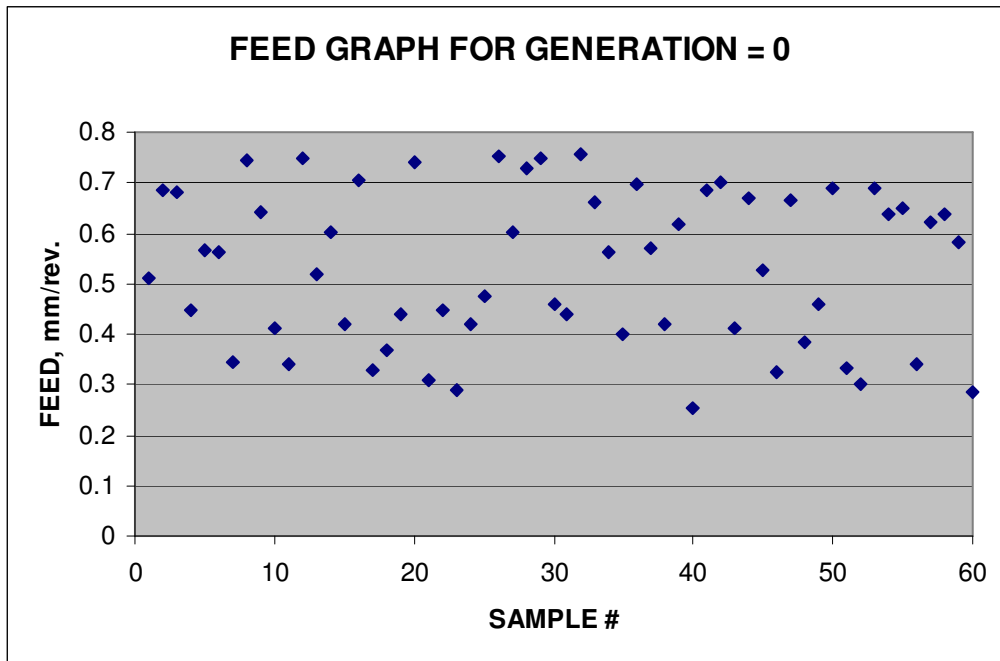


FIG. 5.5 (a)

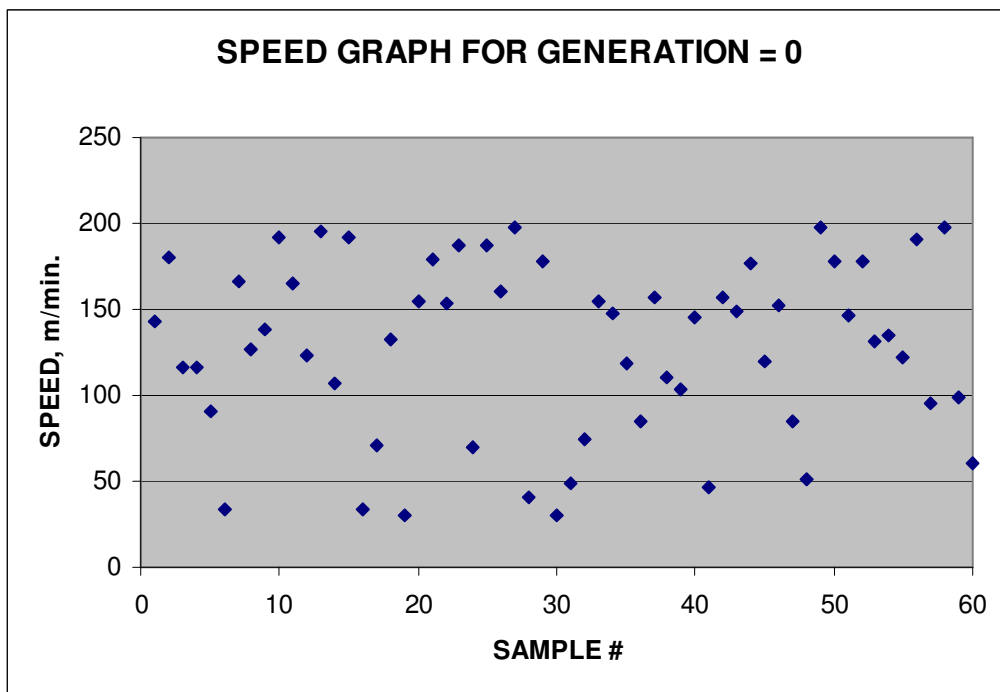


FIG. 5.5 (b)

Fig. 5.5 Speed and feed graphs for starting generation with doc = 2.54mm

TABLE 5.5(b)

