

**Preparation and Characterization of SrFe<sub>12</sub>O<sub>19</sub>/  
Ba<sub>2</sub>Co<sub>2</sub>Fe<sub>12</sub>O<sub>22</sub> Composite Hexaferrite**

*Dissertation submitted in partial fulfillment of the requirement for the Degree of*

**MASTER OF SCIENCE**

BY

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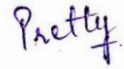
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## CERTIFICATE

I hereby certify that the present work in thesis '**Preparation and Characterization of SrFe<sub>12</sub>O<sub>19</sub>/Ba<sub>2</sub>Co<sub>2</sub>Fe<sub>12</sub>O<sub>22</sub> composite hexaferrite**' in the partial fulfillment of the requirement for the award of the degree of Master of Science (M. Sc.) in Physics in School of Physics and Materials Science, Thapar Institute of Engineering & Technology, Patiala is an authentic record of my own work carried out under the supervision of Dr. Puneet Sharma. The matter embodied in this thesis has not been submitted in part or full to any other institute/university for the award of any degree.



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This is to certify that the above mentioned statement of the student is correct to the best of my knowledge and belief.



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## Abstract

In the present work, composites of  $\text{SrFe}_{12}\text{O}_{19}$  (SrM)/ $\text{Ba}_2\text{Co}_2\text{Fe}_{12}\text{O}_{22}$  ( $\text{Co}_2\text{Y}$ ) in different weight ratio (98/2, 96/4, 94/6, 92/8) were prepared. Their structural, morphological and magnetic properties were investigated using various techniques; viz. X-ray diffraction (XRD), Field Emission Scanning Electron Microscope (FE-SEM), Raman Spectroscopy and Vibrating Sample Magnetometer (VSM). X-ray diffraction pattern confirmed the co-existence of both phases in composites which is also supported by Raman analysis. The magnetic measurements show non-linear rise in saturation magnetization with the  $\text{Co}_2\text{Y}$  content, while the coercivity drastically decreases. Smooth demagnetization curve of sintered composites confirmed the well-exchange coupling between M-Y phases within the studied composition range.

# Chapter 1

## Introduction

### **Overview**

This chapter provides a general introduction to ferrites and their crystal structures. Classification of ferrites based upon magnetic and structural properties has been described. A brief description about exchange coupling and exchange-spring mechanism are given. Some important applications of exchange coupled composites are mentioned. The chapter concludes with the motivation and objectives for the present work.

## 1.1 Ferrites

Ferrites are ceramic materials composed of iron oxide ( $\text{Fe}_2\text{O}_3$ ) along with other metal oxides having general chemical formula  $\text{A}(\text{Fe}_x\text{O}_y)$ , where A(divalent ion): Co, Zn, Ni, Ba, or Sr[1]. They were first investigated by Snoek et. al in 1930's[2]. Ferrites are known for their high electrical resistivity and minimal eddy current losses, which makes them plausible candidate for use in high-frequency electromagnetic fields, permanent magnets, magnetic sensors, etc[3].

Based on magnetic characteristics ferrites are classified as soft and hard ferrites. Soft ferrites have a low coercive force and are easily magnetized and demagnetized, making them ideal for use in electrical device applications. Whereas, hard ferrites have a high coercive force and are difficult to magnetize and demagnetize; which makes them suitable for use in permanent magnets [4]. Further on the basis of their crystal structure, Spinel and garnet ferrites (cubic), hexaferrites (hexagonal), and orthoferrites (perovskite) are the four major types of ferrites. [5].

**Table 1.1: Classification of ferrites based on their magnetic and microwave properties**

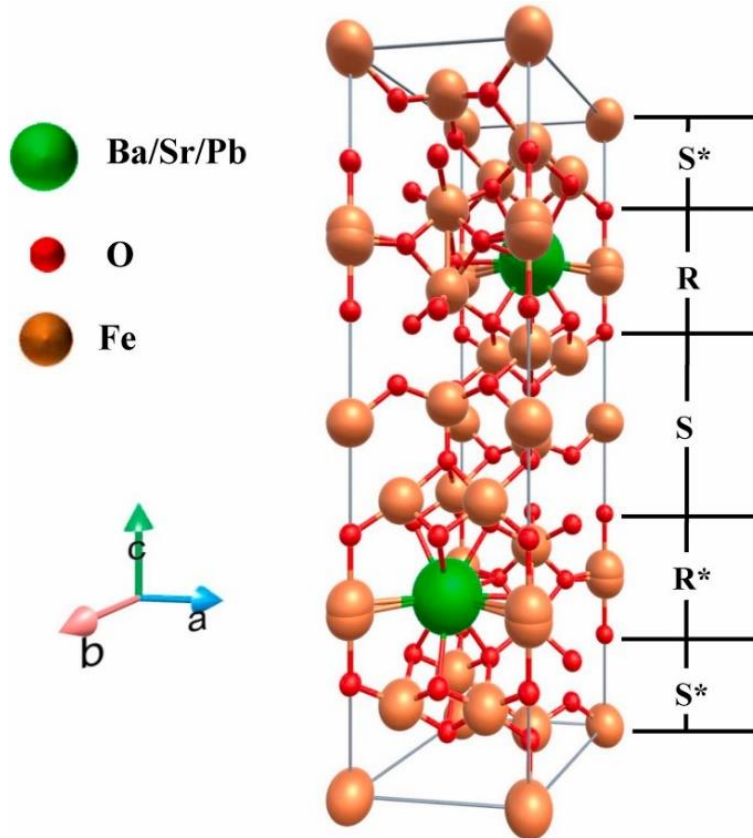
Crystal Structure	Type	Example	Ms (G)	Hc (Oe)	Ha (Oe)	Operable Frequency (GHz)
Cubic	Spinels	$\text{NiFe}_2\text{O}_4$	3200			0.750
		$\text{CoFe}_2\text{O}_4$	5300	1566	6800	
	Garnets	$\text{Y}_3\text{Fe}_5\text{O}_{12}$	1750		82	<1
Hexaferrites	M	$\text{BaFe}_{12}\text{O}_{19}$	4000	3187	17460	Upto 36
		$\text{SrFe}_{12}\text{O}_{19}$	4320	3193	20000	
	Y	$\text{Ba}_2\text{Co}_2\text{Fe}_{12}\text{O}_{22}$	2300	60	28,000	Upto 14
	Z	$\text{Ba}_3\text{Co}_2\text{Fe}_{24}\text{O}_{41}$	3390	23	12000	1.3
	X	$\text{Ba}_2\text{Me}_2\text{Fe}_{28}\text{O}_{46}$	3400	50	9500	3
	W	$\text{BaMe}_2\text{Fe}_{16}\text{O}_{27}$	4800	80	21000	3
U	$\text{Ba}_4\text{Co}_2\text{Fe}_{36}\text{O}_{60}$	4200	2600	10000	30	
Orthoferrites	Pervoskite	$\text{GdFeO}_3$	5035	729		

Spinel and Garnets are traditional ferrites having cubical crystal symmetry which leads to low magnetocrystalline anisotropy ( $H_a$ ) and restricts their operational frequency below 3 GHz, however with substitution their application can be enhanced above X band [6].

On the other hand, the hexagonal crystal symmetry of hexaferrites leads to high  $H_a$  due to which they are commonly employed in high frequency application devices such as microwave absorbers, antenna substrates as well as in non-reciprocal devices[7].

## 1.2 M-type ferrite

Among the family of hexaferrites, M-type-ferrites also known as magnetoplumbite have received substantial interest in recent decades due to their remarkable properties, which include extremely high coercivity( $H_c$ ), saturation magnetization( $M_s$ ), and strong magnetic uniaxial anisotropy along the  $c$ -axis which makes them suitable candidate for microwave absorbers in the GHz range[8,9]. Their general chemical formula is  $MFe_{12}O_{19}$ , where M: Ba, Sr and Pb. The crystal structure of these ferrites consists of spinel blocks containing two oxygen layers separated by a hexagonal block containing the divalent ion. It is denoted as  $RSR^*S^*$ , where R denotes hexagonal symmetry and S spinel structure. The asterisk (\*) represents the structure's  $180^\circ$  rotation [10]. In the unit cell of M-type hexaferrites,  $Fe^{+3}$  ions situated at various crystallographic sites i.e. octahedral, tetrahedral and hexahedral, in which 12k,2a,2b sites are spin up whereas 4f1 and 4f2 are spin down, which are responsible for the net magnetization which is approximately  $40 \mu B$ [11].