Accumulated Statistics for Generation ---> 240

```

*****Calculated Constraints*****
FEED      SPEED      FITNESS      POWER      ROUGHNESS      TEMP      FORCE
*****
1)  0.254953  166.342361  0.521014    2.71700    1.81225    480.30862  372.59769
2)  0.262269  178.028809  0.507461    2.81335    1.97273    483.51126  390.29193
3)  0.254336  176.711060  0.507453    2.74384    1.78825    482.38657  372.61282
4)  0.262269  176.700684  0.509370    2.78273    1.86917    483.36621  380.99033
5)  0.262416  176.718658  0.509379    2.78420    1.86994    483.44290  381.14157
6)  0.254477  172.054337  0.513767    2.56366    1.99864    467.61911  375.01410
7)  0.254446  165.678223  0.521647    2.56470    1.99970    467.66995  375.15677
8)  0.317979  173.132172  0.000183    3.17501    2.33939    498.81601  438.99414
9)  0.264756  176.699875  0.509944    2.80328    1.88698    484.31232  383.60675
10) 0.258921  178.708466  0.505712    2.78314    1.81380    484.34454  377.02673
11) 0.258960  165.678329  0.000241    2.60013    2.03532    469.38058  379.97058
12) 0.254417  178.448532  0.505026    2.74171    1.78607    482.29379  372.31467
13) 0.255687  178.433792  0.505351    2.75218    1.79525    482.77563  373.66461
14) 0.354479  165.678299  0.000007    3.72099    2.73063    521.95825  499.99963
15) 0.271633  178.677322  0.508540    2.88870    1.90371    489.14548  390.36411
16) 0.254479  166.074554  0.521192    2.57048    1.99271    468.14670  375.10104
17) 0.255826  172.758301  0.513200    2.67440    1.88669    476.39893  375.03833
18) 0.256441  176.345337  0.508481    2.72943    1.83307    480.71716  374.90967
19) 0.254478  166.341064  0.520877    2.57419    1.98785    468.45819  375.03934
20) 0.262040  176.366104  0.509793    2.77610    1.87292    482.89905  380.82254
21) 0.254478  166.341064  0.520877    2.57419    1.98785    468.45819  375.03934
22) 0.271825  176.697418  0.511513    2.86146    1.93761    486.96268  391.00626
23) 0.254336  176.711060  0.507453    2.71700    1.81225    480.30862  372.59769
24) 0.254483  165.678452  0.521658    2.56500    1.99998    467.68423  375.19595
25) 0.256461  176.700684  0.507989    2.73455    1.82762    481.12671  374.85495
26) 0.254336  176.711060  0.507453    2.71700    1.81225    480.30859  372.59766
27) 0.262911  176.698135  0.509523    2.78801    1.87381    483.60864  381.66739
28) 0.271825  176.365387  0.511998    2.85662    1.94316    486.58307  391.08075
29) 0.254587  176.699860  0.507531    2.71894    1.81422    480.39453  372.86737
30) 0.256463  165.678299  0.000246    2.58055    2.01561    468.43735  377.31064
31) 0.254478  176.302002  0.508056    2.71252    1.81967    479.90274  372.83630
32) 0.262415  166.403534  0.000238    2.63750    2.04893    471.52789  383.46979
33) 0.398314  176.207367  0.000000    3.84531    2.85562    526.44177  515.95184
34) 0.270831  123.842369  0.000091    2.07215    3.31358    419.74664  404.26477
35) 0.262393  172.754486  0.514880    2.72774    1.93537    478.90582  381.99384
36) 0.259790  175.410797  0.510598    2.74404    1.87217    480.95123  378.65659
37) 0.264756  172.056625  0.516407    2.73690    1.96493    478.99240  384.64294
38) 0.322414  177.362778  0.000000    3.27999    2.28668    505.27603  442.34155
39) 0.254479  133.707352  0.000130    2.11486    2.77043    427.78397  383.42960
40) 0.258293  174.034576  0.512121    2.71240    1.88375    478.80798  377.37439
41) 0.264757  176.699875  0.509944    2.80328    1.88699    484.31241  383.60706
42) 0.254479  176.690811  0.507517    2.71791    1.81359    480.34186  372.75409
43) 0.254467  166.052368  0.521215    2.57009    1.99302    468.11633  375.09387
44) 0.258921  176.698715  0.508585    2.75496    1.84525    482.07803  377.45892
45) 0.254448  177.912628  0.505794    2.73456    1.79447    481.70462  372.46085
46) 0.258797  178.067047  0.506608    2.77312    1.82286    483.57480  377.03311
47) 0.383440  176.693405  0.000000    3.74211    2.73708    522.91034  501.77011
48) 0.256463  176.355728  0.508472    2.72976    1.83307    480.73764  374.93121
49) 0.258921  176.698715  0.508585    2.75496    1.84525    482.07803  377.45892
50) 0.271825  176.697418  0.511513    2.86146    1.93761    486.96268  391.00626
51) 0.254480  176.690811  0.507517    2.71792    1.81360    480.34222  372.75507
52) 0.254479  165.678299  0.521657    2.56497    1.99996    467.68265  375.19202
53) 0.254943  166.065933  0.521339    2.57402    1.99651    468.31387  375.59930
54) 0.255827  172.758301  0.513200    2.67441    1.88669    476.39926  375.03931
55) 0.254479  176.192764  0.508208    2.71101    1.82139    479.77972  372.86066
56) 0.274169  176.684677  0.512032    2.88049    1.95460    487.81528  393.44971
57) 0.254479  165.678299  0.521657    2.56497    1.99996    467.68262  375.19199
58) 0.262415  176.366104  0.509880    2.77920    1.87562    483.04233  381.21771
59) 0.254477  172.054337  0.513767    2.65362    1.88838    475.07074  373.75748
60) 0.254479  165.678299  0.521657    2.56497    1.99996    467.68262  375.19199

```

max=0.521658 min=0.0000 avg=0.435470 sum=26.128193 no_mutation=17695 no_cross=4362

```

FEED      0.254483
SPEED    165.678452
FITNESS   0.521658

```

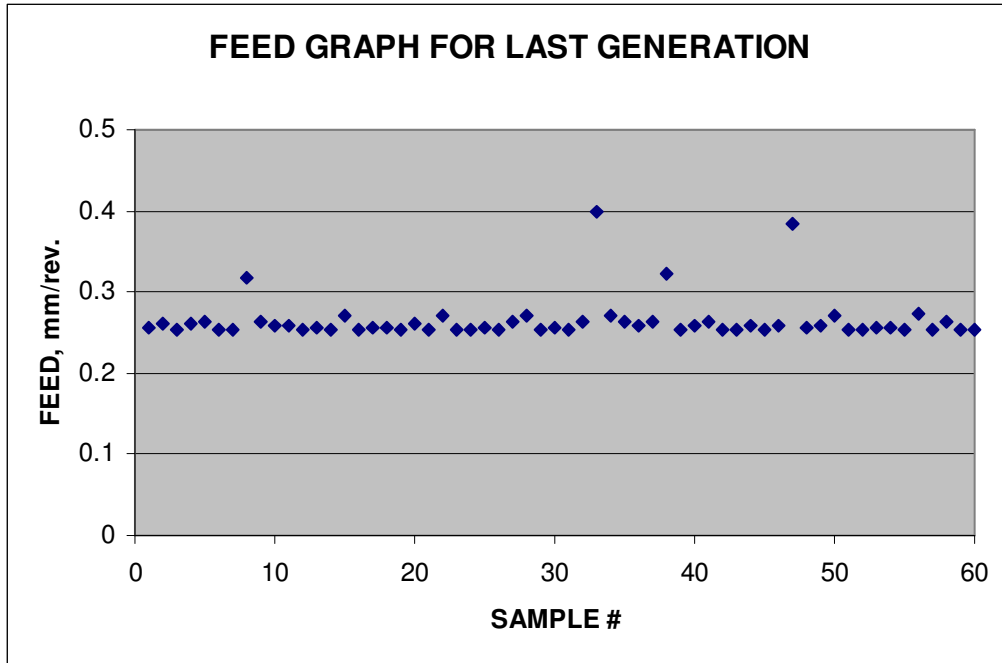


FIG. 5.5 (c)