**Fig. 1.1** Crystal structure of M-type hexaferrite [10].

### 1.3 Y-type ferrite

The first ferroplana ferrites to be found were the  $Zn_2Y$  and  $Co_2Y$  ferrites, all Y-type ferrites preferred plane of magnetization perpendicular to the  $c$ -axis at room temperature. These ferrites have chemical formula  $Ba_2Me_2Fe_{12}O_{22}$ , where Me is a divalent cation[12]. As illustrated in [fig. 1.2](#), one hexagonal unit cell of Y-type has just S and T blocks. The T block is stacked at the bottom of the unit cell, and the S block is piled on top of it. A T\* block (the asterisk (\*) indicates a  $120^\circ$  rotation along the  $c$ - axis) and a S\*\* block are piled on top of the first two blocks. S and T blocks are layered to form the unit cell of Y-type hexaferrite[13]. Among the hexaferrites they are a type of soft ferrites with high magnetic permeability and low dielectric losses, making them a viable



1990s, Kneller and Hawing were the first to present the notion of exchange-spring magnets in hard and soft magnetic materials [16].

The exchange-spring phenomena is defined as the interaction of hard and soft magnetic spins at the interface. In 2003, V.M Chakka et al.[17] explained these interactions by using two types of spin reversal mechanisms i.e. coherent and non-coherent. If the two phases are strongly coupled, a coherent rotation of spins occurred at the interface which makes smooth hysteresis curve. In contrast, a stepped  $M-H$  loop denotes an uncoupled system, in which the rotation of spins are non-coherent at the interface. As exchange coupling is interfacial in nature, it is greatest near the interface and gradually decreases with distance away from the contact. The distance up to which exchange coupling predominate is referred to as exchange length.

In the case of nanoparticles, coupling is highly influenced by particle size distribution whereas in the case of thin films, the quantity of coupling is governed by the thickness of the film [18]. Many aspects, including as synthesis technique and annealing temperature, influence the coupling phenomena.[19]. As a combination of high and low FMR phase, composite ferrites are useful material which operates across a wide frequency range.

## **1.5 Synthesis methods for ferrites**

Ferrites are synthesized using several processing techniques because their electrical and magnetic properties are extremely vulnerable to the synthesis methods. The following are some of the most widely used techniques.

- Solid-state ceramic route
- Sol- gel auto combustion method
- Hydrothermal synthesis
- Chemical co-precipitation

In the present study, composites of SrM and Co<sub>2</sub>Y were synthesized via solid-state ceramic route.

The experimental section explains the synthesis mechanism.

### **1.6 Applications of Exchange-Coupled composite ferrites:**

Exchange-coupled composite ferrites have emerged as versatile materials with various applications. Their unique magnetic properties and exchange coupling behavior open up a range of possibilities for their utilization. The interaction of hard and soft magnetic phases improves magnetic stability and noise reduction in magnetic recording medium such as hard disc drives (HDDs) and magnetic tapes, resulting in increased data storage and retrieval capabilities[20]. In microwave devices, exchange-coupled composite ferrites find use in circulators, isolators, and phase shifters[21]. Their exchange coupling behavior enables efficient control and manipulation of microwave signals, facilitating effective signal routing and isolation in communication systems[10]. Moreover, these ferrite composites have potential in magnetic sensors, offering improved sensitivity and selectivity in detecting magnetic fields for applications such as position sensing, proximity detection, and non-destructive testing[22]. Furthermore, exchange-coupled composite ferrites show potential in biological applications such as magnetic hyperthermia therapy, where their magnetic characteristics can be used to selectively target and destroy cancer cells.[23].

## 1.7 Motivation

Modern microwave ferrites have piqued the interest of the microwave sector because of their distinctive electrical and magnetic properties. However, low anisotropic ferrites with low FMR can only be used in the MHz range, whereas high FMR ferrites can be used in the GHz range. As a result, current emphasis has been placed on composite ferrites, which may be used throughout a large frequency spectrum. Several studies have reported exchange coupling between hard/soft composites, but no data on hard/hard composites are known. The structural and magnetic properties of composites of  $\text{SrFe}_{12}\text{O}_{19}/\text{Ba}_2\text{Co}_2\text{Fe}_{12}\text{O}_{22}$  in weight ratios of 98/2, 96/4, 94/6, and 92/8 were examined in this study.

## 1.8 Objectives

1. Preparation of  $\text{SrFe}_{12}\text{O}_{19}/\text{Ba}_2\text{Co}_2\text{Fe}_{12}\text{O}_{22}$  composite of various weight ratio.
2. To investigate the effect of compositional parameters on structural and magnetic properties of M+Y composite ferrites.

## Chapter 2

### Literature Review

#### **Overview**

Large amount of research has been carried out to investigate magnetic and structural properties of ferrites. This section briefly addresses the important work done in last few years on M-type, Y-type and composite ferrites, followed by studies on exchange coupled ferrite involving hexaferrite as one of the phase.

## 2.1 M-type hexaferrites

Among the hexaferrites, Barium and Strontium ferrites have received substantial interest in recent decades due to their distinctive features such as high  $H_a$ ,  $H_c$ , mild  $M_s$ , and high FMR frequency. The important studies on pure and substituted strontium hexaferrite are the focus of this section.

In 1996, Zhiqiang Jin et al. [24] synthesized SrM hexaferrite by mechanical alloying. It has been found that low-temperature annealing treatment can influence structural change similarly to a protracted milling procedure.  $M_s$  of 74.8 emu/g and  $H_c$  of 5.6 kOe found in those samples which milled for 30 hours and annealed at 1000 °C. The results showed little changes in the  $M_s$  and  $H_c$  of powders can be seen with prolonged annealing, whereas low properties are produced by short annealing times. Further in early 20s, Mohammad Naeem Ashiq et al. [25] used chemical coprecipitation method to synthesize  $\text{SrZr}_x\text{Cd}_x\text{Fe}_{12-2x}\text{O}_{19}$  (for  $x = 0.0, 0.2, 0.4, 0.6$ ). It has been found that at modest doping levels of  $x = 0.2$  the saturation magnetization increased while the coercivity decreased. The results suggested that synthesized materials are suitable for high-density recording media applications.

Later on, Ebrahim Roohani et al. [26] synthesized  $(\text{SrFe}_{12-x}\text{Co}_x\text{O}_{19}, x = 0 \text{ to } 1)$  by sol-gel auto-combustion method. They performed FT-IR which shows the values of characteristic frequencies for the  $\text{SrFe}_{12-x}\text{Co}_x\text{O}_{19}$  samples were moved to a lower frequency as the cobalt doping level increased. The results showed the  $M_s$  increased with cobalt content up to  $x = 0.5$  and then gradually declined when the dopant concentration was increased further, while the  $H_c$  steadily decreased with increasing Co content. To investigate the structural and magnetic characteristics Chaocheng Liu et al. [27] synthesized  $\text{SrCo}_x\text{Ti}_x\text{Fe}_{12-x}\text{O}_{19}$  ( $x=0.00-1.25$ ) via ceramic reaction route in 2019. The results showed  $M_s$  increased slowly as a whole, while  $H_c$  decreased gradually when  $x = 1.00$ . According to  $M(T)$  data, Co-Ti substitution can successfully lower the sample's  $T_p$  and  $T_c$ . The

results suggested  $\text{SrCo}_x\text{Ti}_x\text{Fe}_{12-x}\text{O}_{19}$  show potential characteristics for use in multilayer inductors. However, J.C. Guzman-Mínguez et al. [8] in 2020 prepared SrM hexaferrite with the addition of  $\text{SiO}_2$  and CaO via dry mixing method to maximize the energy product  $(BH)_{max}$ . They investigated  $\text{SiO}_2$  effectively suppress exaggerated grain growth which significantly increases the  $H_c$  of the ceramic dense samples. The results showed that the optimal balance between  $H_c$ ,  $M_s$  and density values is achieved by sintering for 4h at 1200 °C with a  $\text{SiO}_2$  content of 1 wt%. In addition, Raman microscopy shows the presence of hematite phase formation.

In the year 2021, Le-Zhong Li et al. [28] synthesized  $\text{Sr}_{1-x}\text{Y}_x\text{Fe}_{12-x}\text{Co}_x\text{O}_{19}$  ( $0 \leq x \leq 0.50$ ) via solid-state route to investigate structural and magnetic characteristics. It has been found that porosity of samples increased as the density of sintered samples declined with increasing Y-Co substitution. The results showed that  $M_s$  dropped monotonically as the amount of Y-Co substitution increased while the coercivity initially increased till x rises from 0 to 0.20 after which it decreased.

Sachin Kumar Godara et al. [29] prepared  $\text{SrZn}_x\text{Zr}_x\text{Fe}_{12-2x}\text{O}_{19}$  ( $x = 0.00-0.15$ ) to analyze structural as well as magnetic behavior in 2022. Increase in lattice parameter and volume was observed from XRD analysis. Raman spectra showed that crystals are undergoing strain with increasing  $\text{Zn}^{2+}$ - $\text{Zr}^{4+}$  concentration. The results showed that  $H_c$  lies in the range from 5164Oe ( $x = 0.00$ ) to 6210Oe ( $x = 0.15$ ) and  $M_s$  lies between 71.22 and 82.16 emu/g. Thus, the improvement in SrM's magnetic properties after doping with  $\text{Zn}^{2+}$ - $\text{Zr}^{4+}$  may be crucial for applications involving permanent magnets. Jae-Young Choi et al. [30] synthesized (SrM-Al,  $\text{SrFe}_{12-x}\text{Al}_x\text{O}_{19}$ ,  $0 \leq x \leq 4$ ) by solid state reaction method in the same year. They found significant microstructural inhomogeneity and residual strain which corresponds to poor magnetic performance, therefore to encourage phase formation and slow down rapid grain growth, sodium ions were added using a type of NaOH. As

a consequence, the simultaneous addition of Na and Al ions significantly increased the  $(BH)_{max}$  of randomly aligned hard magnetic ceramics to 1.23MGOe.

Recently, Xiang Yu et al. [31] used conventional ceramic method to prepare  $\text{SrFe}_{12-2x}\text{Zn}_x\text{Sn}_x\text{O}_{19}$  ( $x = 0, 0.25, 0.5, 1, 1.5, 2$ ). The larger ionic radii of  $\text{Zn}^{2+}$ - $\text{Sn}^{4+}$  leads to lattice expansion with increasing substitution. It has been observed that saturation magnetization reaches its maximum value,  $M_s = 77$  emu/g, with  $x = 0.25$ . The sample's  $M_s$  and  $H_c$  will drop monotonically when the amount of  $\text{Zn}^{2+}$ - $\text{Sn}^{4+}$  co-substitution is more than or equal to 0.5. Overall, the result suggests  $\text{SrFe}_{12-2x}\text{Zn}_x\text{Sn}_x\text{O}_{19}$  is a prospective high-density magnetic recording candidate when  $x=0.25$ .

## 2.2 Y-type hexaferrites

In early 20s, Yang Bai et al. [32] synthesized Cu, Zn-modified  $\text{Co}_2\text{Y}$  by solid-state ceramic route. XRD analysis shows single phase of modified Y-type hexaferrites formed at low temperature. Magnetic measurements showed increase in  $M_s$  and decrease in  $H_a$  with the substitution of  $\text{Zn}^{2+}$  and reduced sintered temperature with the substitution of  $\text{Cu}^{2+}$ . The results recommended modified  $\text{Co}_2\text{Y}$  had better magnetic characteristics in the hyper-frequency band. To investigate how temperature affects microstructure and magnetic characteristics Nimai Chand Pramanik et al. [33] prepared  $\text{Ba}_2\text{Co}_2\text{Fe}_{12}\text{O}_{22}$  ( $\text{Co}_2\text{Y}$ ) by polymeric sol–gel method in 2006. It has been discovered that microstructure with particle sizes ranging from 130 to 400nm are created at 900°C, which is significantly lower than the solid state approach. The results revealed a range of  $H_c$  (130–1566Oe) and  $M_s$  (30.9–47.6emu/g) depending upon temperature. The maximum  $M_s$  value reported is 47.60 emu/g at 800°C.

M.M. Costa et. al. [34] prepared  $\text{Ba}_2\text{Co}_2\text{Fe}_{12}\text{O}_{22}$  ( $\text{Co}_2\text{Y}$ ) doped with  $\text{Bi}_2\text{O}_3$  via solid state reaction method in 2011. The parameters of the dielectric impedance were investigated over the frequency

range of 1 Hz to 1 MHz and in the temperature range of 313 to 493 K. In the next year, Rajshree B. Jotania et al. [11] synthesized series of  $\text{Sr}_2\text{Cu}_{2-x}\text{Co}_x\text{Fe}_{12}\text{O}_{22}$  ( $x = 0.0$  to  $1.0$ ) via chemical co-precipitation technique. XRD analysis shows single phase Y-type hexaferrite formed below  $950^\circ\text{C}$  sintering temperature Dielectric measurements were taken, and a drop in dielectric properties was seen as frequency increased. Results showed that  $M_s$  and  $M_r$  decreased with the Co doping content.

M. M. Rashad et al. [35] synthesized  $\text{Ba}_2\text{Co}_2\text{Fe}_{12}\text{O}_{22}$  via two routes, namely sol-gel auto-combustion (SGA) and co-precipitation (CP) method in 2018. It was observed that porosity decreased in CP route. The result shows for the SGA and CP techniques,  $M_s$  of 23.64 and 24.37 emu/g and  $H_c$  of 417.76 and 280.92 Oe were achieved for samples pre-annealed at  $600^\circ\text{C}$  for 4 h and then annealed at  $1000^\circ\text{C}$  for 2 h, respectively. In the same year, R. Vinaykumar et al. [36] prepared  $\text{Ba}_{2-x}\text{La}_x\text{Co}_2\text{Fe}_{12-x}\text{Zn}_x\text{O}_{22}$ , (for  $x = 0.0, 0.1, 0.3$  and  $0.5$ ) via solid-state route. The value of  $M_s$  increased from 32 emu/g in unsubstituted  $\text{Co}_2\text{Y}$  to 47.7 emu/g in  $x = 0.5$  composition, while the  $H_c$  also increased with La-Zn substitution. The results concluded La-Zn substitution in  $\text{Co}_2\text{Y}$  ferrite was an excellent approach for increasing its magnetic and dielectric properties.

In-situ polymerization technique was used by G Packiaraj et al. [37] in 2020 to prepare polyaniline-blended  $\text{Ba}_2\text{Ni}_2\text{Fe}_{12}\text{O}_{22}$  hexaferrite (weight ratios 1:1, 1:2 and 2:1) . It has been found that value of dielectric constants increased in polyaniline-blended Y-type hexaferrite. The value of  $M_s$ ,  $H_c$  and  $M_r$  decreased and tuned with polyaniline concentration. Recently in 2022, Yu Gao et al. [38] synthesized  $\text{Co}_2\text{Y}$  using sol-gel method to study the dielectric and magnetic characteristics by varying sintering temperature (T). The single Y-type hexaferrite phase was formed at  $T \leq 1200^\circ\text{C}$ . It was discovered that as temperature increased, the resonance peak of frequency moved from 10.2 GHz to 1.9 GHz. The effective absorption bandwidth reached 7.3 GHz

at 1100°C with a thickness of only 1.4 mm demonstrates remarkable microwave absorption capabilities.

### 2.3 Composite Ferrites

Composites have gained a lot of attention in recent years because of their incredible microwave applications, and there has been a lot of research done on their magnetic characteristics over the last few decades. This section outlines the work reported thus far.

To study the structural and magnetic properties with heat treatment Xiansong Liu et al. [39] formed  $\text{SrFe}_{12}\text{O}_{19}/\gamma\text{-Fe}_2\text{O}_3$  in 2002. The results revealed that value of  $H_c=6015$  Oe,  $M_s=75.6$  emu/g and  $(BH)_{max}=1.87$  MGOe has found in the samples treated at 800°C. From the magnetic measurements and the dM plot, the exchange coupling interaction was observed in the sample which treated below 800°C. In 2009, Debansu Roy et al. [19] synthesized  $\text{BaFe}_{12}\text{O}_{19}/\text{Ni}_{0.8}\text{Zn}_{0.2}\text{Fe}_2\text{O}_4$  composite and studied its structural and magnetic properties. The behavior of exchange coupling was investigated at two distinct temperatures: 400 °C and 800 °C. The composite heated at 400 °C has more profound exchange interactions. The presence of a wide region in the second quadrant revealed that chemical preparation along with adequate sintering conditions resulted the development of a magnet with a high  $(BH)_{max}$  value. Also, Liuyang Zhang et al. [40] used two step co-precipitation method to synthesize  $\text{SrFe}_{12}\text{O}_{19}/\text{CoFe}_2\text{O}_4$  nanocomposites with core-shell structure. An XRD study revealed a coating of  $\text{CoFe}_2\text{O}_4$  nanoparticles on the surface of  $\text{SrFe}_{12}\text{O}_{19}$  nanoparticle which was also supported by Raman and TEM measurements. The result shows, in composites the magnetic properties found to be decreased while their microwave absorption capabilities improve significantly.

Haibo Yang et al. [18] prepared BaFe<sub>12</sub>O<sub>19</sub>/Y<sub>3</sub>Fe<sub>5</sub>O<sub>12</sub> nanocomposite via one step chemical method in 2015. SEM images revealed the presence of hexagonal and plate-like grains. It has been found that the largest reflection loss was -40.8 dB at 9.9GHz. One pot solution combustion method was used by S. R. Saeedi Afshar et al. [41] to synthesize SrFe<sub>12</sub>O<sub>19</sub>/Ni<sub>0.6</sub>Zn<sub>0.4</sub>Fe<sub>2</sub>O<sub>4</sub> in 2018. The results showed that 90:10 composites had well exchange coupled interaction with maximum  $M_s$  of 56emu/g. Hence, with the addition of the Ni-Zn ferrite phase, the  $H_c$  of composites dropped from 5143 to 1778 Oe. Microwave measurements for 90:10 composite was carried out at 9.9 GHz; minimum reflection loss was -23.5 dB.