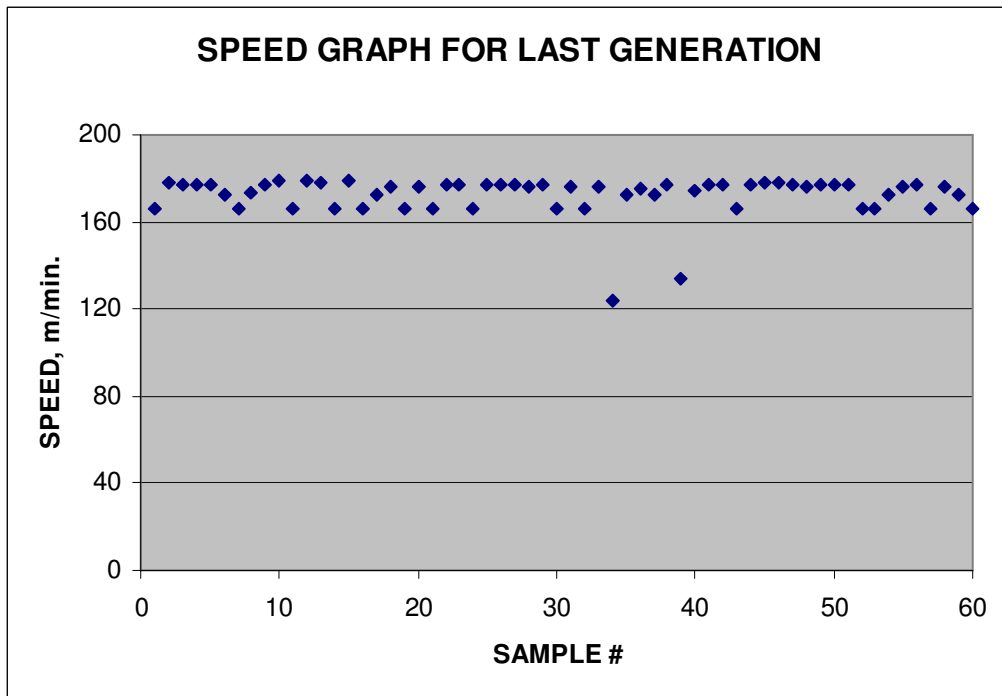


FIG. 5.5 (d)

Fig. 5.5 Speed and feed graphs for last generation with doc = 2.54mm

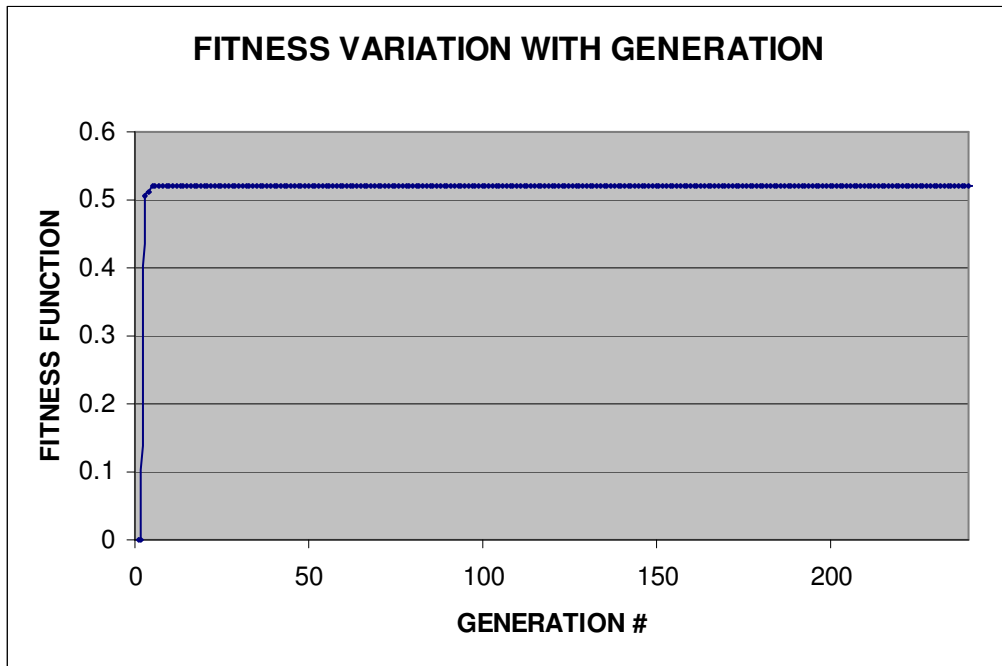


FIG. 5.5 (e)

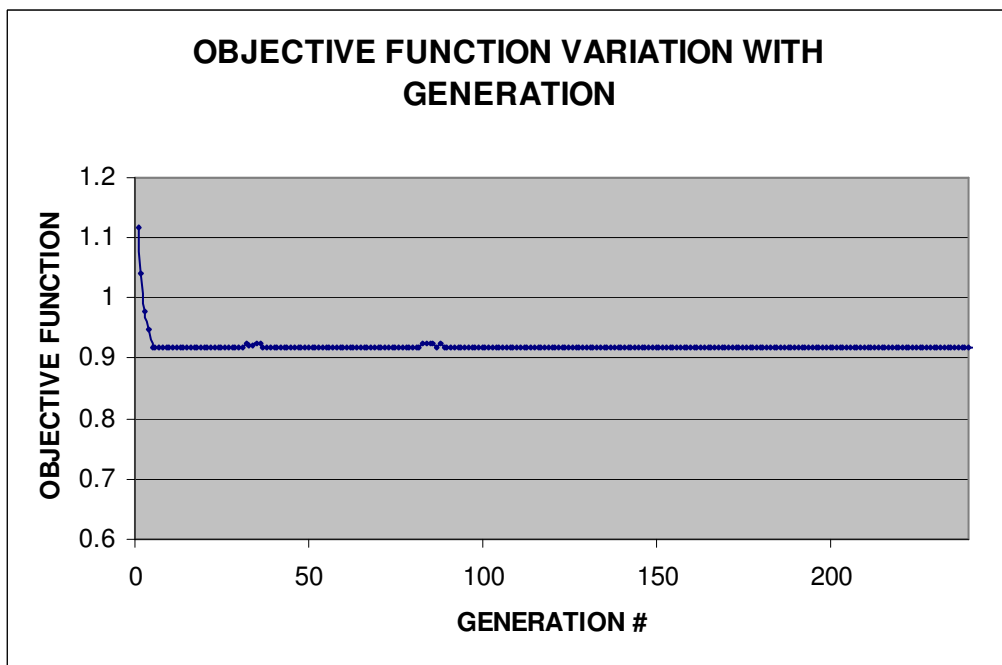


FIG. 5.2 (f)

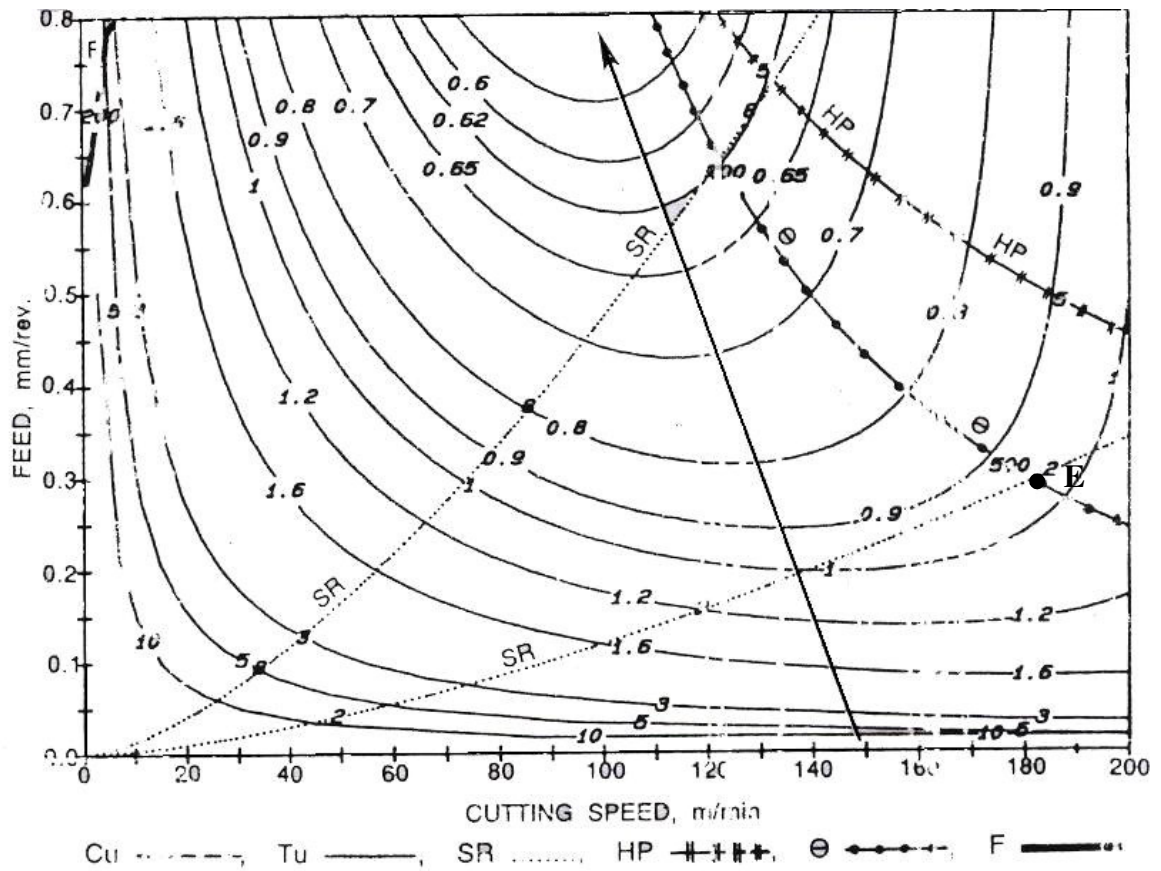


FIG. 5.5(g) Location of best result found by GA on the contours given by Agapiou [6], for $d_{oc} = 2.54$ mm and the constraints of power, force, surface roughness, and temperature.

In the section 5.6, the combined objective function is taken that includes both the total production cost and the total production time with weight coefficients 0.6 and 0.4 respectively, and depth of cut, $doc = 5.08$ mm having the constraints force, surface roughness, temperature and power.

Machining parameters used for the example are::

Parameter	Value
SR_{max}	8 μm
HP_{max}	5 KW
F_{max}	1200 N
T_{max}	500 deg C
λ	0.244

Fig. 5.6(e) and fig. 5.6(f), shows the variation of best fitness function and the objective function with generation, respectively. These figures clearly show how the values of both these functions get improved with generation after applying the GA operations. From fig. 5.6(f), the best value of the objective function is approximated to be 0.96076685. It is clear from table 5.6(b) that the constraints surface roughness = 7.98187 μm , force = 1002.70300 N and temperature = 429.58472 deg C have their extreme limits for the calculated best objective function value. From fig. 5.6(g), that we have from J. S. Agapiou [6], the value of objective function lies at point F (nearer to 0.9) that justifies our objective function value.

5.6 COMBINED OBJECTIVE FUNCTION with doc = 5.08mm

TABLE 5.6(a)