In the year 2019, Farzin Mohseni et al. [42] prepared BaM/Fe<sub>3</sub>O<sub>4</sub> core-shell-like nanocomposite via hydrothermal method. The results indicated a 40% increase in  $M_s$  and a 75% rise in  $(BH)_{max}$  in the BaM/Fe<sub>3</sub>O<sub>4</sub> 9:1 hard/soft nanocomposite. It has been concluded that synthesized composite employed as permanent magnets in a number of applications, including permanent magnet motors and electrical devices. Chhavi Pahwa et al. [43] synthesized BaFe<sub>12</sub>O<sub>19</sub>/Ni<sub>0.5</sub>Zn<sub>0.5</sub>Fe<sub>2</sub>O<sub>4</sub> by sol-gel auto combustion route in different weight ratios. The composite with weight ratio 70/30 showed maximum  $M_s$  while decrease in coercivity observed. The maximum RL for annealed samples at 1050 °C was found to be -38 dB.

P. Maltoni et al. [44] used one-pot sol-gel route in 2021 to prepare SrFe<sub>12</sub>O<sub>19</sub>/Co<sub>1-x</sub>Zn<sub>x</sub>Fe<sub>2</sub>O<sub>4</sub> composite (for x= 0.1, 0.3 and 0.5) having 80/20 hard to soft ratio. Lattice parameter increases with Zn<sup>2+</sup> content was observed through XRPD analysis. Magnetic measurements showed maximum  $M_s$  is 74Am<sup>2</sup>/kg for x = 0.3 and  $H_c$  is 240kA/m. Recently, V. Bilovol et al. [45] prepared (100-x)SrFe<sub>12</sub>O<sub>19</sub>/(x)CoFe<sub>2</sub>O<sub>4</sub> composites using physical mixing method with x= 10, 20, 30 and 40 wt%. XRD analysis confirms the co-existence of both phases for the samples which annealed at 900°C for 3 h. The results showed that composite with 10% CoFe<sub>2</sub>O<sub>4</sub> has the  $(BH)_{max} = 10.9$

$\text{kJ/m}^3$ , this value is nearly 20% greater than the pure  $\text{SrFe}_{12}\text{O}_{19}$ . The existence of exchange coupling effect, as confirmed by Henkel plots, explains the improved magnetic characteristics of composite.

## Chapter 3

### Experimental Details

#### **Overview**

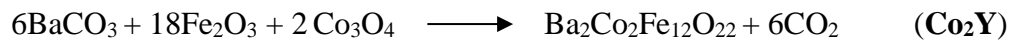
In this chapter, details of the processing technique used for the preparation of  $\text{SrFe}_{12}\text{O}_{19}$  (SrM),  $\text{Ba}_2\text{Co}_2\text{Fe}_{12}\text{O}_{22}$  (Co<sub>2</sub>Y) and series of SrM/Co<sub>2</sub>Y composite ferrites are explained. Various characterization techniques used for structural, morphological and magnetic measurements of ferrites has been briefly explained.

### 3.1 Sample Preparation

The preparation of samples has been divided into two sections. At first, pure M-type and Y-type hexaferrites were prepared via solid-state ceramic route. And in second section preparation of composites using as-prepared powders are explained.

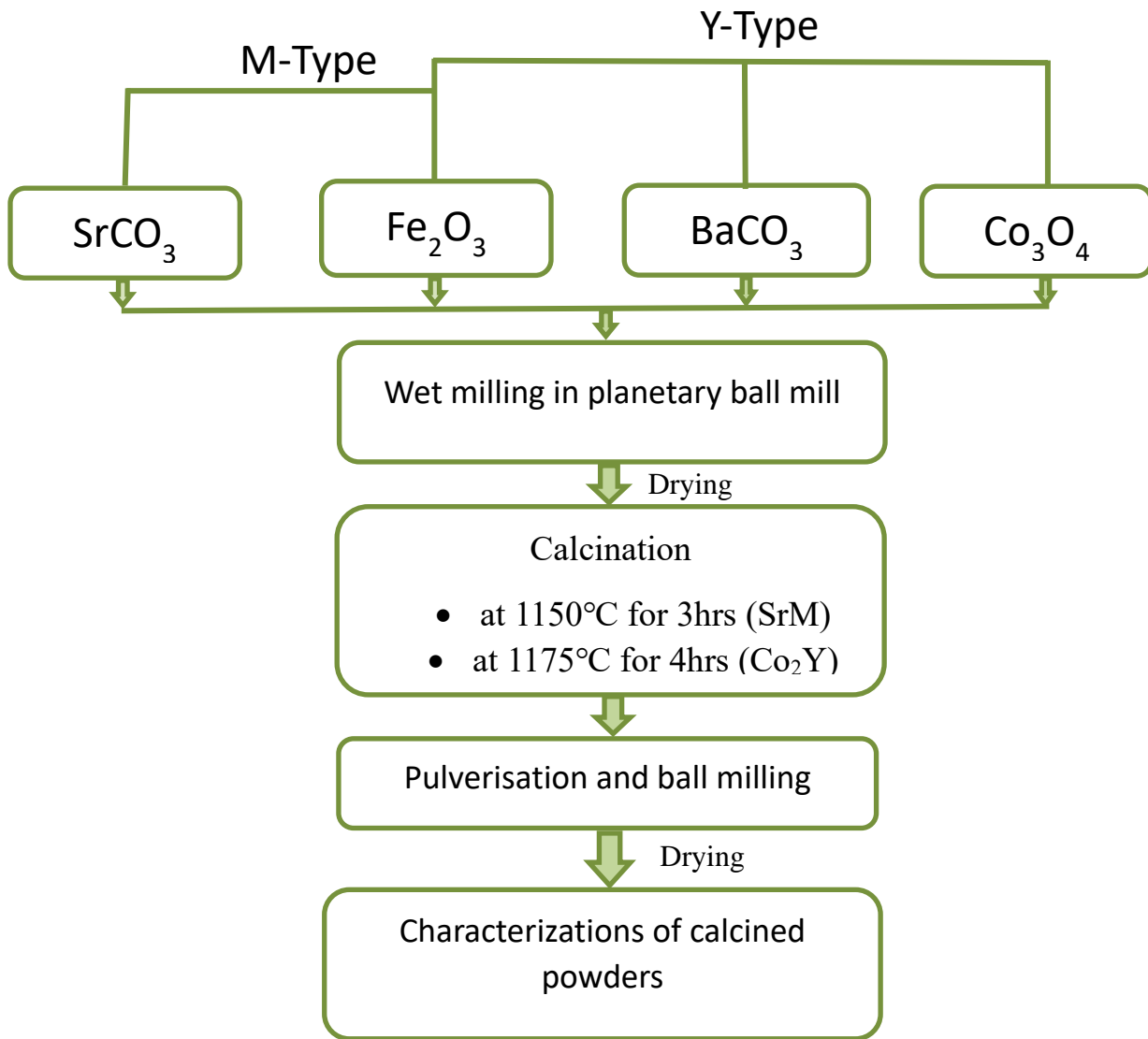
#### 3.1.1 Preparation of powders:

Analytical grade Strontium carbonate ( $\text{SrCO}_3$ ), Barium carbonate ( $\text{BaCO}_3$ ), Cobalt oxide ( $\text{Co}_3\text{O}_4$ ) and Iron oxide ( $\text{Fe}_2\text{O}_3$ ) were used as precursors. For the synthesis, precursors were weighed in stoichiometric amount given below:



The powders were wet milled in zirconia jar for 3 hours using planetary ball mill. The charge to ball ratio and rpm were kept constant to 1:2 and 100 respectively. As-mixed powders were dried and pelletized using hydraulic press at a pressure of 13 tons. Further the pellets were calcined in tubler furnace. The calcination temperature and time for SrM and  $\text{Co}_2\text{Y}$  were kept  $1130^\circ\text{C}$  for 3 hrs and  $1175^\circ\text{C}$  for 4 hrs, respectively. The heating as well as cooling rate was kept constant to  $5^\circ\text{C}/\text{min}$ . The calcined pellets were pulverized, sieved and again wet milled in tungsten jar for 1 hour with constant charge to ball ratio (1:5) and rpm  $\sim 175$  using planetary ball mill.

**Flowchart 1** Preparation of SrM and Co<sub>2</sub>Y powders by solid-state ceramic route



### 3.1.2 Preparation of SrM/ Co<sub>2</sub>Y composites

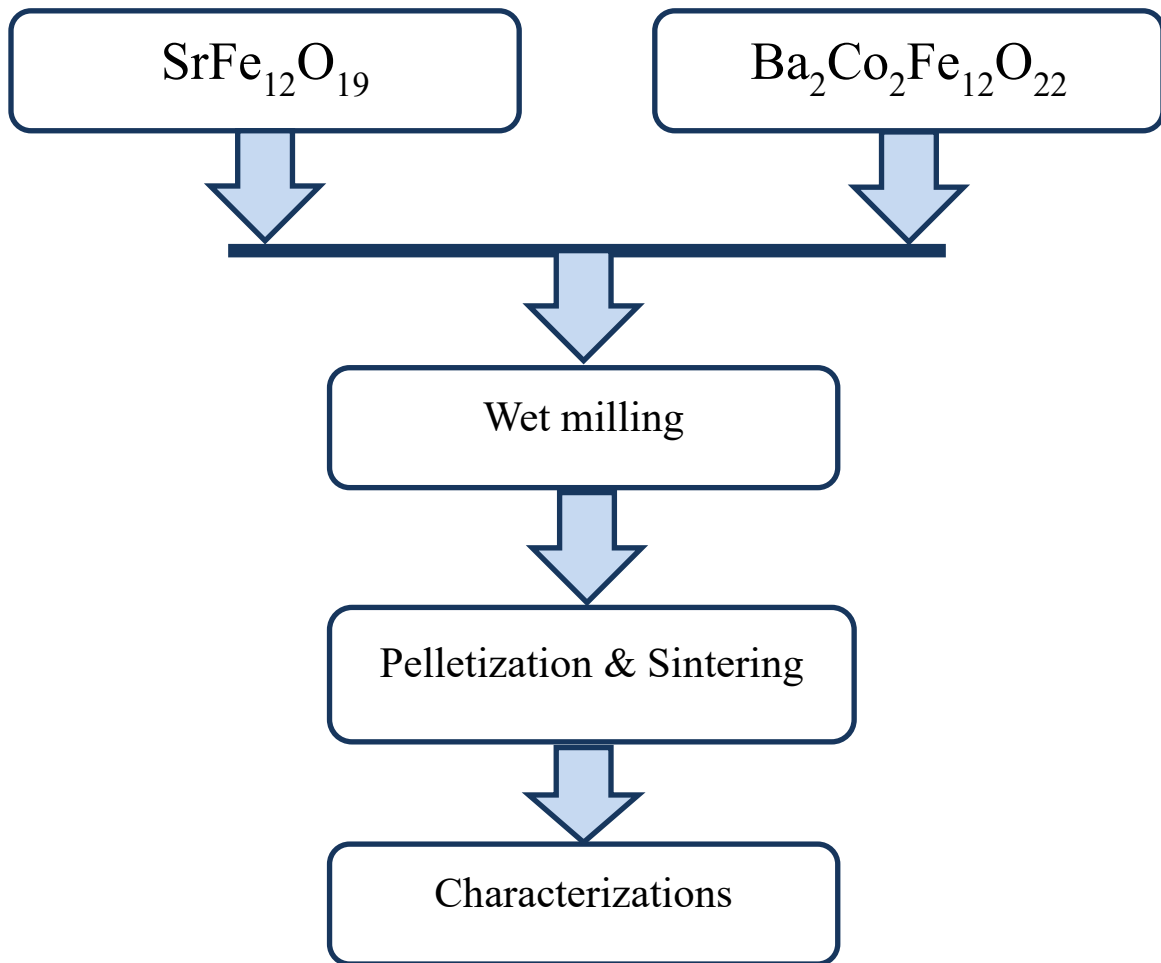
(1-x)SrM/xCo<sub>2</sub>Y (x=0.2,0.4,0.6,0.8) composites were synthesized by mixing as-prepared powders of M- type and Y-type using ball milling for 3 hrs. The charge to ball ratio and rpm were kept constant to 1:2 and 120 respectively.



**Fig. 3.1** Planetary Ball mill and Zirconia jar with M-Y sample.

Further, the powder was mixed with 5 wt % PVA binder and dried. The dried powder was pelletized using hydraulic press. These pellets were sintered in a muffle furnace for 1 h at 1200 °C. After sintering, the pellets were pulverized, sieved and wet milled using tungsten jar for 1 hour with constant charge to ball ratio (1:5) and rpm ~175 in planetary ball mill.

**Flowchart 2** Preparation of SrM/Co<sub>2</sub>Y composites.



### **3.2 Characterization technique:**

The structural, morphological and magnetic properties of SrM, Co<sub>2</sub>Y and SrM/Co<sub>2</sub>Y composites were analyzed using following techniques:

#### **1. X-ray Diffractometer**

Rigaku SmartLabSE XRD instrument was used to study the phase formation in SrM, Co<sub>2</sub>Y and SrM/Co<sub>2</sub>Y composites. The phase analysis was performed at room temperature in a scanning range of 20°-80° (2θ) and step size of 0.02°.

#### **2. Raman Spectroscopy**

Raman Spectroscopy was carried by Labram HR Confocal Micro-Raman Spectrometer equipped with 532nm laser. The spectral signature obtained from Raman spectroscopy were deconvoluted by Lorentzian fit to verify different Raman active modes.

#### **3. Field Emission Scanning Electron Microscope:**

Surface morphology of SrM, Co<sub>2</sub>Y and SrM/Co<sub>2</sub>Y composites was determined using Carl Zeiss Sigma 500 FEG-SEM instrument. Before measuring, the sample surface was sputtered with gold to prevent sample charging induced by static field accumulation.

#### **4. Vibrating Sample Magnetometer:**

The magnetic characteristics of SrM, Co<sub>2</sub>Y, and SrM/Co<sub>2</sub>Y composites were investigated using the Lake Shore 7404 VSM instrument. At room temperature, a magnetic field in -1 tesla to +1 tesla range was applied.

## Chapter 4

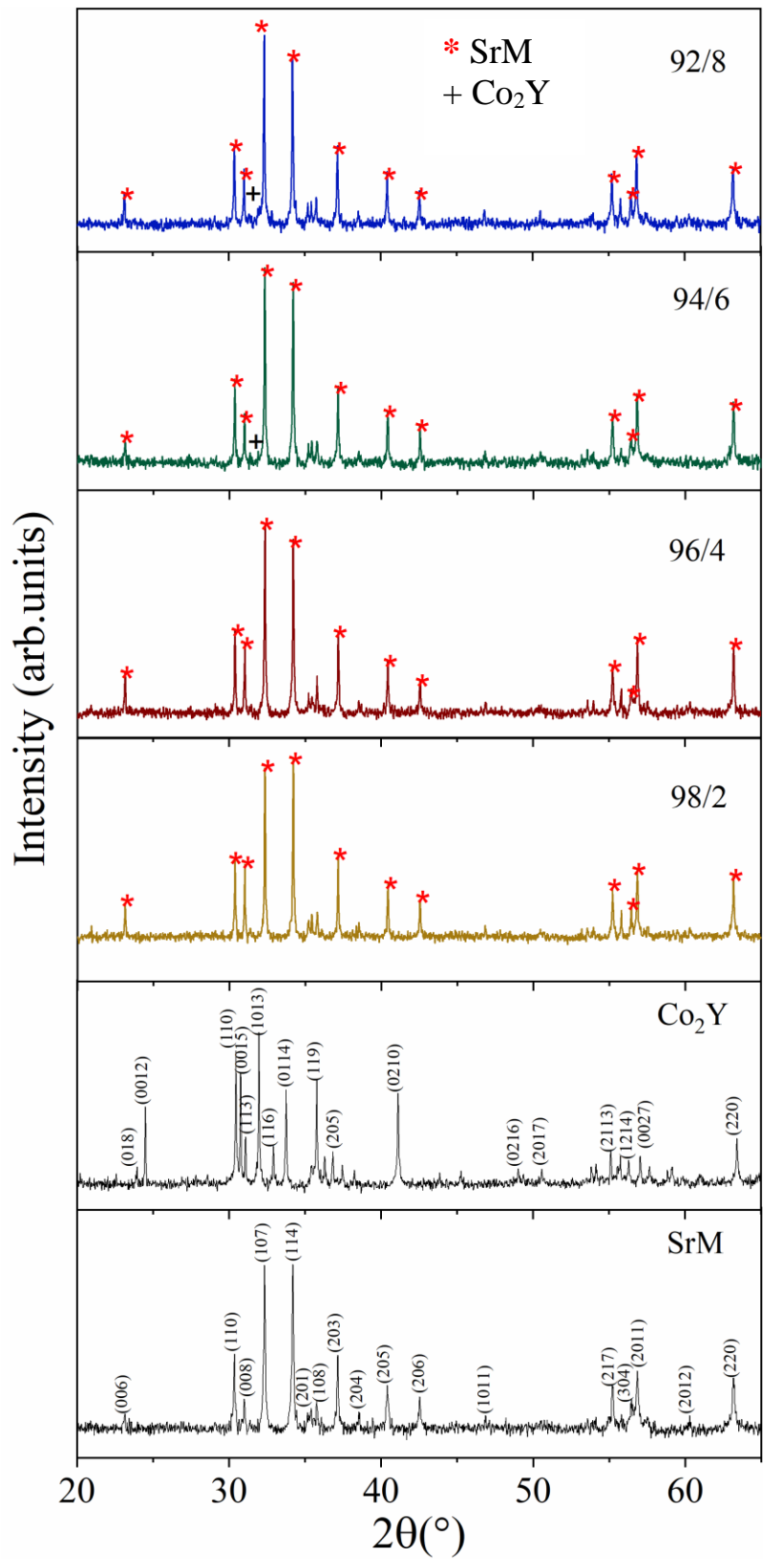
### Results and Discussions

#### **Overview**

Firstly, XRD analysis of SrM, Co<sub>2</sub>Y and their compositions were discussed. Further, FE-SEM and Raman analysis was performed to investigate microstructure and lattice vibrations of SrM, Co<sub>2</sub>Y and their compositions. Lastly, the magnetic behavior of powder and composite was investigated using Vibrating Sample Magnetometer (VSM).