Accumulated Statistics for Generation ---> 0
 *****Calculated Constraints*****

	FEED	SPEED	FITNESS	POWER	ROUGHNESS	TEMP	FORCE
1)	0.612423	122.740631	0.000000	6.53275	9.06201	534.21497	1229.52637
2)	0.678436	119.421120	0.000000	6.90330	10.47029	539.48773	1327.93176
3)	0.273445	192.543091	0.000000	5.22325	2.03434	544.71033	654.70929
4)	0.455292	63.933033	0.000003	2.88221	18.13459	382.96829	1059.44971
5)	0.264219	76.250244	0.000015	2.20930	8.03401	367.88660	701.44403
6)	0.650119	48.781765	0.000000	2.98313	39.11834	368.43069	1409.74121
7)	0.433076	196.774963	0.000000	7.62429	3.12294	604.27960	911.73737
8)	0.408484	78.017464	0.000000	3.16808	12.01642	406.87524	959.76056
9)	0.339722	143.846878	0.000000	4.75875	3.94027	504.99344	789.24060
10)	0.627434	80.237244	0.000000	4.54096	17.71715	450.16055	1306.36230
11)	0.736122	186.309845	0.000000	10.97842	5.78025	658.95209	1346.80322
12)	0.607295	154.015030	0.000000	7.96095	6.36392	585.66266	1194.27600
13)	0.312628	95.397766	0.000000	3.08186	6.76701	418.48077	774.65448
14)	0.358075	190.530197	0.000000	6.38519	2.70977	573.38794	796.91309
15)	0.699571	116.513130	0.000000	6.91533	11.21008	537.41553	1361.19263
16)	0.352511	163.008270	0.000000	5.48138	3.38135	535.88605	800.46680
17)	0.698644	163.512863	0.000000	9.37179	6.68838	617.84869	1313.99219
18)	0.726852	117.241928	0.000000	7.16488	11.53912	543.07697	1398.58960
19)	0.263216	192.980759	0.000000	5.08058	1.95119	540.94476	636.71417
20)	0.705009	88.909630	0.000000	5.45447	17.04012	481.27261	1406.86670
21)	0.681566	66.276970	0.000000	4.07821	25.74292	422.94955	1414.26025
22)	0.624260	44.120346	0.000000	2.64038	43.75054	350.22220	1382.86108
23)	0.671521	102.112976	0.000000	5.94821	13.14777	504.58365	1339.17883
24)	0.725819	79.240639	0.000000	5.03044	20.90057	461.59131	1453.70898
25)	0.624508	66.033371	0.000000	3.79676	23.71192	414.67221	1327.89282
26)	0.582016	194.911255	0.000000	9.51939	4.26314	639.65643	1130.72607
27)	0.279201	56.053886	0.000005	1.74851	13.55525	327.00296	753.17596
28)	0.288975	105.644295	0.000000	3.17716	5.35482	429.55847	724.18250
29)	0.387278	186.852264	0.000000	6.66980	3.01985	578.06677	845.18927
30)	0.382324	174.342209	0.000000	6.20391	3.31220	560.28607	843.23529
31)	0.670497	100.350288	0.000000	5.84875	13.47974	500.79956	1340.06018
32)	0.612311	168.627701	0.000000	8.69322	5.59082	608.97437	1190.43860
33)	0.678965	199.990311	0.000000	10.98640	4.78551	667.24371	1261.06421
34)	0.640633	41.220367	0.000000	2.53433	49.79124	342.20776	1418.79980
35)	0.295305	176.637543	0.000000	5.13207	2.50538	534.06476	698.32422
36)	0.514001	191.465591	0.000000	8.50237	3.86649	618.95789	1035.17371
37)	0.340393	160.476776	0.000000	5.25924	3.34326	528.59454	781.66071
38)	0.329614	158.465591	0.000000	5.07099	3.29962	522.35754	764.61200
39)	0.432540	116.725510	0.000000	4.76054	6.89867	486.88077	960.40643
40)	0.631769	68.513145	0.000000	3.96040	22.68150	422.11276	1334.07825
41)	0.460225	110.510033	0.000000	4.75647	7.97882	482.11932	1010.17548
42)	0.577692	122.926353	0.000000	6.25044	8.52649	528.13702	1178.39026
43)	0.394405	175.138046	0.000000	6.38240	3.39371	564.95477	862.07220
44)	0.715556	77.832420	0.000000	4.89523	21.17315	456.81143	1441.39258
45)	0.551581	64.535622	0.000000	3.37584	21.67542	400.21024	1216.39380
46)	0.687958	76.484352	0.000000	4.67326	20.90110	449.81314	1403.35254
47)	0.475531	104.925789	0.000000	4.65693	8.92141	475.07175	1039.87097
48)	0.263354	55.109398	0.000006	1.64525	13.11735	320.68817	723.17828
49)	0.514130	180.512177	0.000000	8.06491	4.22975	604.16010	1041.55981
50)	0.272018	60.149509	0.000007	1.82558	11.86289	335.02359	733.81616
51)	0.291924	150.163879	0.000000	4.39467	3.16985	498.17111	704.00317
52)	0.640047	89.955063	0.000000	5.11181	15.19166	474.01068	1310.09033
53)	0.544707	178.785309	0.000000	8.36397	4.54831	608.97345	1087.16907
54)	0.478318	76.765381	0.000000	3.53130	14.43017	417.66650	1077.87280
55)	0.255900	78.322708	0.472239	2.20750	7.46931	369.55963	683.50269
56)	0.431421	197.652527	0.000000	7.63206	3.08999	604.91095	908.80121
57)	0.389283	170.275650	0.000000	6.15958	3.49593	556.92419	856.38147
58)	0.386755	99.719345	0.000000	3.78624	7.83301	445.58746	899.81903
59)	0.683114	38.688187	0.000000	2.51670	58.47891	337.72919	1495.98108
60)	0.451550	62.037014	0.000003	2.78717	18.82708	377.51828	1056.34741

max=0.472239 min=0.000000 avg=0.007871 sum=0.472280 no_mutation=0 no_cross=0

FEED 0.255900
 SPEED 78.322708
 FITNESS 0.472239

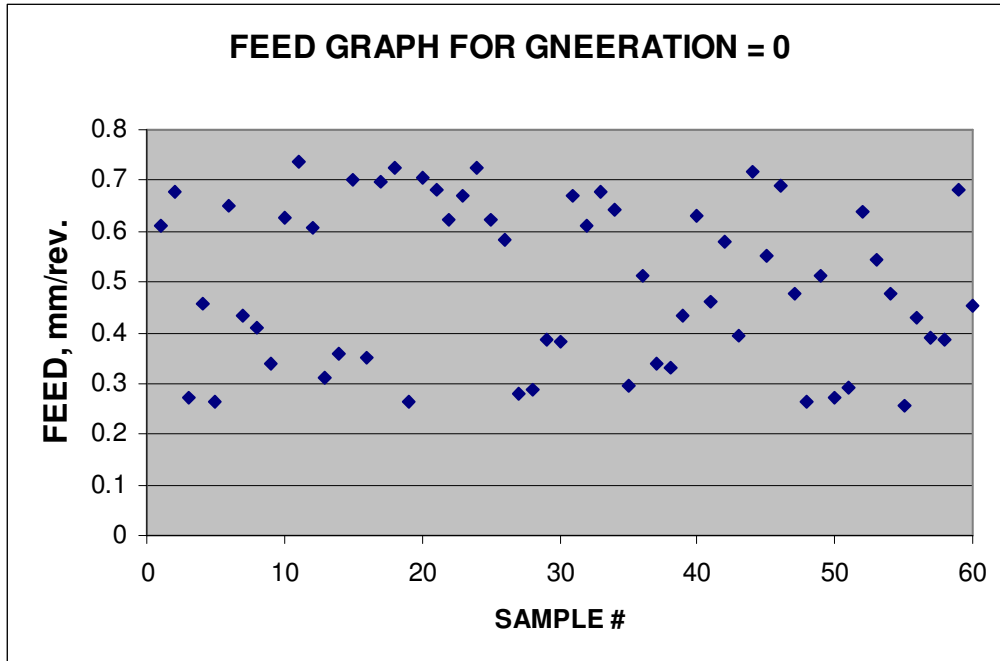


FIG. 5.6 (a)

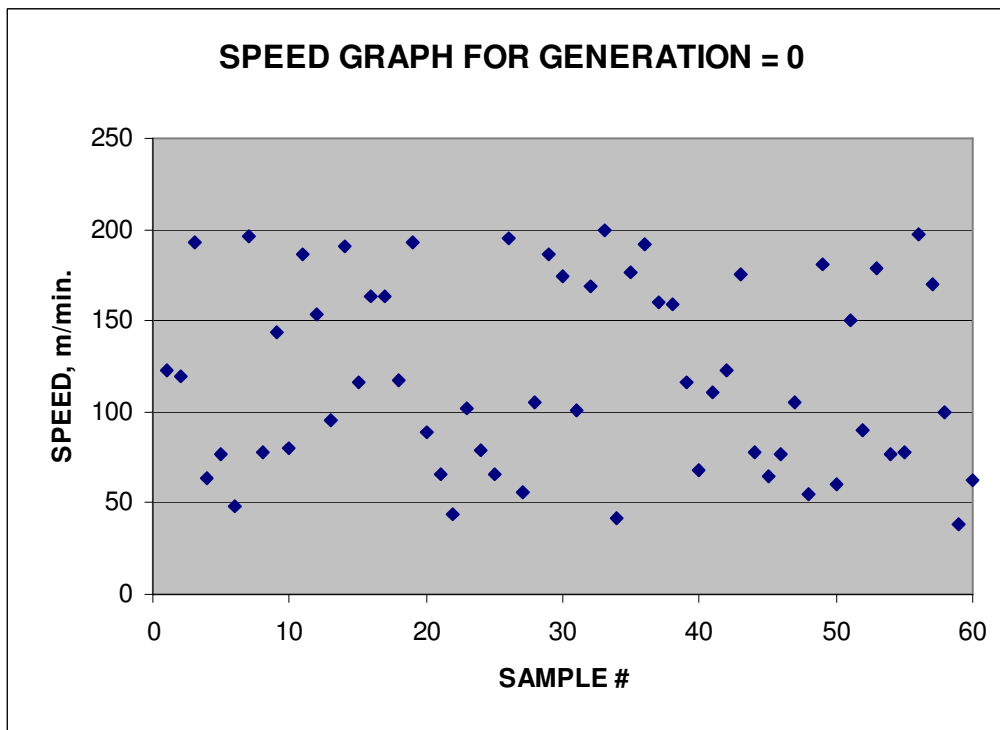


FIG. 5.6 (b)

Fig. 5.6 Speed and feed graphs for starting generation with doc = 5.08mm

TABLE 5.6(b)