## 4.1 X-Ray Diffraction (XRD)

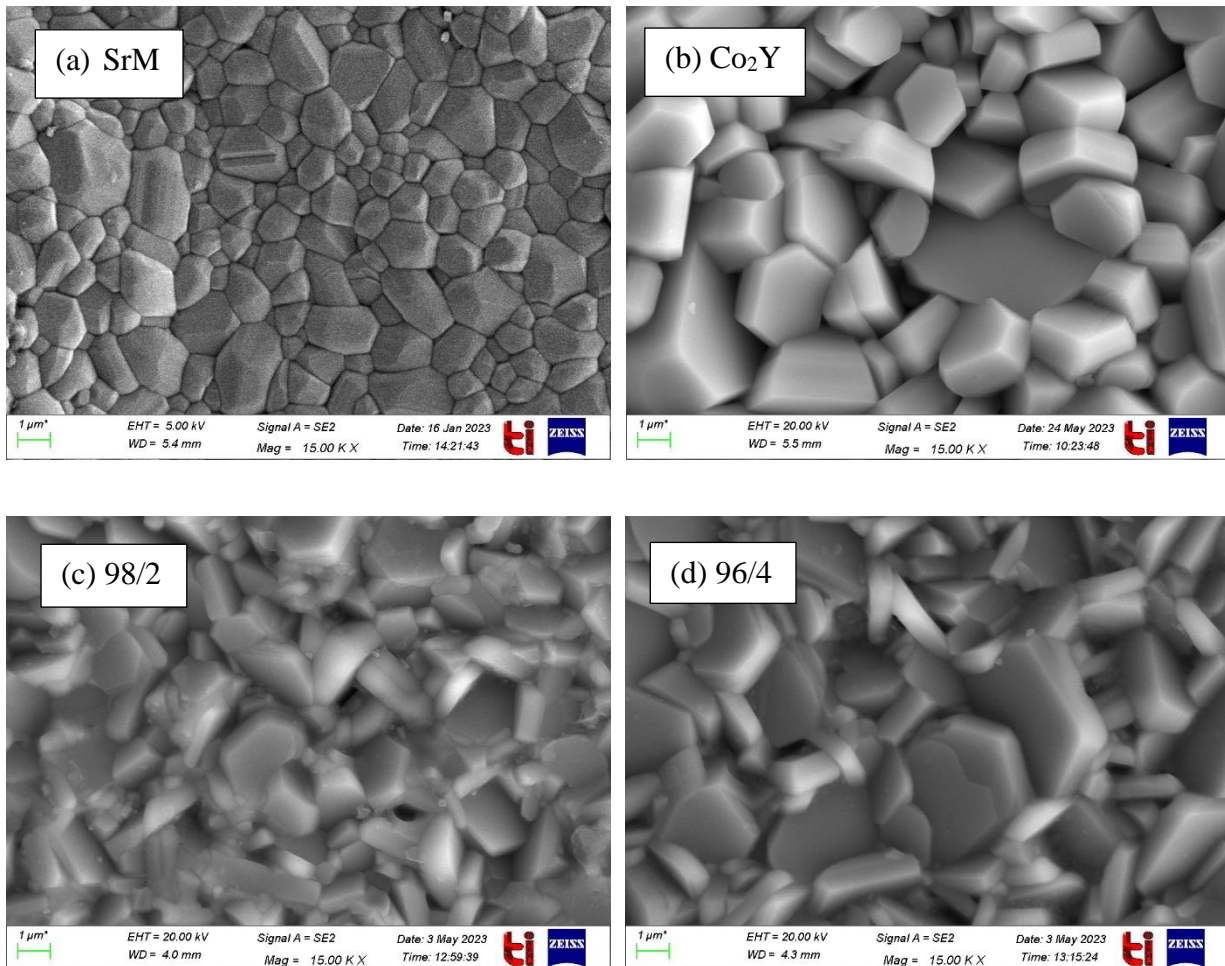
XRD patterns of pure SrM, Co<sub>2</sub>Y and SrM/Co<sub>2</sub>Y composite ferrites in different weight ratios (98/2, 96/4, 94/6, 92/8) are shown in [fig. \(4.1\)](#). All diffraction peaks in SrM and Co<sub>2</sub>Y ferrite corresponds to hexagonal phase which are well matched with standard ICDD card no. #01-079-1412, #00-044-0206. In SrM/Co<sub>2</sub>Y composites with weight ratio 98/2 and 96/4 all diffraction peaks correspond to M-type and Y-type phase peaks are not identified due to its low content increasing the Y content to 6% (94/6) and 8% (92/8) characteristics peak of Co<sub>2</sub>Y is appeared., which confirms the co-existence of both phases.

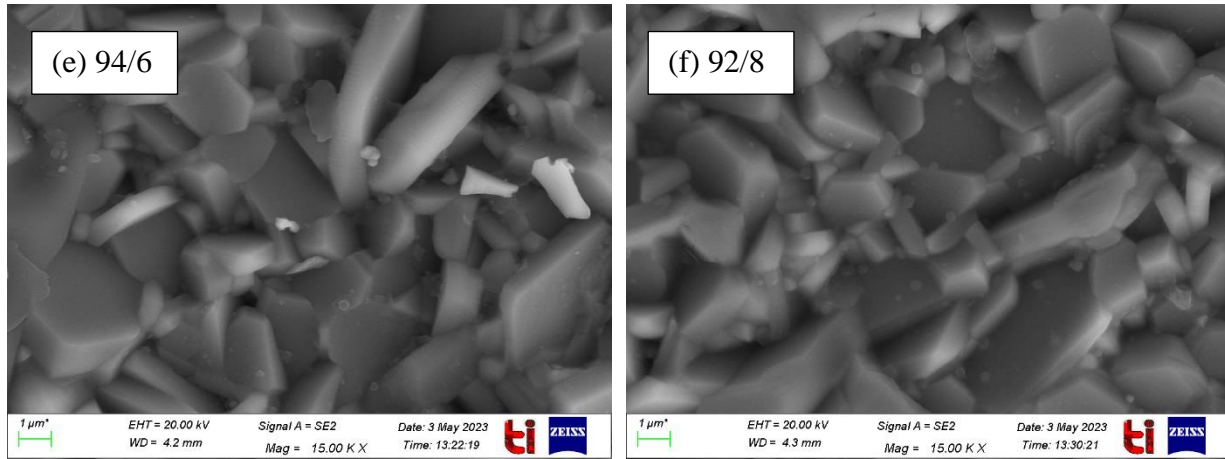


**Fig 4.1** X-ray diffraction pattern of pure SrM, pure Co<sub>2</sub>Y and SrM/Co<sub>2</sub>Y composites.

## 4.2 Field Emission Scanning Electron Microscope (FE-SEM)

Fig. 4.2 represents surface morphology of SrM, Co<sub>2</sub>Y and SrM/Co<sub>2</sub>Y composite ferrites in different weight ratios sintered at 1200°C. Micrographs of pure SrM, and Co<sub>2</sub>Y showed densely packed well separated grains with hexagonal morphology. The Y-type hexaferrite shows relative larger grain than M-type ferrite, this suggested that the sintering temperature is sufficiently high for in-plane grain growth. In composites, grains are not well separated as in pure ferrites, which may due to the competitive pinning and growth mechanism between both the phases. Moreover, it is difficult to distinguish among the phase due to it similar grain morphology and elements. It is notable that with increasing Y-type phase content, the fraction of large platelets are increasing.





**Fig. 4.2** SEM images of (a) SrM, (b) Co<sub>2</sub>Y and (c-f) SrM/Co<sub>2</sub>Y composites in different weight ratios

### 4.3 Raman Spectroscopy

Raman spectroscopy was employed to determine vibrations related with the crystal structure of SrM and Co<sub>2</sub>Y hexaferrites. The Raman spectrum of hexaferrites typically exhibits a range of vibrational modes, which can be attributed to different types of lattice vibrations, such as stretching, bending, and rotational motions of the atoms within the crystal lattice.