Accumulated Statistics for Generation ---> 240

```

*****Calculated Constraints*****
FEED      SPEED      FITNESS      POWER      ROUGHNESS      TEMP      FORCE
*****
1)  0.311328  85.665413  0.509459  2.78831  7.93622  399.75247  780.78235
2)  0.312612  90.499306  0.000061  2.79940  8.00041  400.09976  784.47687
3)  0.286935  90.739250  0.000608  2.77527  8.01234  398.84055  781.64014
4)  0.309826  85.168518  0.508495  2.76331  7.96793  398.37927  778.50842
5)  0.286757  85.571175  0.497406  2.61254  7.31972  392.76245  735.68793
6)  0.311450  41.224251  0.000002  1.44407  24.13330  293.86212  841.06909
7)  0.311450  85.737190  0.509553  2.79127  7.92924  399.92514  780.93823
8)  0.311330  85.665359  0.509460  2.78832  7.93628  399.75287  780.78595
9)  0.302805  85.572502  0.505409  2.72593  7.73084  397.26059  765.31067
10) 0.302805  85.333282  0.505270  2.71907  7.76381  396.79611  765.52795
11) 0.286881  84.139290  0.496457  2.57403  7.51314  390.03564  737.17688
12) 0.312612  84.420120  0.000015  2.76065  8.14844  397.65570  784.27814
13) 0.312612  85.582314  0.510005  2.79484  7.98084  399.93411  783.19263
14) 0.311454  85.737190  0.509555  2.79130  7.92934  399.92618  780.94525
15) 0.281688  85.665359  0.494807  2.57900  7.17779  391.48053  726.15497
16) 0.298927  85.415611  0.503439  2.69421  7.65277  395.88840  758.33435
17) 0.312612  85.499306  0.509961  2.79240  7.99263  399.77200  783.26959
18) 0.311082  85.665359  0.509346  2.78659  7.92993  399.68631  780.33490
19) 0.311454  85.415611  0.509385  2.78187  7.97476  399.29877  781.24255
20) 0.302892  85.333282  0.505312  2.71968  7.76606  396.82004  765.68805
21) 0.312612  85.499306  0.509961  2.79240  7.99263  399.77200  783.26959
22) 0.312612  85.582314  0.510005  3.24943  7.98187  429.58472  1002.70300
23) 0.255185  85.739250  0.479759  2.38955  6.49138  383.61005  675.89508
24) 0.373078  85.618568  0.000000  3.20938  9.52513  415.04495  890.27832
25) 0.311454  85.737190  0.509555  2.79130  7.92934  399.92618  780.94525
26) 0.311328  85.500641  0.509372  2.78349  7.95948  399.43103  780.93463
27) 0.311546  85.623856  0.509538  2.69077  7.72258  395.47272  760.28381
28) 0.311330  85.665359  0.509460  2.78832  7.93628  399.75287  780.78595
29) 0.306779  85.760201  0.507398  2.75923  7.80667  398.70929  772.40820
30) 0.286881  84.388313  0.496643  2.58088  7.47947  390.51804  736.95624
31) 0.311327  85.483437  0.509363  2.78298  7.96190  399.39731  780.94971
32) 0.310865  85.636757  0.509231  2.78424  7.92840  399.57230  779.96649
33) 0.302805  85.572502  0.505409  2.72593  7.73084  397.26059  765.31067
34) 0.310748  85.664673  0.509192  2.78424  7.92148  399.59537  779.72839
35) 0.312612  85.499306  0.509961  2.79240  7.99263  399.77200  783.26959
36) 0.306779  85.760201  0.507398  2.75923  7.80667  398.70929  772.40820
37) 0.311314  85.483444  0.509357  2.78288  7.96155  399.39368  780.92499
38) 0.311330  85.636787  0.509445  2.78749  7.94030  399.69717  780.81238
39) 0.302752  88.376053  0.000000  2.80579  7.35987  402.63278  762.71942
40) 0.311454  106.987183  0.000000  3.40684  5.66331  438.61160  763.62347
41) 0.310834  85.665359  0.509232  2.78486  7.92358  399.61975  779.88385
42) 0.309826  85.665314  0.508767  2.77781  7.89780  399.34866  778.05005
43) 0.309826  85.621216  0.508743  2.77653  7.90398  399.26276  778.09064
44) 0.311206  85.664665  0.509403  2.78744  7.93320  399.71826  780.56122
45) 0.311330  85.001297  0.000016  2.76886  8.03071  398.45514  781.40167
46) 0.311454  84.409065  0.000015  2.75235  8.11975  397.32568  782.18103
47) 0.439550  42.999306  0.000001  1.96231  31.98939  321.77167  1075.10632
48) 0.311546  85.168571  0.000016  5.07521  2.70499  529.33575  713.50610
49) 0.311330  85.636787  0.509445  2.78749  7.94030  399.69717  780.81238
50) 0.311454  85.621216  0.509494  2.78790  7.94567  399.70007  781.05231
51) 0.301888  89.721672  0.000000  2.83788  7.17215  404.94019  759.97705
52) 0.286877  85.126953  0.497169  2.60118  7.38095  391.94281  736.29895
53) 0.302805  85.572830  0.505409  2.72594  7.73079  397.26123  765.31036
54) 0.311546  85.623856  0.509538  2.78862  7.94767  399.73001  781.21796
55) 0.302892  85.737190  0.505544  2.73126  7.71052  397.60394  765.32190
56) 0.305501  85.333282  0.506557  2.73793  7.83320  397.53168  770.46283
57) 0.311327  85.483437  0.509363  2.78298  7.96190  399.39728  780.94946
58) 0.311454  85.737190  0.509555  2.79130  7.92934  399.92618  780.94525
59) 0.301888  85.168571  0.504730  2.70794  7.76298  396.22476  763.99707
60) 0.311546  85.167267  0.000016  2.77523  8.01252  398.83798  781.64124

```

max=0.510005 min=0.000000 avg=0.413583 sum=24.814966 no_mutation=21544 no_cross=5411

```

FEED      0.312612
SPEED     85.582314
FITNESS   0.510005

```

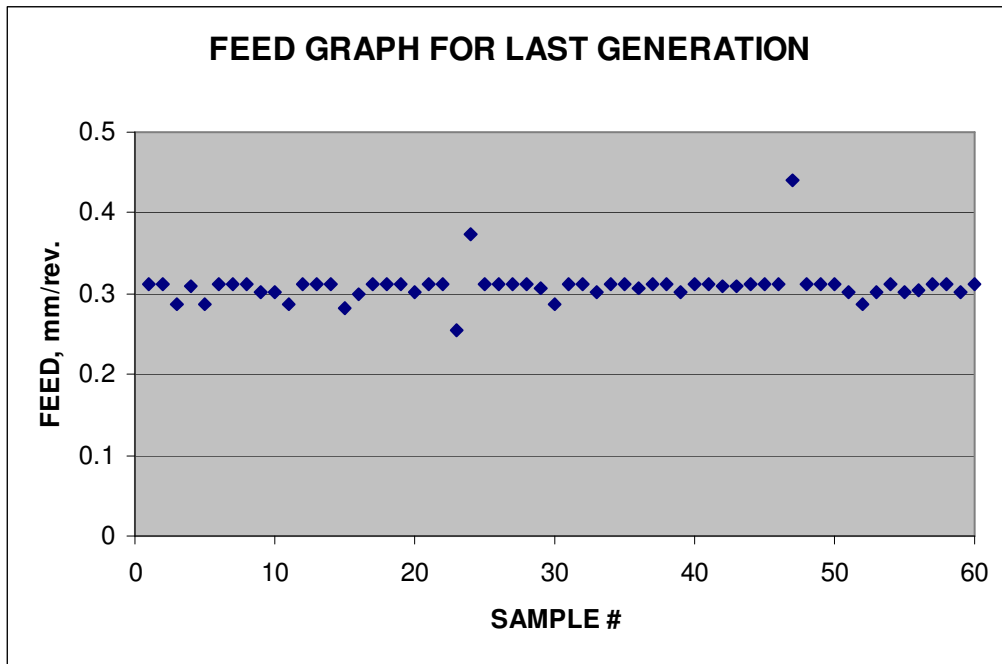


FIG. 5.6 (c)