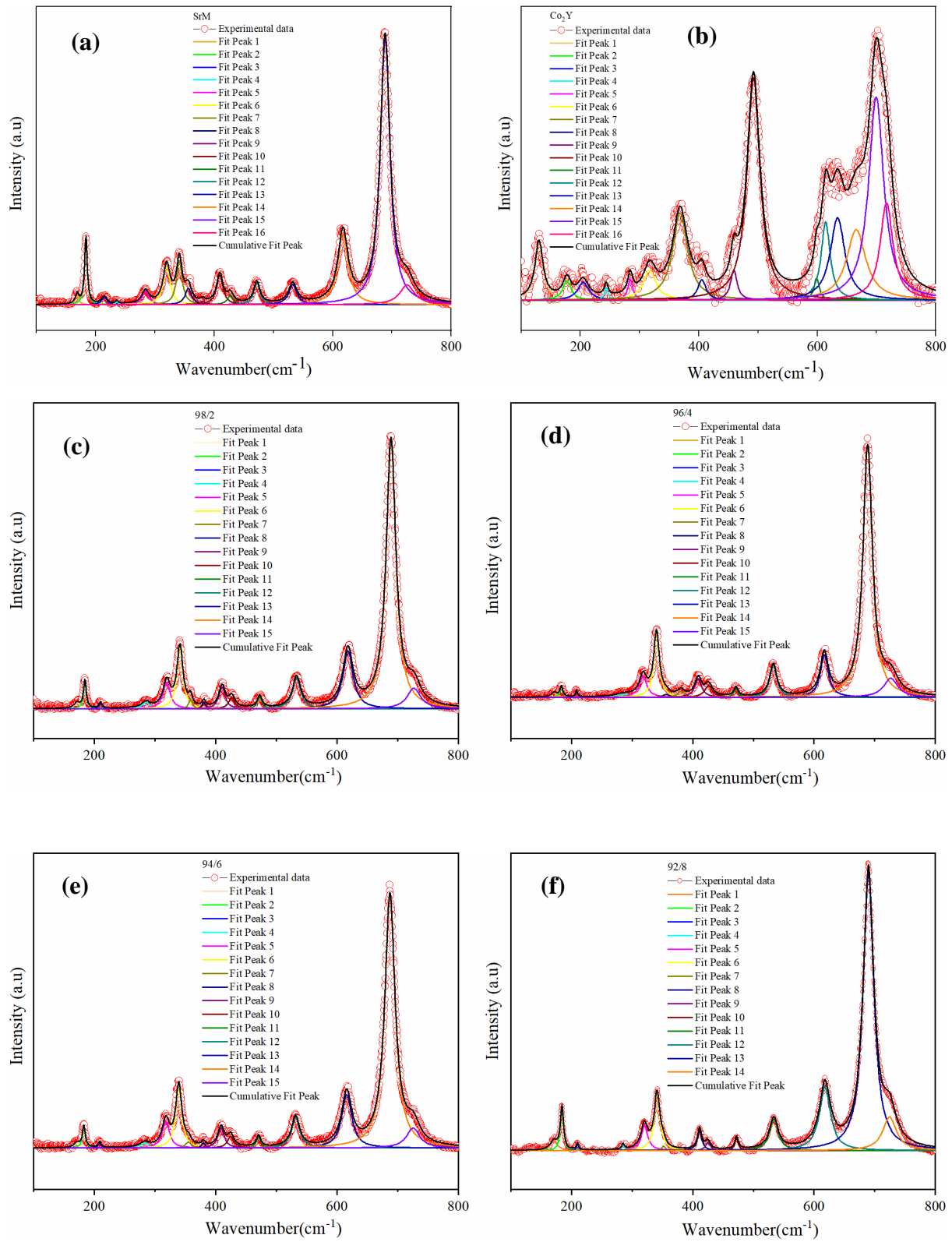
Fig. 4.3 shows Raman spectra of SrM, Co<sub>2</sub>Y, and SrM/Co<sub>2</sub>Y composite ferrites within the range of 200 to 800 cm<sup>-1</sup>. Peak parameters obtained from Lorentzian fits are given in Table 4.1. Group theory treatment yields SrM has 42 Raman active modes (11A<sub>1g</sub>+14E<sub>1g</sub>+17E<sub>2g</sub>) and 30 IR-active modes (13A<sub>2u</sub>+17E<sub>1u</sub>) [46]. All the peaks observed in fig 4.3 (a) agreed with the magnetoplumbite structure as reported in literature[47]. The Raman-active modes at 168 and 183 cm<sup>-1</sup> correspond to spinel block vibrations with E<sub>1g</sub> symmetry. Peaks at 409, 472, 617, 688 and 726 cm<sup>-1</sup> of A<sub>1g</sub> symmetry associated to 12k, 12k+2a, 4f<sub>2</sub>, 2b and 4f<sub>1</sub> sites respectively, whereas the peak centered at 341 cm<sup>-1</sup> of A<sub>1g</sub>+E<sub>1g</sub> symmetry assigned to octahedra mixed site. In Y-type hexaferrites the results of a group-theory analysis of the lattice vibrations at the  $\Gamma$  point are as follows[48]:

$$\Gamma = 14A_{1g}(a^2 + b^2, c^2) + 4A_{1u}(-) + 4A_{2g}(-) + 16A_{2u}(c) + 18E_g(a^2 - b^2, ab, ac, bc) + 20E_u(ab) \quad (2)$$

Raman spectra of Co<sub>2</sub>Y barium hexaferrite exhibit modes at 177, 205, 244, 284, 317, 368, 405, 459, 492, 599, 614, 634, 666, 699 and 717 cm<sup>-1</sup> fig. 4.4 (b). The peak at 177 cm<sup>-1</sup> with E<sub>1g</sub> symmetry is assigned to spinel block, while the bands at 614, 699 and 717 cm<sup>-1</sup> with A<sub>1g</sub> symmetry are assigned to 4f<sub>2</sub>, 2b and 4f<sub>1</sub> sites respectively. To the best of our knowledge, there is minimal literature on Y-type hexaferrite Raman spectroscopy[49]. The Raman spectra of SrM/Co<sub>2</sub>Y composites shows a dominant peak at 689 cm<sup>-1</sup> fig. 4.3 (c-f) corresponding to SrM hexaferrite. However, the Co<sub>2</sub>Y peak was not visible in the composites this could be due to the low concentration of Y-type content; as the Raman intensity is depending on the materials concentration.

**Table 4.1: Band assignment and Raman shift from fitted spectra of SrM/Co<sub>2</sub>Y composite ferrite**

Peak	Symmetry	SrM	Co <sub>2</sub> Y	98/2	96/4	94/6	92/8
			130				
<b>Spinel block</b>	E <sub>1g</sub>	168	177	172	172	171	171
<b>Spinel block</b>	E <sub>1g</sub>	183		184	183	183	184
	E <sub>1g</sub>	214	205	210	208	209	210
		236					
	E <sub>1g</sub>		244				
	E <sub>1g</sub>	284	284	285	287	284	285
	E <sub>2g</sub>	320	317	319	318	318	320
<b>Octahedra mixed</b>	A <sub>1g</sub> +E <sub>1g</sub>	341		341	340	339	341
--	--	356		358	356	355	352
	E <sub>1g</sub>		368				
		381		381	381	380	--
	A <sub>1g</sub>		405				
<b>12k (dominated)</b>	A <sub>1g</sub>	409		410	409	409	411
--	E <sub>2g</sub>	428		427	426	425	425
			459				
<b>12k+2a</b>	A <sub>1g</sub>	472		473	471	471	472
	A <sub>1g</sub>		492				
--	E <sub>2g</sub>	533		533	533	532	534
			599				
<b>4f2</b>	A <sub>1g</sub>	617	614	618	617	616	618
			634				
			666				
<b>2b</b>	A <sub>1g</sub>	688	699	689	688	687	690
<b>4f1</b>	A <sub>1g</sub>	726	717	727	727	726	725



**Fig. 4.3** Raman spectra for (a) SrM, (b) Co<sub>2</sub>Y and (c-f) SrM/Co<sub>2</sub>Y composite at different weight ratios.

## 4.4 Magnetic measurements

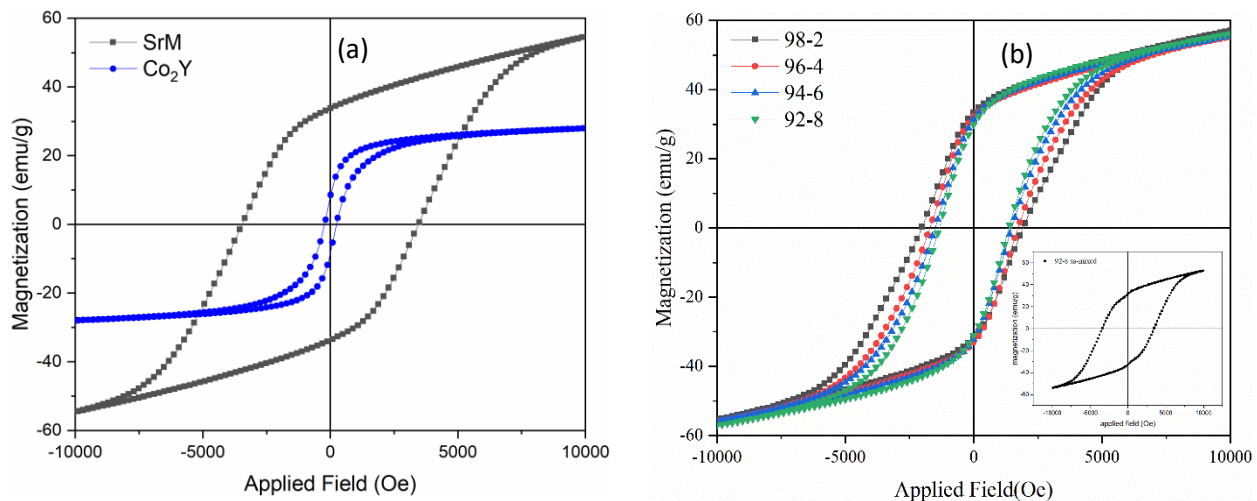
The room temperature  $M-H$  loop of SrM, Co<sub>2</sub>Y, and SrM/Co<sub>2</sub>Y composite ferrites are shown in [fig. 4.4 \(a & b\)](#). A non-saturated magnetization curve of SrM is observed, which requires a higher applied field to saturate. A very high coercivity and magnetization at 1 tesla represent the characteristic of hard magnets. The  $M-H$  loop of Co<sub>2</sub>Y is well saturated verifies its in-plane low magneto-crystalline anisotropy and depicts the properties of soft magnets.