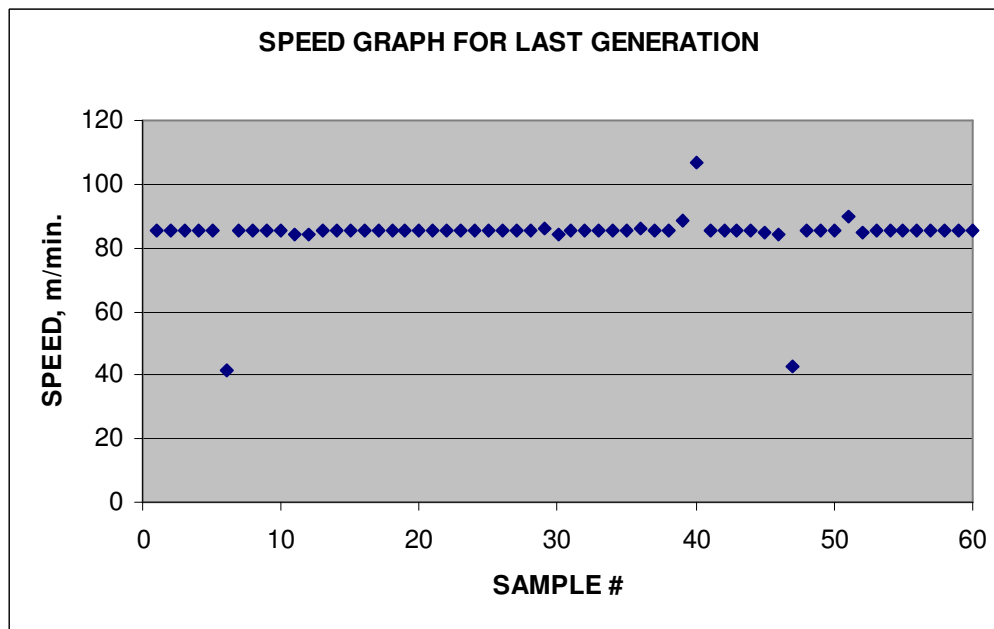


FIG. 5.6 (d)

Fig. 5.6 Speed and feed graphs for last generation with doc = 5.08mm

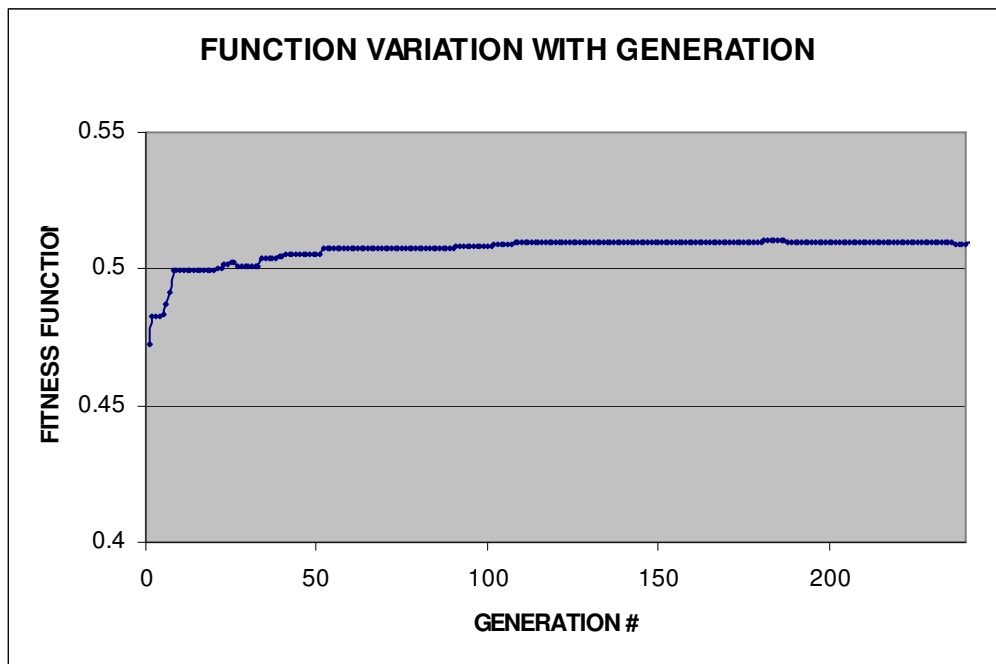


FIG. 5.6 (e)

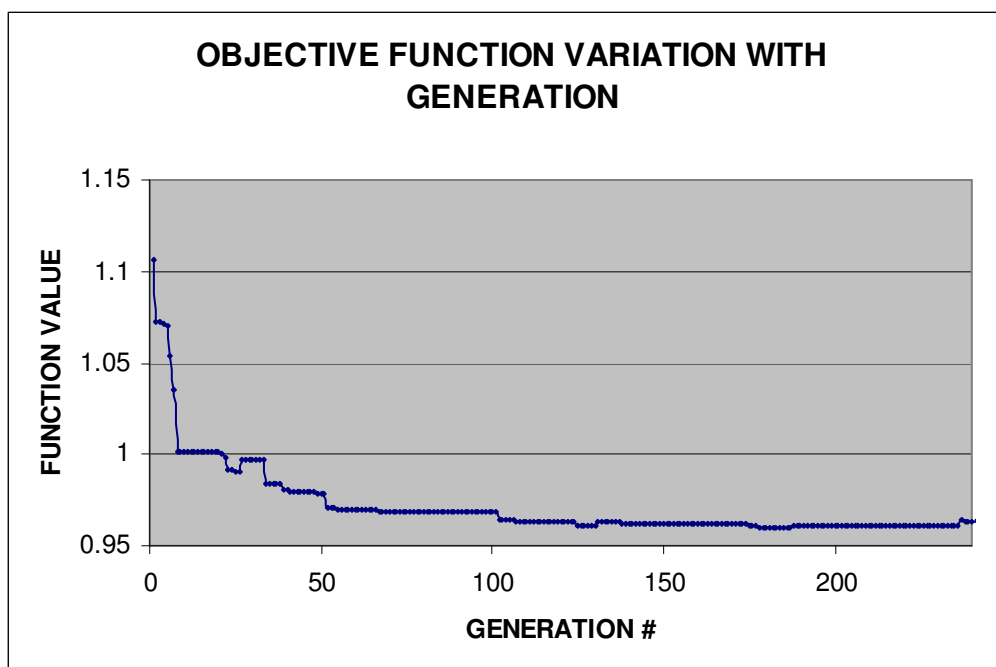


FIG. 5.6 (f)

CHAPTER 6

SCOPE OF FURTHER WORK

In the present work, the cutting conditions such as feed and speed are optimized based on the total production cost, total production time and combined of these two, as objective functions by taking into consideration the various constraints such as feed, cutting speed, power, cutting force, temperature, and surface roughness. Where as, there are other constraints also such as dimensional accuracy, rigidity and reliability of the system etc. that could also be considered.

Here the optimization is done only for the single-pass turning operation that can also be further extended to the multi-pass operations.

Tool selection, machine selection, process selection and tool path selection are the other important areas for optimization in process planning. Besides this, the sequencing and scheduling optimization are the other important areas for the GA implementation. Also the other advanced GA operators for reproduction, crossover and mutation could be applied to the optimization problem.

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