The  $M-H$  loop of as-prepared composites of different composition exhibited smooth demagnetization curve (second quadrant) similar to single-phase hysteresis loop, confer to good exchange coupling between M-Y ferrite. The kink observed in as-mixed composite ([inset 4.4 \(b\)](#)) represents non-exchange couple system. The observed magnetic parameters are tabulated in [table 4.2](#).

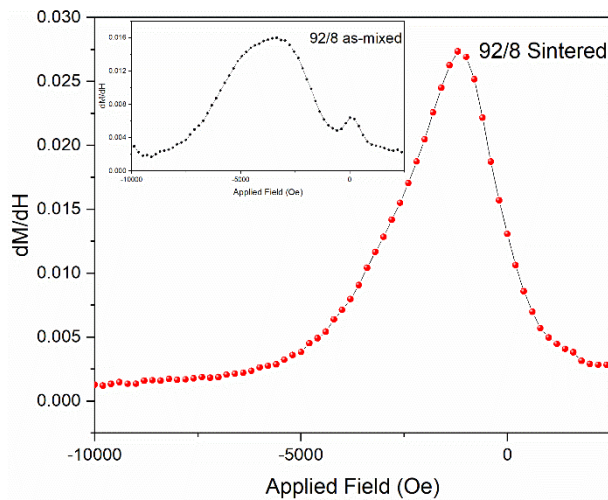
To confirm exchange coupling between composites single field distribution (SFD) curves were plotted. The obtained single peak in SFD curve [fig 4.5](#) indicates strong coupling between M-Y ferrite corresponds to coherent switching of both phases with applied field. On the other hand, SFD curve ([inset 4.5](#)) of non-exchange coupled composite contains two distinct peaks; indicating individual switching of both phases with applied field.

**Table 4.2: Magnetic properties of SrM, Co<sub>2</sub>Y and SrM/Co<sub>2</sub>Y composites**

Magnetic Properties	SrM/Co <sub>2</sub> Y weight ratio					
	SrM	98/2	96/4	94/6	92/8	Co <sub>2</sub> Y
<b>M<sub>s</sub> (emu/g)</b>	54.4	55.5	55.6	55.1	55.8	27.92
<b>H<sub>c</sub> (Oe)</b>	3461.2	2021.6	1750	1613.8	1416.2	231.4
<b>M<sub>r</sub>(emu/g)</b>	33.7	33.2	30.9	29.8	27.2	14.3



**Fig. 4.4** *M-H* loops of (a) SrM & Co<sub>2</sub>Y, and (b) sintered SrM/Co<sub>2</sub>Y composites in different weight ratios (inset shows *M-H* loop of as-mixed SrM/Co<sub>2</sub>Y (92/8) composite)

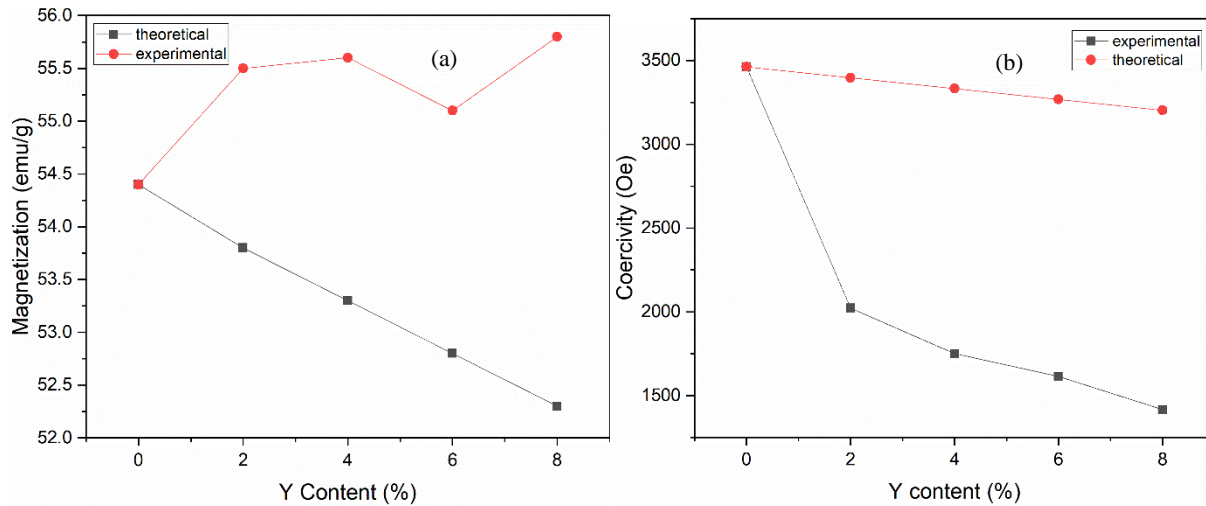


**Fig. 4.5** *dM/dH* vs applied field curve of exchange-coupled SrM/Co<sub>2</sub>Y (92/8) sintered composite; inset represents *dM/dH* vs applied field curve of non-exchange coupled composite.

Fig. 4.6 (a & b) depicts the change in  $M_s$  and  $H_c$  with  $\text{Co}_2\text{Y}$  content in composites. Theoretical values for  $M_s$  and  $H_c$  were computed using the rule of mixture and compared to experimental results:

$$M_c = (1-x)M_{IT}\text{SrM} + xM_{IT}\text{Co}_2\text{Y} \quad (1)$$

where,  $M_{IT}\text{SrM}$  and  $M_{IT}\text{Co}_2\text{Y}$  represents  $M_s$  of SrM (54.4 emu/g) and  $\text{Co}_2\text{Y}$  (27.92 emu/g) respectively. Similarly,  $H_c$  of the composites was computed and compared to experimental values for varied  $\text{Co}_2\text{Y}$  weight content.



**Fig. 4.6** Variation in theoretical and experimental observed (a)  $M_s$  and (b)  $H_c$  of SrM/ $\text{Co}_2\text{Y}$  composites with  $\text{Co}_2\text{Y}$  content

According to fig. 4.6 (a), the theoretical  $M_s$  of the composite decreases with the  $\text{Co}_2\text{Y}$  content. However experimentally,  $M_s$  of the composites increases with Y content this could be due to well interfacial coupling among M-type and Y-type phases as confirmed by demagnetization curve. Moreover, in SrM major fraction of spins are aligned in the field direction but due to grain boundary hinderance there are some spins which requires larger field or an additional driving force

to make them align in field direction. With addition of Co<sub>2</sub>Y phase due to its soft magnetic nature spins gets quickly align at much lower magnetic fields as it provides torque to hindered spins [43]. Consequently, a higher percentage of spin alignment raises the magnetization. Further in SrM/Co<sub>2</sub>Y composite having 94/6 weight ratio shows declination in  $M_s$  value as compared to other compositions which might occur due to the weak coupling between both phases.

On the contrary,  $H_c$  of the composites found to decrease [fig. 4.6 \(b\)](#) with Y content due to strong interfacial coupling between the phases where switching of Co<sub>2</sub>Y magnetic spins at low nucleation field drive away the hard magnetic spins. The obtained results shows that magnetic properties of composites are Y-phase dependent.

## Conclusion

The SrM/Co<sub>2</sub>Y composites in different weight ratios (98/2,96/4,94/6,92/8) were successfully synthesized by physical mixing of individual SrM and Co<sub>2</sub>Y powder. The impact of relative weight ratio on structural, morphological, and magnetic properties was studied. XRD pattern shows the coexistence of both phases which is also confirmed by Raman analysis. Magnetic property analysis at room temperature revealed smooth *M-H* loop which confirms the well exchange coupling in composites. Experimental  $M_s$  of composites found to be higher than both the phase, which further suggest the existing of interfacial coupling among the phase. An initial sharp decrease followed by linear decrease in coercivity was observed with the increasing Y content.

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